# $\checkmark$ Buchanan 1987 

Handbook of Electronics Tables and Formulas

# Handbook of Electronics Tables and Formulas <br> SIXTH EDITION 

Compiled and Edited by<br>The Howard W. Sams Engineering Staff

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## SIXTH EDITION

FIRST PRINTING—1986
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International Standard Book Number: 0-672-22469-0
Library of Congress Catalog Card Number: 86-60032
Editor: Sara Black
Illustrator: Ralph E. Lund
Interior Design: T. R. Emrick
Cover Art: Stephanie Ray
Shirley Engraving Co, Inc.
James F. Mier, Keller, Mier, Inc.
Composition: Photo Comp Corp.

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## Preface

The electronics industry is rapidly changing. New developments require frequent updating of information if any handbook such as this is to remain a useful tool. With this thought in mind, each item in the sixth edition was reviewed. Where necessary, additions or changes were made.

In previous editions, we asked for recommendations of additional items to consider for inclusion in future editions. Many suggestions were received and considered; most of them are incorporated in this volume. Hence, this book contains the information that users of the first five editions-engineers, technicians, students, experimenters, and hobbyists-have told us they would like to have in a comprehensive, one-stop edition.

We have added new sections on resistor and capacitor color codes, laws of heat flow in transistors and heat sinks, operational amplifiers, and basic fiber optics. We also detail how to add, subtract, multiply, and divide vectors on a computer as well as work with natural logarithms in computer programs. Computer programs that calculate many of the electronics formulas that appear in the text are part of the two new appendices.

Throughout the text we have attempted to clarify many misconceptions. For example, we clearly distinguish between the phys-
ical movement of a free electron and the guided wave motion produced by the electron's field. In addition, we present the volt as a unit of work or energy rather than a unit of electrical pressure or force. We also make a distinction between formulas or mathematical concepts and physical objects or measurements.

In addition, we have retained our comprehensive coverage of the broad range of commonly used electronics formulas and mathematical tables from the fifth edition.

- Chapter 1-The basic formulas and laws, so important in all branches of electronics. Nomographs that speed up the solution of DC power, parallel resistance, and reactance. Dimensions of the electrical units are also discussed.
- Chapter 2-Useful, but hard-toremember constants and governmentand industry-established standards. The comprehensive table of conversion factors is especially helpful in electronics calculations.
- Chapter 3-Symbols and codes that have been adopted over the years. The latest semiconductor information is included.


## Preface

- Chapter 4-ltems of particular interest to electronics service technicians.
- Chapter 5-Data most often used in circuit design work. The filter and attenuator configurations and formulas are particularly useful to service technicians and design engineers.
- Chapter 6-Mathematical tables and formulas. The comprehensive table of powers, roots, and reciprocals is an important feature of this section.
- Chapter 7-Miscellaneous items such as measurement conversions, table of elements, and temperature scales.
- Appendices-Computer programs for basic electronics formulas.

No effort has been spared to make this handbook of maximum value to anyone, in any branch of electronics. Once again your comments, criticisms, and recommendations for any additional data you would like to see included in a future edition will be welcomed.

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## Chapter 1

## Electronics Formulas AND LAWS

## OHM'S LAW FOR DIRECT CURRENT

All substances offer some obstruction to the flow of current. According to Ohm's law, the current that flows is directly proportional to the applied voltage and inversely proportional to the resistance. Thus, referring to Fig. 1-1:

$$
\begin{aligned}
I & =\frac{E}{R} \\
E & =I R \\
R & =\frac{E}{I}
\end{aligned}
$$

where
$I$ is the current, in amperes,
$E$ is the voltage, in volts, $R$ is the resistance, in ohms.


Fig. 1-1

Note. The volt is the work that is done by a battery or generator in separating unit charges through unit distance; the volt is the basic unit of potential energy per unit of charge flow.

## DC POWER

The power $P$ expended in load resistance $R$ when current $I$ flows under a voltage pressure $E$ can be determined by the formulas:

$$
\begin{aligned}
& P=E I \\
& P=I^{2} R \\
& P=\frac{E^{2}}{R}
\end{aligned}
$$

where
$P$ is the power, in watts, $E$ is the voltage, in volts, $I$ is the current, in amperes, $R$ is the resistance, in ohms.

## OHM'S LAW FORMULAS

A composite of the electrical formulas that are based on Ohm's law is given in Fig.

1-2. These formulas are virtually indispensable for solving DC electronic circuit problems.

| UnknowR <br> Value | Formulas |  |  |
| :---: | :--- | :--- | :--- |
| $E$ | $E=\mathbb{R}$ | $E=P / I$ | $E=\sqrt{P R}$ |
| 1 | $I=E / R$ | $I=P / E$ | $I=\sqrt{P / R}$ |
| $P$ | $P=E l$ | $P=E^{2} / R$ | $P=I^{2} R$ |
| $R$ | $R=E / I$ | $R=E^{2} / P$ | $R=P / I^{2}$ |

## Fig. 1-2

Free electrons travel slowly in conductors because there is an extremely large number of free electrons available to carry the charge flow (current). If a current of 1 A flows in ordinary bell wire (diameter about 0.04 in ), the velocity of each free electron is approximately $0.001 \mathrm{in} / \mathrm{s}$. Thus, if the wire were run 3000 mi across the country, it would take more than 6025 years for an electron entering the wire at San Francisco to emerge from the wire at New York. Nevertheless, because each free electron exerts a force on its adjacent electrons, the electrical impulse travels along the wire at the rate of $186,000 \mathrm{mi} / \mathrm{s}$. Or, the electrical impulse would be evident at New York in less than 0.02 s .

Formulas are used to calculate unknown values from known values. For example, if it is known that $E=10$ and $R=2$, then the formula $I=E / R$ can be used to calculate that $I=5$ A. Similarly, the formula $P=E I$ can be used to calculate that $P=50 \mathrm{~W}$. Since $I=E / R$, the formula $P=E I$ can be used to calculate that $P=E^{2} / \mathrm{R}$, or $100 / 2=50 \mathrm{~W}$. The same answer is obtained whether the formula $P=E I$ or the formula $P=E^{2} / \mathrm{R}$ is used.

Note, however, that $E$ is physically real and that $E^{2}$ is physically unreal. In other words, $E$ is both physically and mathematically real. On the other hand, $E^{2}$ is physi-
cally unreal, although $E^{2}$ is mathematically real. $E^{2}$ is a mathematical stepping-stone to go from one physical reality to another physical reality. Thus, the formula $P=E^{2} /$ R states a mathematical reality, although this formula is a physical fiction. Such relations are summarized by the basic principle that states equations are mathematical models of electrical and electronic circuits.

## OHM'S LAW NOMOGRAPH

The nomograph presented in Fig. 1-3 is a convenient way of solving most Ohm's law and DC power problems. If two values are known, the two unknown values can be determined by placing a straightedge across the two known values and reading the unknown values at the points where the straightedge crosses the appropriate scales. The figures in boldface (on the right-hand side of all scales) cover one range of given values, and the figures in lightface (on the left-hand side) cover another range. For a given problem, all values must be read in either the bold- or lightface figures.

Example. What is the value of a resistor if a $10-\mathrm{V}$ drop is measured across it and a current of 500 $\mathrm{mA}(0.5 \mathrm{~A})$ is flowing through it? What is the power dissipated by the resistor?
Answer. The value of the resistor is $20 \Omega$. The power dissipated in the resistor is 5 W .

## KIRCHHOFF'S LAWS

According to Kirchhoff's voltage law, "The sum of the voltage drops around a DC series circuit equals the source or applied voltage." In other words, disregarding losses due to the wire resistance, as shown in Fig. 1-4:

$$
E_{\mathrm{T}}=E_{1}+E_{2}+E_{3}
$$

## Electronics Formulas and Laws



Fig. 1-3. Ohm's law and DC power nomograph.

Fig. 1-4

where
$E_{\mathrm{T}}$ is the source voltage, in volts, $E_{1}, E_{2}$, and $E_{3}$ are the voltage drops across the individual resistors.

According to Kirchhoff's current law, "The current flowing toward a point in a circuit must equal the current flowing away from that point." Hence, if a circuit is divided into several parallel paths, as shown in Fig. 1-5, the sum of the currents through the individual paths must equal the current flowing to the point where the circuit branches, or:

$$
I_{1}=I_{1}+I_{2}+I_{3}
$$

where
$I_{1}$ is the total current, in amperes, flowing through the circuit,
$I_{1}, I_{2}$, and $I_{3}$ are the currents flowing through the individual branches.


Fig. 1-5
In a series-parallel circuit (Fig. 1-6), the relationships are as follows:

$$
\begin{aligned}
E_{\mathrm{T}} & =E_{1}+E_{2}+E_{3} \\
I_{\mathrm{T}} & =I_{1}+I_{2} \\
I_{1} & =I_{3}
\end{aligned}
$$

where
$E_{\mathrm{T}}$ is the source voltage, in volts, $E_{1}, E_{2}$, and $E_{3}$ are the voltage drops across the individual resistors,
$I_{\mathrm{r}}$ is the total current, in amperes, flowing through the circuit, $I_{1}, I_{2}$, and $I_{3}$ are the currents flowing through the individual branches.


Fig. 1-6

Note. Although the term "current flow" is in common use, it is a misnomer in the physical sense of the words. Current is defined as the rate of charge flow. Voltage does not flow, resistance does not flow, and current does not flow.

## RESISTANCE

The following formulas can be used for calculating the total resistance in a circuit.

Resistors in series (Fig. 1-7):

$$
R_{\mathrm{T}}=R_{\mathrm{i}}+R_{2}+R_{3}+\cdots
$$

Resistors in parallel (Fig. 1-8):

$$
R=\frac{1}{\frac{1}{R_{1}}+\frac{1}{R_{2}}+\frac{1}{R_{3}}+\cdots}
$$

Two resistors in parallel (Fig. 1-9):

$$
R_{\mathrm{T}}=\frac{R_{1} \times R_{2}}{R_{1}+R_{2}}
$$



Fig. 1-7


Fig. 1-9


Fig. 1-8
where
$R_{\mathrm{T}}$ is the total resistance, in ohms, of the circuit,
$R_{1}, R_{2}$, and $R_{3}$ are the values of the individual resistors.

The equivalent value of resistors in parallel can be solved with the nomograph in Fig. 1-10. Place a straightedge across the points on scales $R_{1}$ and $R_{2}$ where the known value resistors fall. The point at which the


Fig. 1-10. Parallel-resistance nomograph.
straightedge crosses the $R_{\mathrm{r}}$ scale will show the total resistance of the two resistors in parallel. If three resistors are in parallel, first find the equivalent resistance of two of the resistors, then consider this value as being in parallel with the remaining resistor.

If the total resistance needed is known, the straightedge can be placed at this value on the $R_{\mathrm{T}}$ scale and rotated to find the various combinations of values on the $R_{1}$ and $R_{2}$ scales that will produce the needed value.

Scales $R_{\mathrm{IY}}$ and $R_{\mathrm{TY}}$ are used with the $B_{1}$ scale when the values of the known resistors differ greatly. The range of the nomograph can be increased by multiplying the values of all scales by $10,100,1000$, or more, as required.

Note. Ohm's law states that $R=E / I$. In turn, effective resistance is often calculated as an $E / I$ ratio. For example, if the beam current in a TV picture tube is 0.5 mA , and the potential-energy difference from cathode to screen is $15,000 \mathrm{~V}$, then the effective resistance from cathode to screen is 30 $\mathrm{M} \Omega$. The power dissipated in the effective resistance is 7.5 W . From a practical viewpoint, the physical power is dissipated by the screen and not in the space from cathode to screen. In other words, the effective resistance is a mathematical reality but a physical fiction.

Example 1. What is the total resistance of a $50-\Omega$ and a $75-\Omega$ resistor in parallel?

Answer. $30 \Omega$.

Example 2. What is the total resistance of a $1500-\Omega$ and a $14,000-\Omega$ resistor in parallel?

Answer. $1355 \Omega$. (Use $R_{1}$ and $R_{\mathrm{TY}}$ scales; read answer on $R_{\text {TY }}$ scale.)

Example 3. What is the total resistance of a $75-\Omega$, an $85-\Omega$, and a $120-\Omega$ resistor in parallel?

Answer. $30 \Omega$. (First, consider the $75-\Omega$ and $85-\Omega$ resistors, which will give $40 \Omega$; then consider this 40 $\Omega$ and the $120-\Omega$ resistor, which will give $30 \Omega$.)

## CAPACITANCE

The following formulas can be used for calculating the total capacitance in a circuit. Capacitors in parallel (Fig. 1-11):

$$
C_{\mathrm{T}}=C_{1}+C_{2}+C_{3}+\cdots
$$



Fig. 1-11
Capacitors in series (Fig. 1-12):

$$
\begin{aligned}
& C_{\mathrm{T}}= \frac{1}{\frac{1}{C_{1}}+\frac{1}{C_{2}}+\frac{1}{C_{3}}+\cdots} \\
& \\
& c_{\mathrm{T}}- \\
& c_{1} c_{2} \\
& c_{3}
\end{aligned}
$$

Fig. 1-12
Two capacitors in series (Fig. 1-13):

$$
C_{\mathrm{T}}=\frac{C_{1} \times C_{2}}{C_{1}+C_{2}}
$$

where
$C_{\mathrm{T}}$ is the total capacitance in a circuit, $C_{1}, C_{2}$, and $C_{3}$ are the values of the individual capacitors.

Note. $\mathrm{C}_{1}, \mathrm{C}_{2}$ may be in any unit of measurement as long as all are in the same unit. $\mathrm{C}_{\mathrm{T}}$ will be in this same unit.


Fig. 1-13
The parallel-resistance nomograph in Fig. 1-10 can also be used to determine the total capacitance of capacitors in series.

The capacitance of a parallel-plate capacitor is determined by:

$$
C=0.2235 \frac{k A}{d}(N-1)
$$

where
$C$ is the capacitance, in picofarads,
$k$ is the dielectric constant,*
$A$ is the area of one plate, in square inches,
$d$ is the thickness of the dielectric, in inches,
$N$ is the number of plates.

## Charge Stored

The charge stored in a capacitor is determined by:

$$
Q=C E
$$

where
$Q$ is the charge, in coulombs,
$C$ is the capacitance, in farads,
$E$ is the voltage impressed across the capacitor, in volts.

## Energy Stored

The energy stored in a capacitor can be determined by:

$$
W=\frac{C E^{2}}{2}
$$

[^0]where
$W$ is the energy, in joules (wattseconds),
$C$ is the capacitance, in farads, $E$ is the applied voltage, in volts.

## Voltage Across Series Capacitors

When an AC voltage is applied across a group of capacitors connected in series (Fig. 1-14), the voltage drop across the combination is, of course, equal to the applied voltage. The drop across each individual capacitor is inversely proportional to its capacitance. The drop across any capacitor in a group of series capacitors is calculated by the formula:

$$
E_{\mathrm{C}}=\frac{E_{\mathrm{A}} \times C_{\mathrm{r}}}{C}
$$

where
$E_{\mathrm{C}}$ is the voltage across the individual capacitor in the series ( $C_{1}, C_{2}$, or $C_{3}$ ), in volts,
$E_{A}$ is the applied voltage, in volts,
$C_{\mathrm{r}}$ is the total capacitance of the series combination, in farads,
$C$ is the capacitance of the individual capacitor under consideration, in farads.


Fig. 1-14
Since a capacitor is composed of a pair of metal plates separated by an insulator, such as air, a unit capacitor could be a pair of metal plates separated by 0.001 in , with
an area of $4.46 \times 10^{\prime} \mathrm{in}^{2}$. This unit capacitor will have a capacitance of 1 F . Voltage is potential energy per unit charge. In turn, if this capacitor is charged to a potentialenergy difference of 1 V (potential difference of 1 V ), the plates will attract each other with a force of approximately 4400 lb , or about two long tons. This force is exerted through a distance of 0.001 in . In other words, the potential difference gives the plates potential energy (energy of position).

As an example of voltage generation (potential-energy generation) by charge separation, suppose that the capacitor described above has been charged to a potential-energy difference of 1 V . Then, if the separation between the plates is increased from 0.001 in to 0.002 in , the poten-tial-energy difference increases to 2 V . In other words, $Q=C E$, and $E$ is inversely proportional to the separation between the plates. $Q$ remains constant ( 1 C ), $E$ is doubled ( 2 V ), and $C$ is halved ( 0.5 F ). The separation between unit charges has been increased through unit distance, with the result that a potential-energy difference of 1 V has been generated.

The formula for calculating the capacitance is:

$$
C=2.24 \times 10^{-17} k A \frac{N-1}{d}
$$

where
$C$ is the capacitance, in farads, $k$ is the dielectric coefficient, $A$ is the area of one side of one plate, in square inches,
$d$ is the separation between the plates, in inches,
$N$ is the number of plates.
The formula for calculating the force of attraction between the two plates is:

$$
F=\frac{A V^{2}}{k(1504 S)^{2}}
$$

where
$F$ is the attractive force, in dynes, $A$ is the area of one plate, in square centimeters, $F$ is the potential-energy difference, in volts, $k$ is the dielectric coefficient, $S$ is the separation between the plates, in centimeters.

A dyne is about $1 / 980 \mathrm{~g}$; there are 454 g in 1 lb . When the separation between plates is doubled, the voltage (potential-energy difference) between the plates is doubled, but the charge and the force of attraction between the plates remain the same. Because the initial unit separation has been doubled, twice as much work has been done (the initial voltage has been doubled). Initial unit separation was assigned as 0.001 in in the foregoing example. The initial potentialenergy difference will, in turn, be assigned as 1 mV when calculating basic relations.

## INDUCTANCE

The following formulas can be used for calculating the total inductance in a circuit.

Inductors in series with no mutual inductance (Fig. 1-15):

$$
L_{\mathrm{r}}=L_{1}+L_{2}+L_{3}+\cdots
$$



Fig. 1-15

Inductors in parallel with no mutual inductance (Fig. 1-16):

$$
L_{\mathrm{T}}=\frac{1}{\frac{1}{L_{1}}+\frac{1}{L_{2}}+\frac{1}{L_{3}}+\cdots}
$$



Fig. 1-16
Two inductors in parallel with no mutual inductance (Fig. 1-17):

$$
L_{\mathrm{T}}=\frac{L_{1} \times L_{2}}{L_{1}+L_{2}}
$$

where
$L_{\mathrm{T}}$ is the total inductance of the circuit, in henrys,
$L_{1}$ and $L_{2}$ are the inductances of the individual inductors (coils).


Fig. 1-17
The parallel-resistance nomograph in Fig. 1-10 can also be used to determine the total inductance of inductors in parallel.

## Mutual Inductance

The mutual inductance of two coils with fields interacting can be determined by:

$$
M=\frac{L_{\mathrm{A}}-L_{\mathrm{B}}}{4}
$$

where
$M$ is the mutual inductance of $L_{\wedge}$ and $L_{B}$, in henrys,
$L_{\mathrm{A}}$ is the total inductance of coils $L_{1}$ and $L_{2}$ with fields aiding, in henrys, $L_{8}$ is the total inductance of coils $L_{1}$ and $L_{2}$ with fields opposing, in henrys.

## Coupled Inductance

The coupled inductance can be determined by the following formulas.

In parallel with fields aiding:

$$
L_{\mathrm{T}}=\frac{1}{\frac{1}{L_{1}+M}+\frac{1}{L_{2}+M}}
$$

In parallel with fields opposing:

$$
L_{\mathrm{T}}=\frac{1}{\frac{1}{L_{1}-M}-\frac{1}{L_{2}-M}}
$$

In series with fields aiding:

$$
L_{\mathrm{T}}=L_{1}+L_{2}+2 M
$$

In series with fields opposing:

$$
L_{\mathrm{T}}=L_{1}+L_{2}-2 M
$$

where
$L_{\mathrm{T}}$ is the total inductance, in henrys, $L_{1}$ and $L_{2}$ are the inductances of the
individual coils, in henrys, $M$ is the mutual inductance, in henrys.

## Coupling Coefficient

When two coils are inductively coupled to give transformer action, the coupling coefficient is determined by:

$$
K=\frac{M}{\sqrt{L_{1} L_{2}}}
$$

where
$K$ is the coupling coefficient, $M$ is the mutual inductance, in henrys, $L_{1}$ and $L_{2}$ are the inductances of the two coils, in henrys.

Note. An inductor in a circuit has a reactance of $j 2 \pi f L \Omega$. Mutual inductance in a circuit also has a reactance equal to $j 2 \pi f M \Omega$. The operator $j$ denotes that the reactance dissipates no energy, although the reactance opposes current flow.

## Energy Stored

The energy stored in an inductor can be determined by:

$$
W=\frac{L I^{2}}{2}
$$

where
$W$ is the energy, in joules (wattseconds),
$L$ is the inductance, in henrys, $I$ is the current, in amperes.

## Q FACTOR

The ratio of reactance to resistance is known as the $Q$ factor. It can be determined by the following formulas.

For a coil where $R$ and $L$ are in series:

$$
Q=\frac{\omega L}{R}
$$

For a capacitor where $R$ and $C$ are in series:

$$
Q=\frac{1}{\omega R C}
$$

where
$Q$ is a ratio expressing the factor of merit,
$\omega$ equals $2 \pi f$ and $f$ is the frequency, in hertz,
$L$ is the inductance, in henrys,
$R$ is the resistance, in ohms,
$C$ is the capacitance, in farads.

## RESONANCE

The resonant frequency, or the frequency at which the reactances of the circuit add up to zero ( $X_{L}=X_{C}$ ), is determined by:

$$
f_{\mathrm{R}}=\frac{1}{2 \pi \sqrt{L C}}
$$

where
$f_{\mathrm{R}}$ is the resonant frequency, in hertz,
$L$ is the inductance, in henrys,
$C$ is the capacitance, in farads.

The resonance equation for either $L$ or $C$ can also be solved when the frequency is known. Transposing the previous formula:

$$
\begin{aligned}
& L=\frac{1}{4 \pi^{2} f_{\mathrm{k}}{ }^{2} C} \\
& C=\frac{1}{4 \pi^{2} f_{\mathrm{R}}{ }^{2} L}
\end{aligned}
$$

The resonant frequency of various combinations of inductance and capacitance can also be obtained from the reactance charts in Fig. 1-18. Simply lay a straightedge across the values of inductance and capacitance, and read the resonant frequency from the frequency scale of the chart.

## ADMITTANCE

The measure of the ease with which alternating current flows in a circuit is the admittance of the circuit.

Admittance of a series circuit is given by:

$$
Y=\frac{1}{\sqrt{R^{2}+X^{2}}}
$$

Admittance is also expressed as the reciprocal of impedance; thus:

$$
Y=\frac{1}{Z}
$$

where
$Y$ is the admittance, in siemens,
$R$ is the resistance, in ohms,
$X$ is the reactance, in ohms,
$Z$ is the impedance, in ohms.

Admittance is equal to conductance plus susceptance. Conductance is the reciprocal of resistance. The unit of conductance is the siemens (formerly the mho). Inductive reactance is positive, and capacitive reactance is negative. Inductive susceptance is negative, and capacitive susceptance is positive. If an impedance has a positive phase angle, its corresponding admittance will have a negative phase angle, and the values of the two phase angles will be the same.

## SUSCEPTANCE

The susceptance of a series circuit is given by:

$$
B=\frac{X}{R^{2}+X^{2}}
$$

When the resistance is zero, susceptance becomes the reciprocal of reactance; thus:

$$
B=\frac{1}{X}
$$

where
$B$ is the susceptance, in siemens, $X$ is the reactance, in ohms, $R$ is the resistance, in ohms.

## CONDUCTANCE

Conductance is the measure of the ability of a component to conduct electricity. Conductance for DC circuits is expressed as the reciprocal of resistance; therefore:

$$
G=\frac{1}{R}
$$

where
$G$ is the conductance, in siemens, $R$ is the resistance, in ohms.

Ohm's law formulas when conductance is considered are:

$$
\begin{aligned}
& I=E G \\
& G=\frac{I}{E} \\
& E=\frac{I}{G}
\end{aligned}
$$

where
$I$ is the current, in amperes, $E$ is the voltage, in volts, $G$ is the conductance, in siemens.

## ENERGY UNITS

Energy is the capacity or ability to do work. The joule is a unit of energy. One joule is the amount of energy required to maintain a current of 1 A for 1 s through a resistance of $1 \Omega$. It is equivalent to a wattsecond. The watt-hour is the practical unit of energy; 3600 Ws equals 1 Wh . The number of watt-hours is calculated:

$$
\text { Watt-hours }=P \times T
$$

where
$P$ is the power, in watts, $T$ is the time, in hours, the power is dissipated.

See the section entitled Capacitance to determine the energy stored in a capacitor and the section entitled Inductance to determine the energy stored in an inductor.

## REACTANCE

The opposition to the flow of alternating current by the inductance or capacitance of a component or circuit is called the reactance.

## Capacitive Reactance

The reactance of a capacitor may be calculated by the formula:
where
$X_{\mathrm{c}}$ is the reactance, in ohms, $f$ is the frequency, in hertz,
$C$ is the capacitance, in farads.

## Inductive Reactance

The reactance of an inductor may be calculated by the formula:

$$
X_{\mathrm{i}}=2 \pi f L
$$

where
$X_{1}$ is the reactance, in ohms, $f$ is the frequency, in hertz, $L$ is the inductance, in henrys.

## Reactance Charts

Charts for determining unknown values of reactance, inductance, capacitance, and frequency are shown in Figs. 1-18A through 1-18C. The chart in Fig. 1-18A covers $1-1000 \mathrm{~Hz}$, Fig. $1-18$ B covers $1-1000 \mathrm{kHz}$, and Fig. 1-18C covers $1-1000 \mathrm{MHz}$.

To find the amount of reactance of a capacitor at a given frequency, lay the straightedge across the values for the capacitor and the frequency. Then read the reactance from the reactance scale. By extending the line, the value of an inductance, which will give the same reactance, can be obtained.

Since $X_{\mathrm{C}}=X_{\mathrm{L}}$ at resonance, by laying the straightedge across the capacitance and inductance values, the resonant frequency of the combination can be determined.

Example. If the frequency is 10 Hz and the capacitance is $50 \mu \mathrm{~F}$, what is the reactance of the capacitor? What value of inductance will give this same reactance?
Answer. $310 \Omega$. The inductance needed to produce this same reactance is 5 H . Thus, it follows that a $50-\mu \mathrm{F}$ capacitor and a $5-\mathrm{H}$ choke are resonant at 10 Hz . (Place the straightedge, on the proper chart [Fig. 1-18A], across 10 Hz and $50 \mu \mathrm{~F}$. Read the values indicated on the reactance and inductance scales.)


Fig. 1-18A. Reactance chart $-1 \mathbf{H z}$ to $1 \mathbf{k H z}$.


+ AJNOMO34.


Fig. 1-18B. Reactance chart-1 $\mathbf{k H z}$ to 1 MHz .


FREQUENCY $\ddagger$
in 8 8

200
150
100



Fig. 1-18C. Reactance chart-1 MHz to 1000 MHz .

## IMPEDANCE

The basic formulas for calculating the total impedance are as follows:

For parallel circuits:

$$
Z=\frac{1}{\sqrt{G^{2}+B^{2}}}
$$

or

$$
Z=\frac{R X}{\sqrt{R^{2}+X^{2}}}
$$

For series circuits:

$$
Z=\sqrt{R^{2}+X^{2}}
$$

where
$Z$ is the total impedance, in ohms, $G$ is the total conductance or the reciprocal of the total parallel resistance, in siemens,
$B$ is the total susceptance, in siemens,
$R$ is the total resistance, in ohms,
$X$ is the total reactance, in ohms.
The following formulas can be used to find the impedance of the various combinations of inductance, capacitance, and resistance.

For a single resistance (Fig. 1-19):

$$
\begin{aligned}
& Z=R \\
& \theta=0^{\circ}
\end{aligned}
$$



Fig. 1-19
For resistances in series (Fig. 1-20):

$$
Z=R_{1}+R_{2}+R_{3}+\cdots
$$

$$
\theta=0^{\circ}
$$



Fig. 1-20
For a single inductance (Fig. 1-21):

$$
\begin{aligned}
& Z=X_{1} \\
& \theta=90^{\circ} \\
& \text { min_ }
\end{aligned}
$$

Fig. 1-21
For inductances in series with no mutual inductance (Fig. 1-22):

$$
\begin{aligned}
& Z=X_{\mathrm{t}_{1}}+X_{\mathrm{L}_{2}}+X_{\mathrm{L}_{3}}+\cdots \\
& \theta=90^{\circ}
\end{aligned}
$$



Fig. 1-22
For a single capacitance (Fig. 1-23):

$$
\begin{gathered}
Z=X_{C} \\
\theta=90^{\circ} \\
\stackrel{\circ}{\circ}
\end{gathered}
$$

Fig. 1-23
For capacitances in series (Fig. 1-24):

$$
\begin{aligned}
Z & =X_{c_{1}}+X_{c_{2}}+X_{c_{3}}+\cdots \\
\theta & =90^{\circ}
\end{aligned}
$$



Fig. 1-24

For resistance and inductance in series (Fig. 1-25):

$$
\begin{aligned}
& Z=\sqrt{R^{2}+X_{\mathrm{L}}{ }^{2}} \\
& \theta=\arctan \frac{X_{\mathrm{L}}}{R} \\
& \text { —n_m }_{\text {h }}^{\mathrm{R}}
\end{aligned}
$$

Fig. 1-25
For resistance and capacitance in series (Fig. 1-26):

$$
\begin{aligned}
& Z=\sqrt{R^{2}+X_{\mathrm{C}}{ }^{2}} \\
& \theta=\arctan \frac{X_{\mathrm{C}}}{R}
\end{aligned}
$$

Fig. 1-26
For inductance and capacitance in series (Fig. 1-27):

When $X_{1}$ is larger than $X_{C}$ :

$$
Z=X_{\mathrm{L}}-X_{\mathrm{C}}
$$



Fig. 1-27
When $X_{C}$ is larger than $X_{1}$ :

$$
Z=X_{C}-X_{L}
$$

Note. $\theta=0^{\circ}$ when $X_{1}=X_{C}$.
For resistance, inductance, and capacitance in series (Fig. 1-28):

$$
\begin{aligned}
& Z=\sqrt{R^{2}+\left(X_{\mathrm{L}}-X_{\mathrm{C}}\right)^{2}} \\
& \theta=\arctan \frac{X_{1}-X_{\mathrm{C}}}{R} \\
& \text { n_m }^{\mathrm{R}} \mathrm{~m}^{\mathrm{L}}
\end{aligned}
$$

Fig. 1-28
For resistances in parallel (Fig. 1-29):

$$
\begin{aligned}
& Z=\frac{1}{\frac{1}{R_{1}}+\frac{1}{R_{2}}+\frac{1}{R_{3}}+\cdots} \\
& \theta=0^{\circ}
\end{aligned}
$$

## Fig. 1-29

For inductances in parallel with no mutual inductance (Fig. 1-30):

$$
\begin{aligned}
& Z=\frac{1}{\frac{1}{X_{\mathrm{L}_{1}}}+\frac{1}{X_{\mathrm{L}_{2}}}+\frac{1}{X_{\mathrm{L}_{3}}}+\cdots} \\
& \theta=90^{\circ}
\end{aligned}
$$



Fig. 1-30

For capacitances in parallel (Fig. 1-31):

$$
\begin{aligned}
Z & =\frac{1}{\frac{1}{X_{\mathrm{C}_{1}}}+\frac{1}{X_{\mathrm{C}_{2}}}+\frac{1}{X_{\mathrm{C}_{3}}}+\cdots} \\
\theta & =90^{\circ}
\end{aligned}
$$



Fig. 1-31
For resistance and inductance in parallel (Fig. 1-32):

$$
\begin{aligned}
& Z=\frac{R X_{\mathrm{L}}}{\sqrt{R^{2}+X_{\mathrm{L}}{ }^{2}}} \\
& \theta=\arctan \frac{R}{X_{\mathrm{L}}}
\end{aligned}
$$

Fig. 1-32
For capacitance and resistance in parallel (Fig. 1-33):

$$
\begin{aligned}
Z & =\frac{R X_{C}}{\sqrt{R^{2}+X_{C}^{2}}} \\
\theta & =\arctan \frac{R}{X_{C}}
\end{aligned}
$$



Fig. 1-33
The graphical solution for capacitance and resistance in series or in parallel (Fig. 1-34):


Fig. 1-34
For capacitance and inductance in parallel (Fig. 1-35):

When $X_{1}$ is larger than $X_{C}$ :

$$
Z=\frac{X_{\mathrm{L}} X_{\mathrm{C}}}{X_{\mathrm{L}}-X_{\mathrm{C}}}
$$

When $X_{C}$ is larger than $X_{\mathrm{L}}$ :

$$
Z=\frac{X_{\mathrm{C}} X_{\mathrm{L}}}{X_{\mathrm{C}}-X_{\mathrm{I}}}
$$



Fig. 1-35
Note. $\theta=0^{\circ}$ when $X_{1}=X_{C}$.
The graphical solution for resultant reactance of parallel inductive and capaci-
tive reactances (Figs. 1-36A and 1-36B):
When $X_{\mathrm{L}}$ is larger than $X_{\mathrm{C}}$ :


Fig. 1-36A
When $X_{\mathrm{C}}$ is larger than $X_{\mathrm{L}}$ :


## Fig. 1-36B

Note. In Figs. 1-36A and 1-36B, the base line $0-0$ may have any finite length. The input impedance of any network can be represented at a given frequency by $R$ and $C$ connected in series or by $R$ and $L$ connected in series. Or the input impedance can be represented at a given frequency by $R$ and $C$ connected in parallel or by $R$ and $L$ connected in parallel. Conversely, the output impedance of any network can be similarly represented at a given frequency.

For inductance, capacitance, and resistance in parallel (Fig. 1-37):

$$
\begin{aligned}
Z & =\frac{R X_{1} X_{\mathrm{C}}}{\sqrt{X_{\mathrm{L}}^{2} X_{\mathrm{C}}^{2}+R^{2}\left(X_{\mathrm{L}}-X_{\mathrm{C}}\right)^{2}}} \\
\theta & =\arctan \frac{R\left(X_{\mathrm{L}}-X_{\mathrm{C}}\right)}{X_{\mathrm{L}} X_{\mathrm{C}}}
\end{aligned}
$$



Fig. 1-37
For inductance and series resistance in parallel with resistance (Fig. 1-38):

$$
\begin{aligned}
& Z=R_{2} \sqrt{\frac{R_{1}{ }^{2}+X_{1}{ }^{2}}{\left(R_{1}+R_{2}\right)^{2}+X_{1 .}{ }^{2}}} \\
& \theta=\arctan \frac{X_{1} R_{2}}{R_{1}{ }^{2}+X_{1 .}{ }^{2}+R_{1} R_{2}}
\end{aligned}
$$



Fig. 1-38

For inductance and series resistance in parallel with capacitance (Fig. 1-39):

$$
\begin{aligned}
& Z=X_{\mathrm{C}} \sqrt{\frac{R^{2}+X_{\mathrm{L}}^{2}}{R^{2}+\left(X_{1}-X_{\mathrm{C}}\right)^{2}}} \\
& \theta=\arctan \frac{X_{\mathrm{L}}\left(X_{\mathrm{C}}-X_{\mathrm{L}}\right)-R^{2}}{R X_{\mathrm{C}}}
\end{aligned}
$$



Fig. 1-39

For capacitance and series resistance in parallel with inductance and series resistance (Fig. 1-40):
$Z=\sqrt{\frac{\left(R_{1}^{2}+X_{1}{ }^{2}\right)\left(R_{2}^{2}+X_{C}{ }^{2}\right)}{\left(R_{1}+R_{2}\right)^{2}+\left(X_{1 .}-X_{6}\right)^{2}}}$
$\theta=\arctan \frac{X_{1}\left(R_{2}{ }^{2}+X_{C^{2}}{ }^{2}\right)-X_{\mathrm{C}}\left(R_{1}{ }^{2}+X_{1}{ }^{2}\right)}{R_{\mathrm{I}}\left(R_{2}{ }^{2}+X_{\mathrm{C}}{ }^{2}\right)+R_{2}\left(R_{1}{ }^{2}+X_{\mathrm{L}}{ }^{2}\right)}$
where
$Z$ is the impedance, in ohms,
$R$ is the resistance, in ohms, $L$ is the inductance, in henrys, $X_{L}$ is the inductive reactance, in ohms, $X_{C}$ is the capacitive reactance, in ohms, $\theta$ is the phase angle, in degrees, by which the current leads the voltage in a capacitive circuit or lags the voltage in an inductive circuit. $0^{\circ}$ indicates an in-phase condition.


Fig. 1-40
The formulas in this section are written in "shorthand" form, wherein the signs of quantities and absolute values of quantities are implied rather than expressed. In turn, when the formulas are applied to a circuitaction problem, the appropriate signs must be supplied by the reader. For example, the "shorthand" form for inductive reactance is $Z=X_{\mathrm{L}}, \theta=90^{\circ}$. It is understood that the impedance is positive, and that the phase angle is positive. On the other hand, the "shorthand" form for capacitive reactance is $Z=X_{C}, \theta=90^{\circ}$, and it is understood that
the impedance is negative and that the phase angle is negative. In other words, these formulas state absolute values wherein signs are disregarded.

In the case of an ordinary $R C$ series circuit, its impedance is positive, but its phase angle is negative. In an ordinary $L C$ series circuit, its impedance may be either positive or negative, depending upon the operating frequency. At low frequencies, its impedance is negative (the circuit is capacitive). However, at high frequencies, its impedance is positive (the circuit is inductive). In turn, at low frequencies, an $L C$ series circuit has a phase angle of $-90^{\circ}$, which abruptly changes at a critical (resonant) frequency to $+90^{\circ}$.

## OHM'S LAW FOR ALTERNATING CURRENT

Referring to Fig. 1-41, the fundamental Ohm's law formulas for alternating current are given by:

$$
\begin{aligned}
E & =I Z \\
I & =\frac{E}{Z} \\
Z & =\frac{E}{I}
\end{aligned}
$$

where
$E$ is the voltage, in volts, $I$ is the current, in amperes, $Z$ is the impedance, in ohms.


Fig. 1-41

The power expended in an AC circuit is calculated by the formula:

$$
P=E I \cos \theta
$$

where
$P$ is the power, in watts,
$E$ is the voltage, in volts,
$I$ is the current, in amperes, $\theta$ is the phase angle, in degrees.

The phase angle is the difference in degrees by which the current leads or lags the voltage in a reactive circuit. In a series circuit, the phase angle is determined by the formula:

$$
\theta=\arctan \frac{X}{R}
$$

where
$\theta$ is the phase angle, in degrees,
$X$ is the inductive or capacitive reactance, in ohms,
$R$ is the nonreactive resistance, in ohms.

Therefore:
For a purely resistive circuit:

$$
\begin{aligned}
\theta & =0^{\circ} \\
\cos \theta & =1 \\
P & =E I
\end{aligned}
$$

For a resonant circuit:

$$
\begin{aligned}
\theta & =0^{\circ} \\
\cos \theta & =1 \\
P & =E I
\end{aligned}
$$

For a purely reactive circuit:

$$
\begin{aligned}
\theta & =90^{\circ} \\
\cos \theta & =0 \\
P & =0
\end{aligned}
$$

where
$P$ is the power, in watts, $E$ is the voltage, in volts, $I$ is the current, in amperes, $\theta$ is the phase angle, in degrees.

## AVERAGE, RMS, PEAK, AND PEAK-TO-PEAK VOLTAGE AND CURRENT

Table 1-1 can be used to convert sinusoidal voltage (or current) values from one method of measurement to another. To use the table, first find the given type of reading in the left-hand column, then find the desired type of reading across the top of the table. To convert the given value to the desired value, multiply the given value by the factor listed under the desired value.

Example. What factor must pak voltage be multiplied by to obtain root mean square (rms) voltage?

Answer: 0.707.
TABLE 1-1
Average, RMS, Peak, and Peak-to-Peak Values

| Given value | Multiplying factor to get |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Average | RMS | Peak | Peak-to-peak |
| average | - | 1.11 | 1.57 | 3.14 |
| rms | 0.9 | - | 1.414 | 2.828 |
| peak | 0.637 | 0.707 | - | 2.0 |
| peak-to-peak | 0.32 | 0.3535 | 0.5 | - |

## POWER FACTOR

Power factor is the ratio of true power to apparent power in an AC circuit. Thus, using Fig. 1-42:

$$
\begin{aligned}
p f & =\frac{P_{1}}{P_{A}}=\frac{E I \cos \theta}{E I} \\
& =\cos \theta
\end{aligned}
$$



Fig. 1-42
where
$p f$ is the power factor,
$P_{\mathrm{T}}$ is the true power, in watts,
$P_{\mathrm{A}}$ is the apparent power, in voltamperes,
$E I \cos \theta$ (Fig. 1-42) is the true power, in watts,
$E I$ is the apparent power, in voltamperes.

## Therefore:

For a purely resistive circuit:

$$
\begin{aligned}
\theta & =0^{\circ} \\
p f & =1
\end{aligned}
$$

For a resonant circuit:

$$
\begin{aligned}
\theta & =0^{\circ} \\
p f & =1
\end{aligned}
$$

For a purely reactive circuit:

$$
\begin{aligned}
\theta & =90^{\circ} \\
p f & =0
\end{aligned}
$$

## POWER

As shown in Fig. 1-43, the following relationships exist:

True power $(E I \cos \theta)$ does work
Apparent power $(E I \sin \theta)$ does no work

Reactive power is measured in vars (volt-amperes-reactive)


Fig. 1-43. Power triangle.

Power is the rate of doing work (kilowatt, watt, erg). A kilowatt is equal to 1000 W . A watt equals $1 \mathrm{~J} / \mathrm{s}$. One joule is equal to the movement of 1 C through a potential difference of 1 V . One coulomb is the quantity of electricity that passes a point in 1 s when the current is 1 A and is equal to the passage of $6.281 \times 10^{18}$ electrons. Energy is equal to work; thus, energy is measured in such units as kilowatt-hours and watthours.

Work is the product of force times the distance through which the force has been applied. For example, a horsepower is equal to 746 W and represents the application of 550 lbf through 1 ft each second (or, raising $33,000 \mathrm{lb}$ a distance of 1 ft in 1 min ).

Potential energy is energy of position, as when a weight has been raised above ground level. Kinetic energy is the energy of motion, as when a weight falls to the ground. Voltage is basically a unit of work per unit charge; it is basically potential energy.

Generally, we speak of potential difference instead of potential-energy difference. When a potential difference is applied across a load resistor, potential energy is transformed into heat energy. Energy is transformed only when the power factor is unity; if the power factor is zero, potential energy merely surges back and forth and does no real work, as when an AC voltage is applied across an ideal capacitor.

Electromotive force (emf) is source voltage and is measured in volts. The term "electromotive force" is somewhat of a misnomer inasmuch as voltage and, consequently, emf are potential energy.

## TIME CONSTANTS

A certain amount of time is required after a DC voltage has been applied to an $R C$ or $R L$ circuit and before the capacitor can charge or the current can build up to a portion of the full value. This time is called the time constant of the circuit. However, the time constant is not the time required for the voltage or current to reach the full value; instead, it is the time required to reach $63.2 \%$ of full value. During the next time constant, the capacitor is charged or the current builds up to $63.2 \%$ of the remaining difference, which is $86.5 \%$ of the full value. Table $1-2$ gives the percent of full charge on a capacitor (or current buildup in an inductance

TABLE 1-2
Time Constants Versus Percent of Voltage or Current

| No. of <br> time constants | Percent charge <br> or buildup | Percent discharge <br> or decay |
| :---: | :---: | :---: |
| 1 | 63.2 | 36.8 |
| 2 | 86.5 | 13.5 |
| 3 | 95.0 | 5.0 |
| 4 | 98.2 | 1.8 |
| 5 | 99.3 | 0.7 |

after each time constant). Theoretically, neither the charge on the capacitor nor the current through the coil can ever reach $100 \%$. However, it is usually considered to be $100 \%$ after five time constants.

Likewise, when the voltage source is removed, the capacitor will discharge or the current will decay $63.2 \%$, which is $36.8 \%$ of full value during the first time constant. Table 1-2 also gives the percent of full voltage after each time constant for discharge of a capacitor or decay of the current through a coil.

The time per time constant is calculated as follows.

For an $R C$ circuit (Fig. 1-44):

$$
T=R C
$$



Fig. 1-44
For an $R L$ circuit (Fig. 1-45):

$$
T=\frac{L}{R}
$$

where
$T$ is the time, in seconds,
$R$ is the resistance, in ohms, $C$ is the capacitance, in farads, $L$ is the inductance, in henrys.


Fig. 1-45

In addition, the values can also be expressed by the following relationships:

| $T$ | $R$ | Cor $L$ |
| :--- | :--- | :--- |
| seconds | megohms | microfarads |
| seconds | megohms | microhenrys |
| microseconds | ohms | microfarads |
| microseconds | megohms | picofarads |
| microseconds | ohms | microhenrys |

TABLE 1-3
Dimensional Units of Mechanical Quantities

| Symbol | Physical unit | Dimensional unit |
| :---: | :--- | :--- |
| $F$ | force | $F$ |
| $L$ | length | $L$ |
| $t$ | time | $T$ |
| $M$ | mass | $F T L^{-1}$ |
| $W$ | energy, work | $F L$ |
| $p$ | power | $F L T^{-1}$ |
| $v$ | velocity | $L T^{-1}$ |
| $a$ | acceleration | $L T^{-2}$ |

TABLE 1-4
Dimensional Units of Electrical Quantities

| Symbol | Physical unit | Dimensional unit |
| :---: | :--- | :--- |
| $Q$ | charge | $Q$ |
| $I$ | current | $Q T^{-1}$ |
| $V$ | voltage | $F L Q^{-1}$ |
| $R$ | resistance | $F L T Q^{-2}$ |
| $L$ | inductance | $F L T^{2} Q^{-2}$ |
| $C$ | capacitance | $F-L^{-1} Q^{2}$ |
| $X L$ | inductive | $j F L T Q^{-2}$ |
| $X C$ | reactance <br> capacitive <br> reactance | $-j F L T Q^{-2}$ |

Dimensional units show why the product of capacitance and resistance is equal to time. In other words, $F^{-1} L^{-1} Q^{2}$ multiplied by $F L T Q^{-2}$ is equal to $T$. Dimensional units for mechanical and electrical units are listed in Tables 1-3 and 1-4.

Dimensional units are used extensively in calculating with formulas and in analyz-
ing circuit action. As a basic example, dimensional units provide a quick check concerning whether an algebraic error has been made. In other words, no matter how the terms in a formula may be transposed or substituted back and forth, the dimensional units must always be the same on either side of the equals sign. A dimensional check of a derived electrical formula is comparable to a check of an addition problem by first adding the columns up and then adding the columns down.

Example. If we write $I=E / R$, then $Q T^{-1}=F L Q^{-1 /}$ $F L T Q^{-2}=Q T^{-1}$. Again, if we write $P=E I=$ $E^{2} / R$, then $F L T^{-1}=F L Q^{-1} Q T^{-1}=F^{2} L^{2} Q^{-2 /}$ $F L T Q^{-2}=F L T^{-1}$.

Formulas are customarily simplified insofar as possible. In turn, the terms of a formula and the answer that is obtained may require interpretation. For example, an ideal coaxial cable has a certain capacitance per unit length and a certain inductance per unit length. In turn, the formula $R_{0}=\sqrt{L / C}$ is used to calculate the characteristic resistance of the cable. This formula provides a resistance in ohms, when $L$ is in henrys and $C$ is in farads. However, the characteristic resistance $R_{0}$ is a representational resistance and not a simple physical resistance. A representational resistance dissipates no power, whereas a simple physical resistance dissipates power.

Resistance has the dimensions $F L T Q^{-2}$, inductance has the dimensions $F L T^{2} Q^{-2}$, capacitance has the dimensions $F^{-1} L^{-1} Q^{2}$. Accordingly, $R_{0}=\sqrt{\left(F L T^{2} Q^{-2}\right) /\left(F^{-1} L^{-1} Q^{2}\right)}$ or $R_{0}=\sqrt{F^{2} L^{2} T^{2} Q^{-4}}$, so that $R_{0}=F L T Q^{-2}$. Thus, the resistance term is dimensionally correct, and the correct numerical value will be obtained for $R_{0}$ when the square root is taken of the $L / C$ ratio. On the other hand, the $R_{0}$ value cannot be assumed to be a sim-
ple physical resistance; it is a representational resistance (since it cannot dissipate power).

The foregoing interpretation is based on the circumstance that the $L / C$ ratio has the dimensions $F^{2} L^{2} T^{2} Q^{-4}$, which are the dimensions of $R^{2}$. It is a fundamental principle of circuit action that whenever two electrical units are multiplied or divided (or squared or rooted), a new electrical unit is obtained. In this practical example, the new electrical unit of representational resistance is obtained. As previously noted, the circuit action of representational resistance is not the same as the circuit action of simple physical resistance, although some of its aspects are similar.

This and related principles of circuit action are summarized by the basic principle that although $Y=2 X=\sqrt{4 X^{2}}$ is a mathematically correct series of relations, each term has a particular interpretation insofar as circuit action is concerned.

## TRANSFORMER FORMULAS

In a transformer, the relationships between the number of turns in the primary and secondary, the voltage across each winding, and the current through the windings are expressed by the following equations:

$$
\frac{E_{\mathrm{p}}}{E_{\mathrm{c}}}=\frac{N_{\mathrm{r}}}{N}
$$

and

$$
\frac{E_{\mathrm{p}}}{E_{5}}=\frac{I_{\mathrm{s}}}{I_{\mathrm{r}}}
$$

By rearranging these equations and by referring to Fig. 1-46, any unknown can be determined from the following formulas:

$$
\begin{aligned}
& E_{\mathrm{r}}=\frac{E N_{\mathrm{p}}}{N_{\mathrm{n}}}=\frac{E_{\mathrm{I}}}{I_{\mathrm{v}}} \\
& E_{\curlyvee}=\frac{E_{\mathrm{p}} N_{\curlyvee}}{N_{v}}=\frac{E_{\mathrm{p}} I_{\mathrm{p}}}{I_{.}} \\
& N_{\mathrm{n}}=\frac{E_{\mathrm{n}} N_{\mathrm{n}}}{E_{-}}=\frac{N_{\mathrm{I}} I_{\mathrm{s}}}{I_{\mathrm{p}}} . \\
& N_{\checkmark}=\frac{E_{N_{n}} N_{\mathrm{r}}}{E_{\mathrm{r}}}=\frac{N_{\mathrm{r}} I_{\mathrm{r}}}{I_{.}} \\
& I_{\mathrm{n}}=\frac{E_{I_{\mathrm{n}}}}{E_{\mathrm{r}}}=\frac{N I_{\mathrm{n}}}{N_{\mathrm{v}}} \\
& I_{s}=\frac{E_{\mathrm{r}} I_{\mathrm{p}}}{E_{\mathrm{v}}}=\frac{N_{\mathrm{p}} I_{\mathrm{p}}}{N_{\mathrm{v}}}
\end{aligned}
$$

Fig. 1-46
The turns ratio of a transformer is determined by the following formulas:

For a step-up transformer:

$$
T=\frac{N_{v}}{N_{v}}
$$

For a step-down transformer:

$$
T=\frac{N_{\mathrm{r}}}{N}
$$

The impedance ratio of a transformer is determined by:

$$
Z=T^{2}
$$

The impedance of an unknown winding is determined by the following:

For a step-up transformer:

$$
\begin{aligned}
Z_{\mathrm{p}} & =\frac{Z}{Z} \\
Z_{\mathrm{s}} & =Z \times Z_{\mathrm{r}}
\end{aligned}
$$

For a step-down transformer:

$$
\begin{aligned}
Z_{\mathrm{p}} & =Z \times Z_{\mathrm{s}} \\
Z_{\mathrm{s}} & =\frac{Z_{\mathrm{p}}}{Z}
\end{aligned}
$$

where
$E_{\mathrm{r}}$ is the voltage across the primary winding, in volts,
$E \downarrow$ is the voltage across the secondary winding, in volts,
$N_{\mathrm{p}}$ is the number of turns in the primary winding,
$N_{s}$ is the number of turns in the secondary winding,
$I_{\mathrm{p}}$ is the current through the primary winding, in amperes,
$I_{s}$ is the current through the secondary winding, in amperes,
$T$ is the turns ratio,
$Z$ is the impedance ratio,
$Z_{v}$ is the impedance of the primary winding, in ohms,
$Z_{\checkmark}$ is the impedance of the secondary winding, in ohms.

## VOLTAGE REGULATION

When a load is connected to a power supply, the output voltage drops because more current flows through the resistive ele-
ments of the power supply. Voltage regulation is a measure of how much the voltage drops and is usually expressed as a percentage. It is determined by the following formula:

$$
\% R=\frac{E_{1}-E_{2}}{E_{2}} \times 100
$$

where
$\% R$ is the voltage regulation, in percent,
$E_{1}$ is the no-load voltage, in volts, $E_{2}$ is the voltage under load, in volts.

## DC-METER FORMULAS

The basic instrument for testing current and voltage is the moving-coil meter. The meter can be either a DC milliammeter or a DC microammeter. A series resistor converts the meter to a DC voltmeter, and a parallel resistor converts the meter to a DC ammeter. The resistance of the meter movement is determined first, as follows. Connects a suitable variable resistor $R_{\mathrm{a}}$ and a battery as shown in Fig. 1-47. Adjust resistor $R_{\mathrm{a}}$ until full-scale deflection is obtained. Then connect a variable resistor $R_{\mathrm{b}}$ in parallel with the meter, and adjust $R_{\mathrm{b}}$ until halfscale deflection is obtained. Disconnect $R_{\mathrm{b}}$ and measure its resistance. The measured value is the resistance of the meter movement.


Fig. 1-47

## Voltage Multipliers (Fig. 1-48)

$$
R=\frac{E_{\mathrm{s}}}{I_{\mathrm{s}}}-R_{\mathrm{m}}
$$



Fig. 1-48
where
$R$ is the multiplier resistance, in ohms, $E_{\mathrm{s}}$ is the full-scale reading, in volts, $I_{s}$ is the full-scale reading, in amperes, $R_{\mathrm{m}}$ is the meter resistance, in ohms.

## Shunt-Type Ohmmeter for Low

 Resistance (Fig. 1-49)$$
R_{x}=R_{\mathrm{m}} \frac{I_{2}}{I_{1}-I_{2}}
$$

Fig. 1-49
where
$R_{\mathrm{x}}$ is the unknown resistance, in ohms, $R_{\mathrm{m}}$ is the meter resistance, in ohms, $I_{1}$ is the current reading with probes open, in amperes,
$I_{2}$ is the current reading with probes connected across unknown resistor, in amperes.
$R_{1}$ in Fig. 1-49 is a variable resistance for current limiting to keep meter adjusted for full-scale reading with probes open.

## Series-Type Ohmmeter for High Resistance (Fig. 1-50)

$$
R_{x}=\left(R_{1}+R_{\mathrm{m}}\right) \frac{I_{1}-I_{2}}{I_{2}}
$$

where
$R_{\mathrm{x}}$ is the unknown resistance, in ohms, $R_{1}$ is a variable resistance adjusted for full-scale reading with probes shorted together, in ohms,
$R_{\mathrm{m}}$ is the meter resistance, in ohms,
$I_{1}$ is the current reading with probes shorted, in amperes,
$I_{2}$ is the current reading with unknown resistor connected, in amperes.


Fig. 1-50

Ammeter Shunts (Fig. 1-51)

$$
R=\frac{R_{\mathrm{m}}}{N-1}=\frac{I_{\mathrm{m}} R_{\mathrm{m}}}{I_{\mathrm{s}}}
$$

where
$R$ is the resistance of the shunt, in ohms,
$R_{\mathrm{m}}$ is the meter resistance, in ohms,
$N$ is the scale multiplication factor, $I_{\mathrm{m}}$ is the meter current, in amperes, $I_{s}$ is the shunt current, in amperes.


Fig. 1-51

## Ammeter With Multirange Shunt

 (Fig. 1-52)$$
R_{2}=\frac{\left(R_{1}+R_{2}\right)+R_{\mathrm{m}}}{N}
$$

where
$R_{2}$ is the intermediate value, in ohms,
$R_{1}+R_{2}$ is the total shunt resistance for lowest full-scale reading, in ohms, $R_{\mathrm{m}}$ is the meter resistance, in ohms,
$N$ is the scale multiplication factor.


Fig. 1-52

## FREQUENCY AND <br> WAVELENGTH

## Formulas

Since frequency is defined as the number of complete hertz and since all radio waves travel at a constant speed, it follows that a complete cycle occupies a given distance in space. The distance between two corresponding parts of two waves (the two positive or negative crests or the points
where the two waves cross the zero axis in a given direction) constitutes the wavelength. If either the frequency or the wavelength is known, the other can be computed as follows:

$$
\begin{aligned}
& f=\frac{300,000}{\lambda} \\
& \lambda=\frac{300,000}{f}
\end{aligned}
$$

where
$f$ is the frequency, in kilohertz, $\lambda$ is the wavelength, in meters.

To calculate wavelength in feet, the following formulas should be used:

$$
\begin{aligned}
& f=\frac{984,000}{\lambda} \\
& \lambda=\frac{984,000}{f}
\end{aligned}
$$

where
$f$ is the frequency, in kilohertz, $\lambda$ is the wavelength, in feet.

The preceding formula can be used to determine the length of a single-wire antenna.

For a half-wave antenna:

$$
L=\frac{492}{f}
$$

For a quarter-wave antenna:

$$
L=\frac{246}{f}
$$



Fig. 1-53. Frequency-wavelength conversion chart.
where
$L$ is the length of the antenna, in feet, $f$ is the frequency, in megahertz.

## Conversion Chart

The wavelength of any frequency from 30 kHz to 3000 MHz can be read directly from the chart in Fig. 1-53. Also, if the wavelength is known, the corresponding frequency can be obtained from the chart for wavelengths from 10 cm to 1000 m . To use the chart, merely find the known value (either frequency or wavelength) on one of the scales, and then read the corresponding value from the opposite side of the scale.

Example. What is the wavelength of a $4-\mathrm{MHz}$ signal?

Answer. $\quad 75 \mathrm{~m}$. (Find 4 MHz on the third scale from the left. Opposite 4 MHz on the frequency scale find 75 m on the wavelength scale.)

## TRANSMISSION-LINE FORMULAS

The characteristic impedance of a transmission line is defined as the input impedance of a line of the same configuration and dimensions but of infinite length. When a line of finite length is terminated with an impedance equal to its own characteristic impedance, the line is said to be matched.

## Coaxial Line

The characteristic impedance of a coaxial line (Fig. 1-54) is given by:

$$
Z_{0}=\frac{138}{\sqrt{k}} \log \frac{D}{d}
$$

where
$Z_{0}$ is the characteristic impedance, in ohms,
$D$ is the inside diameter of the outer conductor, in inches, $d$ is the outside diameter of the inner conductor, in inches, $k$ is the dielectric constant of the insulating material* ( $k$ equals 1 for dry air).


Fig. 1-54
The attenuation of a coaxial line in decibels per foot can be determined by the formula:

$$
a=\frac{4.6 \sqrt{f}(D+d)}{D \times d\left(\log \frac{D}{d}\right)} \times 10
$$

where
$a$ is the attenuation, in decibels per foot of line,
$f$ is the frequency, in megahertz, $D$ is the inside diameter of the outer conductor, in inches, $d$ is the outside diameter of the inner conductor, in inches.

## Parallel-Conductor Line

The characteristic impedance of paral-lel-conductor line (twin-lead) as shown in Fig. 1-55 is determined by the formula:

$$
Z_{0}=\frac{276}{\sqrt{k}} \log \frac{2 D}{d}
$$

where
$Z_{0}$ is the characteristic impedance, in ohms,
$D$ is the center-to-center distance between conductors, in inches, $d$ is the diameter of the conductors, in inches,
$k$ is the diclectric constant of the insulating material between conductors* ( $k$ equals 1 for dry air).


Fig. 1-55

## MODULATION FORMULAS

## Amplitude Modulation

The amount of modulation of an ampli-tude-modulated carrier shown in Fig. 1-56 is referred to as the percentage of modulation. It can be determined by the following formulas:

$$
\% M=\frac{E_{\mathrm{c}}-E_{1}}{2 E_{\mathrm{ar}}} \times 100
$$

or

$$
\% M=\frac{E_{\mathrm{C}}-E_{\mathrm{T}}}{E_{\mathrm{T}}+E_{\mathrm{T}}} \times 100
$$

where
$\% M$ is the percentage of modulation, $E_{\mathrm{C}}$ is the amplitude of the crest of the modulated carrier,

[^1]$E_{\mathrm{T}}$ is the amplitude of the trough of the modulated carrier,
$E_{\mathrm{av}}$ is the average amplitude of the modulated carrier.


Fig. 1-56
Also, the percentage of modulation can be determined by applying the modulated carrier wave to the vertical plates and the modulating voltage wave to the horizontal plates of an oscilloscope. This produces a trapezoidal wave, as shown in Fig. 1-57. The dimensions $A$ and $B$ are proportional to the crest and trough amplitudes, respectively. The percentage of modulation can be determined by measuring the height of $A$ and $B$ and using the formula:

$$
\% M=\frac{A-B}{A+B} \times 100
$$

where
$\% M$ is the percentage of modulation, $A$ and $B$ are the dimensions measured in Fig. 1-57.


Fig. 1-57
The sideband power of an amplitudemodulated carrier is determined by:

$$
P_{\mathrm{SB}}=\frac{\% M^{2}}{2} \times P_{\mathrm{C}}
$$

The total radiated power is the sum of the carrier and the radiated powers:

$$
P_{\mathrm{T}}=P_{\mathrm{sB}}+P_{\mathrm{r}}
$$

where
$P_{\mathrm{sB}}$ is the sideband power (includes both sidebands), in watts,
$\% M$ is the percentage of modulation, $P_{\mathrm{C}}$ is the carrier power, in watts, $P_{\mathrm{T}}$ is the total radiated power, in watts.

Note. The carrier power does not change with modulation.

## Frequency Modulation

In a frequency-modulated carrier, the amount the carrier frequency changes is determined by the amplitude of the modulating signal, and the number of times the changes occur per second is determined by the frequency of the modulating signal.

The percentage of modulation of a fre-quency-modulated carrier can be computed from:

$$
\% M=\frac{\Delta f}{\Delta f \text { for } 100 \% M} \times 100
$$

where
$\% M$ is the percentage of modulation,
$\Delta f$ is the change in frequency (or the deviation),
$\Delta f$ for $100 \% M$ is the change in frequency for a $100 \%$ modulated carrier. (For commercial fm, 75 kHz ; for television sound, 25 kHz ; for twoway radio, 15 kHz .)

The modulation index of a frequencymodulated carrier is determined by:

$$
M=\frac{f_{\mathrm{d}}}{f_{\mathrm{a}}}
$$

where
$M$ is the modulation index, $f_{\mathrm{d}}$ is the deviation in frequency, in hertz,
$f_{\mathrm{a}}$ is the modulating audio frequency, in the same units as $f_{\mathrm{u}}$.

## DECIBELS AND VOLUME UNITS

## Equations

The number of decibels corresponding to a given power ratio is 10 times the common logarithm of the ratio. Thus:

$$
\mathrm{dB}=10 \log \frac{P_{2}}{P_{1}}
$$

where
$P_{1}$ and $P_{2}$ are the individual power readings, in watts.

The number of decibels corresponding to a given voltage or current ratio is 20 times the common logarithm of the ratio. Thus, when the impedances across which the signals are being measured are equal, the equations are:

$$
\begin{aligned}
& \mathrm{dB}=20 \log \frac{E_{2}}{E_{1}} \\
& \mathrm{~dB}=20 \log \frac{I_{2}}{I_{1}}
\end{aligned}
$$

where
$E_{1}$ and $E_{2}$ are the individual voltage readings, in volts,
$I_{1}$ and $I_{2}$ are the individual current readings, in amperes.

If the impedances across which the sig-
nals are measured are not equal, the equations become:

$$
\begin{aligned}
& \mathrm{dB}=20 \log \frac{E_{2} \sqrt{Z_{1}}}{E_{1} \sqrt{Z_{2}}} \\
& \mathrm{~dB}=20 \log \frac{I_{2} \sqrt{Z_{2}}}{I_{1} \sqrt{Z_{1}}}
\end{aligned}
$$

where
$E_{1}$ and $E_{2}$ are the individual voltage readings, in volts,
$I_{1}$ and $I_{2}$ are the individual current readings, in amperes,
$Z_{1}$ and $Z_{2}$ are the individual impedances across which the signals were read, in ohms.

## Reference Levels

The decibel is not an absolute value; it is a means of stating the ratio of a level to a certain reference level. Usually, when no reference level is given, it is 6 mV across a 500 $\Omega$ impedance. However, the reference level should be stated whenever a value in decibels is given. Other units, which do have specific reference levels, have been established. Some of the more common are:

| dBj | 1 mV |
| :--- | :--- |
| dBk | 1 kW |
| dBm | $\mathrm{mW}, 600 \Omega$ |
| dBs | Japanese designation for dBm <br> system |
| dBv | 1 V (no longer in use) |
| dBw | 1 W |
| dBvg | voltage gain |
| dBrap | decibels above a reference <br> acoustical power of $10^{-16} \mathrm{~W}$ |

VU $1 \mathrm{~mW}, 600 \Omega$ (complex waveforms varying in both amplitude and frequency)

## Decibel Table

Tables 1-5 and 1-6 are decibel tables that list most of the power, current, and voltage ratios commonly encountered, with their decibel values. Figure $1-58$ shows the relationship between power and voltage or current. If a decibel value is not listed in Tables $1-5$ and 1-6, first subtract one of the given values from the unlisted value (select a value so the remainder will also be listed). Then multiply the ratios given in the chart for each value. To covert a ratio not given in the tables to a decibel value, first factor the ratio so that each factor will be a listed value; then find the decibel equivalents for each factor and add them.

TABLE 1-5
Decibel Table (0-1.9 dB)*

|  |  |  | Current or <br> voltage ratio |  |
| :--- | :--- | :--- | :--- | :--- |
| dB | Gain | Loss | Gain | Loss |
| 0 | 1.000 | 1.0000 | 1.000 | 1.0000 |
| 0.1 | 1.023 | 0.9772 | 1.012 | 0.9886 |
| 0.2 | 1.047 | 0.9550 | 1.023 | 0.9772 |
| 0.3 | 1.072 | 0.9333 | 1.035 | 0.9661 |
| 0.4 | 1.096 | 0.9120 | 1.047 | 0.9550 |
| 0.5 | 1.122 | 0.8913 | 1.059 | 0.9441 |
| 0.6 | 1.148 | 0.8710 | 1.072 | 0.9333 |
| 0.7 | 1.175 | 0.8511 | 1.084 | 0.9226 |
| 0.8 | 1.202 | 0.8318 | 1.096 | 0.9120 |
| 0.9 | 1.230 | 0.8128 | 1.109 | 0.9016 |
|  |  |  |  |  |
| 1.0 | 1.259 | 0.7943 | 1.122 | 0.8913 |
| 1.1 | 1.288 | 0.7762 | 1.135 | 0.8810 |
| 1.2 | 1.318 | 0.7586 | 1.148 | 0.8710 |
| 1.3 | 1.349 | 0.7413 | 1.161 | 0.8610 |
| 1.4 | 1.380 | 0.7244 | 1.175 | 0.8511 |
| 1.5 | 1.413 | 0.7079 | 1.189 | 0.8414 |
| 1.6 | 1.445 | 0.6918 | 1.202 | 0.8318 |
| 1.7 | 1.479 | 0.6761 | 1.216 | 0.8222 |
| 1.8 | 1.514 | 0.6607 | 1.230 | 0.8128 |
| 1.9 | 1.549 | 0.6457 | 1.245 | 0.8035 |

TABLE 1-5 Cont.
Decibel Table (2.0-10.9)

| dB | Power ratio |  | Current or voltage ratio |  | dB | Power ratio |  | Current or voltage ratio |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Gain | loss | Gain | Loss |  | Gain | Loss | Gain | Ioss |
| 2.0 | 1.585 | 0.6310 | 1.259 | 0.7943 | 6.5 | 4.467 | 0.2239 | 2.113 | 0.4732 |
| 2.1 | 1.622 | 0.6166 | 1.274 | 0.7852 | 6.6 | 4.571 | 0.2188 | 2.138 | 0.4677 |
| 2.2 | 1.660 | 0.6026 | 1.288 | 0.7762 | 6.7 | 4.677 | 0.2138 | 2.163 | 0.4624 |
| 2.3 | 1.698 | 0.5888 | 1.303 | 0.7674 | 6.8 | 4.786 | 0.2089 | 2.188 | 0.4571 |
| 2.4 | 1.738 | 0.5754 | 1.318 | 0.7586 | 6.9 | 4.898 | 0.2042 | 2.213 | 0.4519 |
| 2.5 | 1.778 | 0.5623 | 1.334 | 0.7499 |  |  |  |  |  |
| 2.6 | 1.820 | 0.5495 | 1.349 | 0.7413 | 7.0 | 5.012 | 0.1995 | 2.239 | 0.4467 |
| 2.7 | 1.862 | 0.5370 | 1.365 | 0.7328 | 7.1 | 5.129 | 0.1950 | 2.265 | 0.4416 |
| 2.8 | 1.905 | 0.5248 | 1.380 | 0.7244 | 7.2 | 5.248 | 0.1905 | 2.291 | 0.4365 |
| 2.9 | 1.950 | 0.5129 | 1.396 | 0.7161 | 7.3 | 5.370 | 0.1862 | 2.317 | 0.4315 |
|  |  |  |  |  | 7.4 | 5.495 | 0.1820 | 2.344 | 0.4266 |
| 3.0 | 1.995 | 0.5012 | 1.413 | 0.7079 | 7.5 | 5.623 | 0.1778 | 2.371 | 0.4217 |
| 3.1 | 2.042 | 0.4898 | 1.429 | 0.6998 | 7.6 | 5.754 | 0.1738 | 2.399 | 0.4169 |
| 3.2 | 2.089 | 0.4786 | 1.445 | 0.6918 | 7.7 | 5.888 | 0.1698 | 2.427 | 0.4121 |
| 3.3 | 2.138 | 0.4677 | 1.462 | 0.6839 | 7.8 | 6.026 | 0.1660 | 2.455 | 0.4074 |
| 3.4 | 2.188 | 0.4571 | 1.479 | 0.6761 | 7.9 | 6.166 | 0.1622 | 2.483 | 0.4027 |
| 3.5 | 2.239 | 0.4467 | 1.496 | 0.6683 |  |  |  |  |  |
| 3.6 | 2.291 | 0.4365 | 1.514 | 0.6607 | 8.0 | 6.310 | 0.1585 | 2.512 | 0.3981 |
| 3.7 | 2.344 | 0.4266 | 1.531 | 0.6531 | 8.1 | 6.457 | 0.1549 | 2.541 | 0.3936 |
| 3.8 | 2.399 | 0.4169 | 1.549 | 0.6457 | 8.2 | 6.607 | 0.1514 | 2.570 | 0.3890 |
| 3.9 | 2.455 | 0.4074 | 1.567 | 0.6383 | 8.3 | 6.761 | 0.1479 | 2.600 | 0.3846 |
|  |  |  |  |  | 8.4 | 6.918 | 0.1445 | 2.630 | 0.3802 |
| 4.0 | 2.512 | 0.3981 | 1.585 | 0.6310 | 8.5 | 7.079 | 0.1413 | 2.661 | 0.3758 |
| 4.1 | 2.570 | 0.3890 | 1.603 | 0.6237 | 8.6 | 7.244 | 0.1380 | 2.692 | 0.3715 |
| 4.2 | 2.630 | 0.3802 | 1.622 | 0.6166 | 8.7 | 7.413 | 0.1349 | 2.723 | 0.3673 |
| 4.3 | 2.692 | 0.3715 | 1.641 | 0.6095 | 8.8 | 7.586 | 0.1318 | 2.754 | 0.3631 |
| 4.4 | 2.754 | 0.3631 | 1.660 | 0.6026 | 8.9 | 7.762 | 0.1288 | 2.786 | 0.3589 |
| 4.5 | 2.818 | 0.3548 | 1.679 | 0.5957 |  |  |  |  |  |
| 4.6 | 2.884 | 0.3467 | 1.698 | 0.5888 | 9.0 | 7.943 | 0.1259 | 2.818 | 0.3548 |
| 4.7 | 2.951 | 0.3388 | 1.718 | 0.5821 | 9.1 | 8.128 | 0.1230 | 2.851 | 0.3508 |
| 4.8 | 3.020 | 0.3311 | 1.738 | 0.5754 | 9.2 | 8.318 | 0.1202 | 2.884 | 0.3467 |
| 4.9 | 3.090 | 0.3236 | 1.758 | 0.5689 | 9.3 | 8.511 | 0.1175 | 2.917 | 0.3428 |
|  |  |  |  |  | 9.4 | 8.710 | 0.1148 | 2.951 | 0.3388 |
| 5.0 | 3.162 | 0.3162 | 1.778 | 0.5623 | 9.5 | 8.913 | 0.1122 | 2.985 | 0.3350 |
| 5.1 | 3.236 | 0.3090 | 1.799 | 0.5559 | 9.6 | 9.120 | 0.1096 | 3.020 | 0.3311 |
| 5.2 | 3.311 | 0.3020 | 1.820 | 0.5495 | 9.7 | 9.333 | 0.1072 | 3.055 | . 3273 |
| 5.3 | 3.388 | 0.2951 | 1.841 | 0.5433 | 9.8 | 9.550 | 0.1047 | 3.090 | U. 3236 |
| 5.4 | 3.467 | 0.2884 | 1.862 | 0.5370 | 9.9 | 9.772 | 0.1023 | 3.126 | 0.3199 |
| 5.5 | 3.548 | 0.2818 | 1.884 | 0.5309 |  |  |  |  |  |
| 5.6 | 3.631 | 0.2754 | 1.905 | 0.5248 | 10.0 | 10.000 | 0.1000 | 3.162 | 0.3162 |
| 5.7 | 3.715 | 0.2692 | 1.928 | 0.5188 | 10.1 | 10.23 | 0.09772 | 3.199 | 0.3126 |
| 5.8 | 3.802 | 0.2630 | 1.950 | 0.5129 | 10.2 | 10.47 | 0.09550 | 3.236 | 0.3090 |
| 5.9 | 3.890 | 0.2570 | 1.972 | 0.5070 | 10.3 | 10.72 | 0.09333 | 3.273 | 0.3055 |
|  |  |  |  |  | 10.4 | 10.96 | 0.09120 | 3.311 | 0.3020 |
| 6.0 | 3.981 | 0.2512 | 1.995 | 0.5012 | 10.5 | 11.22 | 0.08913 | 3.350 | 0.2985 |
| 6.1 | 4.074 | 0.2455 | 2.018 | 0.4955 | 10.6 | 11.48 | 0.08710 | 3.388 | 0.2951 |
| 6.2 | 4.169 | 0.2399 | 2.042 | 0.4898 | 10.7 | 11.75 | 0.08511 | 3.428 | 0.2917 |
| 6.3 | 4.266 | 0.2344 | 2.065 | 0.4842 | 10.8 | 12.02 | 0.08318 | 3.467 | 0.2884 |
| 6.4 | 4.365 | 0.2291 | 2.089 | 0.4786 | 10.9 | 12.30 | 0.08128 | 3.508 | 0.2851 |

Electronics Formulas and Laws

TABLE 1-5 Cont.
Decibel Table (11.0-19.9)

| dB | Power ratio |  | Current or voltage ratio |  | dB | Power ratio |  | Current or voltage ratio |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Gain | Loss | Gain | Loss |  | Gain | Ioss | Gain | Loss |
| 11.0 | 12.59 | 0.07943 | 3.548 | 0.2818 | 15.5 | 35.48 | 0.02818 | 5.957 | 0.1679 |
| 11.1 | 12.88 | 0.07762 | 3.589 | 0.2786 | 15.6 | 36.31 | 0.02754 | 6.026 | 0.1660 |
| 11.2 | 13.18 | 0.07586 | 3.631 | 0.2754 | 15.7 | 37.15 | 0.02692 | 6.095 | 0.1641 |
| 11.3 | 13.49 | 0.07413 | 3.673 | 0.2723 | 15.8 | 38.02 | 0.02630 | 6.166 | 0.1622 |
| 11.4 | 13.80 | 0.07244 | 3.715 | 0.2692 | 15.9 | 38.90 | 0.02570 | 6.237 | 0.1603 |
| 11.5 | 14.13 | 0.07079 | 3.758 | 0.2661 |  |  |  |  |  |
| 11.6 | 14.45 | 0.06918 | 3.802 | 0.2630 | 16.0 | 39.81 | 0.02512 | 6.310 | 0.1585 |
| 11.7 | 14.79 | 0.06761 | 3.846 | 0.2600 | 16.1 | 40.74 | 0.02455 | 6.383 | 0.1567 |
| 11.8 | 15.14 | 0.06607 | 3.890 | 0.2570 | 16.2 | 41.69 | 0.02399 | 6.457 | 0.1549 |
| 11.9 | 15.49 | 0.06457 | 3.936 | 0.2541 | 16.3 | 42.66 | 0.02344 | 6.531 | 0.1531 |
|  |  |  |  |  | 16.4 | 43.65 | 0.02291 | 6.607 | 0.1514 |
| 12.0 | 15.85 | 0.06310 | 3.981 | 0.2512 | 16.5 | 44.67 | 0.02239 | 6.683 | 0.1496 |
| 12.1 | 16.22 | 0.06166 | 4.027 | 0.2483 | 16.6 | 45.71 | 0.02188 | 6.761 | 0.1479 |
| 12.2 | 16.60 | 0.06026 | 4.074 | 0.2455 | 16.7 | 46.77 | 0.02138 | 6.839 | 0.1462 |
| 12.3 | 16.98 | 0.05888 | 4.121 | 0.2427 | 16.8 | 47.86 | 0.02089 | 6.918 | 0.1445 |
| 12.4 | 17.38 | 0.05754 | 4.169 | 0.2399 | 16.9 | 48.98 | 0.02042 | 6.998 | 0.1429 |
| 12.5 | 17.78 | 0.05623 | 4.217 | 0.2371 |  |  |  |  |  |
| 12.6 | 18.20 | 0.05495 | 4.266 | 0.2344 | 17.0 | 50.12 | 0.01995 | 7.079 | 0.1413 |
| 12.7 | 18.62 | 0.05370 | 4.315 | 0.2317 | 17.1 | 51.29 | 0.01950 | 7.161 | 0.1396 |
| 12.8 | 19.05 | 0.05248 | 4.365 | 0.2291 | 17.2 | 52.48 | 0.01905 | 7.244 | 0.1380 |
| 12.9 | 19.50 | 0.05129 | 4.416 | 0.2265 | 17.3 | 53.70 | 0.01862 | 7.328 | 0.1365 |
|  |  |  |  |  | 17.4 | 54.95 | 0.01820 | 7.413 | 0.1349 |
| 13.0 | 19.95 | 0.05012 | 4.467 | 0.2239 | 17.5 | 56.23 | 0.01778 | 7.499 | 0.1334 |
| 13.1 | 20.42 | 0.04898 | 4.519 | 0.2213 | 17.6 | 57.54 | 0.01738 | 7.586 | 0.1318 |
| 13.2 | 20.89 | 0.04786 | 4.571 | 0.2188 | 17.7 | 58.88 | 0.01698 | 7.674 | 0.1303 |
| 13.3 | 21.38 | 0.04677 | 4.624 | 0.2163 | 17.8 | 60.26 | 0.01660 | 7.762 | 0.1288 |
| 13.4 | 21.88 | 0.04571 | 4.677 | 0.2138 | 17.9 | 61.66 | 0.01622 | 7.852 | 0.1274 |
| 13.5 | 22.39 | 0.04467 | 4.732 | 0.2113 |  |  |  |  |  |
| 13.6 | 22.91 | 0.04365 | 4.786 | 0.2089 | 18.0 | 63.10 | 0.01585 | 7.943 | 0.1259 |
| 13.7 | 23.44 | 0.04266 | 4.842 | 0.2065 | 18.1 | 64.57 | 0.01549 | 8.035 | 0.1245 |
| 13.8 | 23.99 | 0.04169 | 4.898 | 0.2042 | 18.2 | 66.07 | 0.01514 | 8.128 | 0.1230 |
| 13.9 | 24.55 | 0.04074 | 4.955 | 0.2018 | 18.3 | 67.61 | 0.01479 | 8.222 | 0.1216 |
|  |  |  |  |  | 18.4 | 69.18 | 0.01445 | 8.318 | 0.1202 |
| 14.0 | 25.12 | 0.03981 | 5.012 | 0.1995 | 18.5 | 70.79 | 0.01413 | 8.414 | 0.1189 |
| 14.1 | 25.70 | 0.03890 | 5.070 | 0.1972 | 18.6 | 72.44 | 0.01380 | 8.511 | 0.1175 |
| 14.2 | 26.30 | 0.03802 | 5.129 | 0.1950 | 18.7 | 74.13 | 0.01349 | 8.610 | 0.1161 |
| 14.3 | 26.92 | 0.03715 | 5.188 | 0.1928 | 18.8 | 75.86 | 0.01318 | 8.710 | 0.1148 |
| 14.4 | 27.54 | 0.03631 | 5.248 | 0.1905 | 18.9 | 77.62 | 0.01288 | 8.810 | 0.1135 |
| 14.5 | 28.18 | 0.03548 | 5.309 | 0.1884 |  |  |  |  |  |
| 14.6 | 28.84 | 0.03467 | 5.370 | 0.1862 | 19.0 | 79.43 | 0.01259 | 8.913 | 0.1122 |
| 14.7 | 29.51 | 0.03388 | 5.433 | 0.1841 | 19.1 | 81.28 | 0.01230 | 9.016 | 0.1109 |
| 14.8 | 30.20 | 0.03311 | 5.495 | 0.1820 | 19.2 | 83.18 | 0.01202 | 9.120 | 0.1096 |
| 14.9 | 30.90 | 0.03236 | 5.559 | 0.1799 | 19.3 | 85.11 | 0.01175 | 9.226 | 0.1084 |
|  |  |  |  |  | 19.4 | 87.10 | 0.01148 | 9.333 | 0.1072 |
| 15.0 | 31.62 | 0.03162 | 5.623 | 0.1778 | 19.5 | 89.13 | 0.01122 | 9.441 | 0.1059 |
| 15.1 | 32.36 | 0.03090 | 5.689 | 0.1758 | 19.6 | 91.20 | 0.01096 | 9.550 | 0.1047 |
| 15.2 | 35.11 | 0.03020 | 5.754 | 0.1738 | 19.7 | 93.33 | 0.01072 | 9.661 | 0.1035 |
| 15.3 | 33.88 | 0.02951 | 5.821 | 0.1718 | 19.8 | 95.50 | 0.01047 | 9.772 | 0.1023 |
| 15.4 | 34.67 | 0.02884 | 5.888 | 0.1698 | 19.9 | 97.72 | 0.01023 | 9.886 | 0.1012 |

TABLE 1-6
Decibel Table (20-100 dB)*

|  | Power ratio |  | Current or voltage ratio |  |
| :---: | :---: | :---: | :---: | :---: |
| dB | Gain | loss | Gain | Loss |
| 20 | $10^{2}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point one step to the right. | $10^{-2}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point one step to the left. | $10.00$ <br> Use the same numbers as $0-20 \mathrm{~dB}$, but shift point one step to the right. | $0.1000$ <br> Use the same numbers as $0-20 \mathrm{~dB}$, but shift point one step to the left. |
| 30 | $10^{2}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point one step to the right. | $10^{3}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point one step to the left. |  |  |
| 40 | $10^{4}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point two steps to the right. | $10^{-4}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point two steps to the left. | $100$ <br> Use the same numbers as $0-20 \mathrm{~dB}$, but shift point two steps to the right. | $0.01$ <br> Use the same numbers as $0-20 \mathrm{~dB}$, but shift point two steps to the left. |
| 50 | $10^{〔}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point two steps to the right. | $10^{-5}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point two steps to the left. |  |  |
| 60 | $10^{\kappa}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point three steps to the right. | $10^{-6}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point three steps to the left. | 1000 <br> Use the same numbers as $0-20 \mathrm{~dB}$, but shift point three steps to the right. | $0.001$ <br> Use the same numbers as $0-20 \mathrm{~dB}$, but shift point three steps to the left. |
| 70 | $10^{\circ}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point three steps to the right. | $10^{-7}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point three steps to the left. |  |  |
| 80 | $10^{x}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point four steps to the right. | $10^{-8}$ <br> Use the same numbers as ( $)-10 \mathrm{~dB}$, but shift point four steps to the left. | $10,000$ <br> Use the same numbers as $0-20 \mathrm{~dB}$, but shift point four steps to the right. | $0.0001$ <br> Use the same numbers as $0-20 \mathrm{~dB}$, but shift point four steps to the left. |
| 90 | $10^{\prime \prime}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point four steps to the right. | Use the same numbers as $0-10 \mathrm{~dB}$, but shift point four steps to the left. |  |  |
| 100 | $10^{\prime \prime \prime}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point five steps to the right. | $10^{-111}$ <br> Use the same numbers as $0-10 \mathrm{~dB}$, but shift point five steps to the left. | $100,000$ <br> Use the same numbers as $0-20 \mathrm{~dB}$, but shift point five steps to the right. | $0.00001$ <br> Use the same numbers as $0-20 \mathrm{~dB}$, but shift point five steps to the left. |

## Electronics Formulas and Laws

Example 1. Find the decibel equivalent of a power ratio of 0.631 .

Answer. 2-dB loss.

Example 2. Find the current ratio corresponding to a gain of 43 dB .

Answer. 141. (First, find the current ratio for 40 dB [100]; then find the current ratio for 3 dB [1.41]. Multiply $100 \times 1.41=141$.)

Example 3. Find the decibel value corresponding to a voltage ratio of 150 .

Answer. 43.5 (First, factor 150 into $1.5 \times 100$. The decibel value for a voltage ratio of 100 is 40 ; the decibel value for a voltage ratio of 1.5 is 3.5 [approximately]. Therefore, the decibel value for a voltage ratio is $40+3.5$ or 43.5 dB .)


Fig. 1-58. Decibels and power, voltage, or current ratios.

## Chapter 2

## Constants and Standards

## DIELECTRIC CONSTANTS OF MATERIALS

The dielectric constants of most materials vary for different temperatures and frequencies. Likewise, small differences in the composition of materials cause differences in the dielectric constants. A list of materi-
als and the approximate range (where available) of their dielectric constants is given in Table 2-1. The values shown are accurate enough for most applications. The dielectric constants of some materials (such as quartz, Styrofoam, and Teflon) do not change appreciably with frequency. Figure 2-1 shows the relationship between temperature and change in capacitance.


Fig. 2-1. Capacitance variation versus temperature for typical commercial capacitors.

TABLE 2-1
Dielectric Constants of Materials

| Material | Dielectric <br> constant <br> (approx.) | Material | Dielectric <br> constant <br> (approx.) | Material |
| :--- | :---: | :--- | :--- | :--- |

## METRIC SYSTEM

The international system of units developed by the General Conference on Weights and Measures (abbreviated CGPM), commonly called the metric system, is the basis for a worldwide standardization of units. This International System of Units (abbreviated SI) is divided into three classes-base units, supplementary units, and derived units.

## Units and Symbols

The seven base units and the two supplementary units with their symbols are given in Table 2-2.

Derived units are formed by combining base units, supplementary units, and other derived units. Certain derived units have special names and symbols. These units, along with their symbols and formulas, are given in Table 2-3. Other common derived units and their symbols are given in Table 2-4.

TABLE 2-2
SI Base and Supplementary Units

| Quantity | Unit | Symbol |
| :--- | :--- | :--- |
| length <br> mass <br> time <br> electric current <br> thermodynamic <br> temperature | meter | m |
| amount of substance <br> luminous intensity <br> plane angle | kilogram <br> socond | kg |
| sompere angle | mole | s |

*The degree Celsius is also used for expressing temperature.
'Supplementary units.

TABLE 2-3
SI Derived Units with Special Names

| Quantity | Unit | Symbol | Formula |
| :---: | :---: | :---: | :---: |
| ```frequency (of a periodic phenomenon) hertz Z Hz 1/s``` |  |  |  |
|  |  |  |  |
|  |  |  |  |
| force | newton | N | $\mathrm{kg} \cdot \mathrm{m} / \mathrm{s}^{2}$ |
| pressure, stress | pascal | Pa | $\mathrm{N} / \mathrm{m}^{2}$ |
| energy, work, |  |  |  |
| quantity of heat | joule | J | $\mathrm{N} \cdot \mathrm{m}$ |
| power, radiant flux | watt | W | J/s |
| quantity of electricity, <br> electric charge coulomb C A.s |  |  |  |
| electric potential, potential difference, electromotive |  |  |  |
| force | volt | V | W/A |
| capacitance | farad | F | C/V |
| electric resistance | ohm | $\Omega$ | V/A |
| conductance | siemens | S | A/V |
| magnetic flux | weber | Wb | $\mathrm{V} \cdot \mathrm{s}$ |
| magnetic flux density | tesla | T | $\mathrm{Wb} / \mathrm{m}^{2}$ |
| inductance | henry | H | Wb/A |
| luminous flux | lumen | lm | $\mathrm{cd} \cdot \mathrm{sr}$ |
| illuminance | lux | lx | $\operatorname{lm} / \mathrm{m}^{2}$ |
| activity (of radionuclides) | becquerel | Bq | 1/s |
| absorbed dose | gray | Gy | $\mathrm{J} / \mathrm{kg}$ |

TABLE 2-4
Common SI Derived Units

| Quantity | Unit | Symbol |
| :---: | :---: | :---: |
| acceleration | meter per second squared | $\mathrm{m} / \mathrm{s}^{2}$ |
| angular acceleration | radian per second squared | $\mathrm{rad} / \mathrm{s}^{2}$ |
| angular velocity | radian per second | $\mathrm{rad} / \mathrm{s}$ |
| area | square meter | $\mathrm{m}^{2}$ |
| concentration (of amount of substance) | mole per cubic meter | $\mathrm{mol} / \mathrm{m}^{2}$ |
| current density | ampere per square meter | A/m ${ }^{\text {2 }}$ |
| density, mass | kilogram per cubic meter | kg/m ${ }^{3}$ |
| electric charge density | coulomb per cubic meter | $\mathrm{C} / \mathrm{m}{ }^{\text { }}$ |
| electric field strength | volt per meter | $\mathrm{V} / \mathrm{m}$ |
| electric flux density | coulomb per square meter | $\mathrm{C} / \mathrm{m}^{2}$ |
| energy density | joule per cubic meter | $\mathrm{J} / \mathrm{m}^{3}$ |
| entropy | joule per kelvin | $\mathrm{J} / \mathrm{K}$ |
| heat capacity | joule per kelvin | J/K |
| $\left.\begin{array}{l}\text { heat flux density } \\ \text { irradiance }\end{array}\right\}$ | watt per square meter | $\mathrm{W} / \mathrm{m}^{2}$ |
| luminance | candela per square meter | $\mathrm{cd} / \mathrm{m}^{2}$ |
| magnetic field strength | ampere per meter | A/m |
| molar energy | joule per mole | $\mathrm{J} / \mathrm{mol}$ |
| molar entropy | joule per mole kelvin | $\mathrm{J} /(\mathrm{mol} \cdot \mathrm{K})$ |
| molar heat capacity | joule per mole kelvin | $\mathrm{J} /(\mathrm{mol} \cdot \mathrm{K})$ |
| moment of force | newton meter | $\mathrm{N} \cdot \mathrm{m}$ |
| permeability | henry per meter | H/m |
| permittivity | farad per meter | F/m |
| radiance | watt per square meter steradian | $\left.\mathrm{W} / \mathrm{m}^{2} \cdot \mathrm{sr}\right)$ |
| radiant intensity | watt per steradian | W/sr |
| specific heat capacity | joule per kilogram kelvin | $\mathrm{J} /(\mathrm{kg} \cdot \mathrm{K})$ |
| specific energy | joule per kilogram | $\mathrm{J} / \mathrm{kg}$ |
| special entropy | joule per kilogram kelvin | $\mathrm{J} /(\mathrm{kg} \cdot \mathrm{K})$ |
| specific volume | cubic meter per kilogram | $\mathrm{m}^{1 / k g}$ |
| surface tension thermal | newton per meter | $\mathrm{N} / \mathrm{m}$ |
| conductivity | kelvin | $\mathrm{W} /(\mathrm{m} \cdot \mathrm{K})$ |

## TABIE 2-4 Cont.

Common SI Derived Units

| Quantity | Unit | Symbol |
| :--- | :--- | :--- |
| velocity | meter per second | $\mathrm{m} / \mathrm{s}$ |
| viscosity, dynamic | pascal second | $\mathrm{Pa} \cdot \mathrm{s}$ |
| viscosity, | square meter per |  |
| kinematic | second | $\mathrm{m}^{3} / \mathrm{s}$ |
| volume | cubic meter | $\mathrm{m}^{3}$ |
| wavenumber | 1 per meter | $1 / \mathrm{m}$ |

Some units, not part of SI, are so widely used they are impractical to abandon. These units (listed in Table 2-5) are acceptable for continued uses in the United States.

TABLE 2-5
Units in Use with SI

| Quantity | Unit | Symboi | Value |
| :---: | :---: | :---: | :---: |
| time | minute | min | $1 \mathrm{~min}=60 \mathrm{~s}$ |
|  | hour | h | $\begin{aligned} 1 \mathrm{~h} & =60 \mathrm{~min} \\ & =3600 \mathrm{~s} \end{aligned}$ |
|  | day | d | $\begin{aligned} 1 \mathrm{~d} & =24 \mathrm{~h} \\ & =86,400 \mathrm{~s} \end{aligned}$ |
|  | week |  |  |
|  |  |  |  |
| plane angle | degree | - | $1^{\circ}=(\pi / 180) \mathrm{rad}$ |
|  | minute | ' | $\begin{aligned} 1^{\prime} & =(1 / 60)^{\circ} \\ & =(\pi 10,800) \\ & \quad \text { rad } \end{aligned}$ |
|  | second | " | $\begin{aligned} & 1^{\prime \prime}=(1 / 60)^{\prime} \\ &=(\pi / 648,000) \\ & \quad \begin{aligned} \mathrm{rad} \end{aligned} \end{aligned}$ |
| volume | liter | L.* | $\begin{aligned} 1 \mathrm{~L} & =1 \mathrm{dm} \\ & =10^{-3} \mathrm{~m}^{3} \end{aligned}$ |
| mass | metric ton | $t$ | $11=10^{\circ} \mathrm{kg}$ |
| area (land) | hectare | ha | $1 \mathrm{ha}=10^{4} \mathrm{~m}^{2}$ |

*The international symbol for liter is the lowercatse "I," which can be casily confused with the number " 1 ." Therefore, the symbol " $L$ " or spelling out the term her is pretered for United States use.

## Prefixes

The sixteen prefixes in Table 2-6 are used to form multiples and submultiples of the SI units. The use of more than one prefix is to be avoided (e.g., use pico instead of mi-
cromicro and giga instead of kilomega). The preferred U.S. pronunciation of the terms is also included in the table. The accent is on the first syllable of each prefix.

TABLE 2-6
Metric Prefixes

| Multiplication factor | Prefix | Abbreviation | Pronunciation (U.S.) |
| :---: | :---: | :---: | :---: |
| $10^{18}$ | exa | E | ex'a (a as in about) |
| $10^{15}$ | peta | P | as in petal |
| $10^{12}$ | tera | T | as in terrace |
| $10^{\prime \prime}$ | giga | G | jig'a (a as in about) |
| $10^{*}$ | mega | M | as in megaphone |
| $10^{3}$ | kilo | k | as in kilowatt |
| $10^{2}$ | hecto | $h^{*}$ | heck ' toe |
| $1)^{1}$ | deka | da* | deck'a (a as in about) |
| $10^{-1}$ | deci | $\mathrm{d}^{*}$ | as in decimal |
| $10^{-2}$ | centi | $c^{*}$ | as in sentiment |
| $10^{-3}$ | milli | m | as in military |
| $10^{-6}$ | micro | $\mu$ | as in microphone |
| $10^{-9}$ | nano | n | nan'oh (an as in ant) |
| $10^{-12}$ | pico | p | peek'oh |
| $10^{-15}$ | femto | f | fem'toe (fem as in feminine) |
| $10^{-1 s}$ | atto | a | as in anatomy |

*The use of hecto, deka, deci, and centi should be avoided for SI unit multiples except for area and volume, and the nontechnical use of centimeter for body and clothing measurements.

## Conversion Table

Table 2-7 gives the number of places and the direction the decimal point must be moved to convert from one metric notation to another. The value labeled "Units" is the basic unit of measurement (e.g., ohms and farads). To use the table, find the desired

TABLE 2-7
Metric Conversion Table*

## Original value

| Desired value | Exa- | Peta- | Tera- | Giga- | Mega- | Myria-* | Kilo- | Hecto- | Deka- | Units | Deci- | Centi- | Milli- | Micro- | Nano- | Pico- | Femto- | Atto- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| exa- |  | $\leftarrow 3$ | -6 | $\leftarrow 8$ | $\leftarrow 9$ | $\leftarrow 10$ | -11 | -12 | -13 | -14 | -15 | $\leftarrow 18$ | $\leftarrow 21$ | $\leftarrow 24$ | - 27 | -30 | $\leftarrow 33$ | - 36 |
| peta- | $3 \rightarrow$ |  | $\leftarrow 3$ | $\leftarrow 5$ | $\leftarrow 6$ | $\leftarrow 7$ | $\leftarrow 8$ | $\leftarrow 9$ | -10 | $\leftarrow 11$ | -12 | +15 | $\leftarrow 18$ | $\leftarrow 21$ | -24 | -27 | $\leftarrow 30$ | --33 |
| tera- | $6 \rightarrow$ | $3 \rightarrow$ |  | $\leftarrow 3$ | $\leftarrow 6$ | 8 | $\leftarrow 9$ | $\leftarrow 10$ | -11 | -12 | -13 | -14 | -15 | -18 | -21 | $\leftarrow 24$ | -27 | $\leftarrow 30$ |
| giga- | $8 \rightarrow$ | $5 \rightarrow$ | $3 \rightarrow$ |  | $\leftarrow 3$ | - 5 | $\leftarrow 6$ | $\leftarrow 7$ | $\leftarrow 8$ | $\leftarrow 9$ | -10 | $\leftarrow 11$ | $\leftarrow 12$ | $\leftarrow 15$ | -18 | $\leftarrow 21$ | $\leftarrow 24$ | $\leftarrow 27$ |
| mega- | $9 \rightarrow$ | $6 \rightarrow$ | $6 \rightarrow$ | $3 \rightarrow$ |  | $\leftarrow 2$ | - 3 | $\leftarrow 4$ | $\leftarrow 5$ | $\leftarrow 6$ | $\leftarrow 7$ | $\leftarrow 8$ | -9 | $\leftarrow 12$ | -15 | -18 | -21 | --24 |
| myria- ${ }^{\text {- }}$ | $10 \rightarrow$ | $7 \rightarrow$ | $8 \rightarrow$ | $5 \rightarrow$ | $2 \rightarrow$ |  | $\leftarrow 1$ | $\leftarrow 2$ | $\leftarrow 3$ | -4 | $\leftarrow 5$ | $\leftarrow 6$ | $\leftarrow 7$ | -10 | $\leftarrow 13$ | $\leftarrow 16$ | -19 | +-22 |
| kilo- | $11 \rightarrow$ | $8 \rightarrow$ | $9 \rightarrow$ | $6 \rightarrow$ | $3 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 1$ | - 2 | - 3 | - 4 | -5 | $\leftarrow 6$ | $\leftarrow 9$ | -12 | -15 | -18 | -21 |
| hecto- | $12 \rightarrow$ | $9 \rightarrow$ | $10 \rightarrow$ | $7 \rightarrow$ | $4 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 1$ | $\leftarrow 2$ | $\leftarrow 3$ | -4 | - 5 | -8 | -11 | -14 | -17 | --20 |
| deka- | $13 \rightarrow$ | $10 \rightarrow$ | $11 \rightarrow$ | $8 \rightarrow$ | $5 \rightarrow$ | $3 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | +1 | $\leftarrow 2$ | -3 | -4 | -7 | -10 | $\leftarrow 13$ | $\leftarrow 16$ | $\leftarrow 19$ |
| units | $14 \rightarrow$ | $11 \rightarrow$ | $12 \rightarrow$ | $9 \rightarrow$ | $6 \rightarrow$ | $4 \rightarrow$ | $3 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 1$ | $\leftarrow 2$ | $\leftarrow 3$ | $\leftarrow 6$ | $\leftarrow 9$ | -12 | -15 | -18 |
| deci- | $15 \rightarrow$ | $12 \rightarrow$ | 13 $\rightarrow$ | $\underline{+}$ | $7 \rightarrow$ | $5 \rightarrow$ | $4 \rightarrow$ | $3 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | -1 | - 2 | $\leftarrow 5$ | -8 | $\leftarrow 11$ | -14 | -17 |
| centi- | $18 \rightarrow$ | $15 \rightarrow$ | $14 \rightarrow$ | $11 \rightarrow$ | 8 -* | $\rightarrow \rightarrow$ | $5 \rightarrow$ | $4 \rightarrow$ | $3 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 1$ | -4 | $\leftarrow 7$ | $\leftarrow 10$ | $\leftarrow 13$ | -16 |
| milli- | $21 \rightarrow$ | $18 \rightarrow$ | $15 \rightarrow$ | $12 \rightarrow$ | $9 \rightarrow$ | $7 \rightarrow$ | $6 \rightarrow$ | $5 \rightarrow$ | $4 \rightarrow$ | $3 \rightarrow$ | $2 \rightarrow$ | $1 \rightarrow$ |  | $\leftarrow 3$ | $\leftarrow 6$ | -9 | -12 | -15 |
| micro- | $24 \rightarrow$ | $21 \rightarrow$ | $18 \rightarrow$ | $15 \rightarrow$ | $12 \rightarrow$ | $10 \rightarrow$ | $9 \rightarrow$ | $8 \rightarrow$ | $7 \rightarrow$ | $6 \rightarrow$ | $5 \rightarrow$ | $4 \rightarrow$ | $3 \rightarrow$ |  | - 3 | $\leftarrow 6$ | $\leftarrow 9$ | -12 |
| nano- | $27 \rightarrow$ | 24 $\rightarrow$ | $21 \rightarrow$ | $18 \rightarrow$ | $15 \rightarrow$ | $13 \rightarrow$ | $12 \rightarrow$ | $11 \rightarrow$ | $10 \rightarrow$ | $9 \rightarrow$ | $8 \rightarrow$ | $7 \rightarrow$ | $6 \rightarrow$ | $3 \rightarrow$ |  | $\leftarrow 3$ | $\leftarrow 6$ | $\leftarrow 9$ |
| pico- | $30 \rightarrow$ | 27 $\rightarrow$ | $24 \rightarrow$ | $21 \rightarrow$ | $18 \rightarrow$ | $16 \rightarrow$ | $15 \rightarrow$ | $14 \rightarrow$ | $13 \rightarrow$ | $12 \rightarrow$ | $11 \rightarrow$ | $10 \rightarrow$ | $9 \rightarrow$ | $6 \rightarrow$ | $3 \rightarrow$ |  | --3 | -6 |
| femto- | $33 \rightarrow$ | $30 \rightarrow$ | $27 \rightarrow$ | $24 \rightarrow$ | $21 \rightarrow$ | $\stackrel{19}{ }$ | $18 \rightarrow$ | $17 \rightarrow$ | $16 \rightarrow$ | $15 \rightarrow$ | $14 \rightarrow$ | $13 \rightarrow$ | $12 \rightarrow$ | $\stackrel{\rightarrow}{ }$ | $6 \rightarrow$ | $3 \rightarrow$ |  |  |
| atto- | $36 \rightarrow$ | $33 \rightarrow$ | $30 \rightarrow$ | 27 $\rightarrow$ | $24 \rightarrow$ | $22 \rightarrow$ | $21 \rightarrow$ | $20 \rightarrow$ | $19 \rightarrow$ | $18 \rightarrow$ | $17 \rightarrow$ | $16 \rightarrow$ | $15 \rightarrow$ | $12 \rightarrow$ | $9 \rightarrow$ | $6 \rightarrow$ | $3 \rightarrow$ |  |

*Arrow indicates direction decimal moves.
tThe prefix "myria" is not normally used.
value in the left-hand column; then follow the horizontal line across to the column with the prefix in which the original value is stated. The number and arrow at this point indicate the number of places and the direction the decimal point must be moved to change the original value to the desired value.

## Miscellaneous

The terms "liter" and "meter" are also spelled "litre" and "metre." However, the most widely accepted U.S. practice is with the "er," and this spelling is recommended by the U.S. Department of Commerce.

While the SI unit for temperature is the kelvin ( K ), wide use is also made of the degree celsius ( ${ }^{\circ} \mathrm{C}$ ) in expressing temperature and temperature intervals in SI. The Celsius scale (formerly called centigrade) is directly related to thermodynamic temperature (kelvin) as follows:

$$
t=T-T_{n}
$$

where
$t$ is the temperature, in degrees Celsius, $T$ is the thermodynamic temperature, in kelvins, $T_{0}$ equals 273.15 K .

Note. A temperature interval of $1^{\circ} \mathrm{C}$ is exactly cqual to 1 K . Thus $0^{\circ} \mathrm{C}=273.15 \mathrm{~K}$.

The special name "liter" is used for a cubic decimeter, but use of this term should be restricted to measurements of liquids and gases. Do not use any prefix other than "milli" with "liter."

Note that "kilogram" is the only base unit employing a prefix. However, to form multiples, the prefix is added to "gram," not to "kilogram." The megagram may be used for large masses. However, the term "metric
ton" is also used in commercial applications. No prefixes should be used with "metric ton."

Other units have been used through the years as part of the metric (cgs) system. Avoid using them in SI.

## CONVERSION FACTORS

Table 2-8 lists the multiplying factors necessary to convert from one unit of mea-
sure to another. To use this table, locate either the unit of measure you are converting from or the one you are converting to in the left-hand column. Opposite this listing are the multiplying factors for converting either unit of measure to the other unit of measure.

Note. Conversions from one metric prefix to another (e.g., from kilo to mega) are not included in Table 2-8. For these conversions, see the preceding section.

TABLE 2-8
Conversion Factors

| To convert | Into | Multiply by | Conversely, multiply by |
| :---: | :---: | :---: | :---: |
| acres | square feet | $4.356 \times 10^{4}$ | $2.296 \times 10^{-5}$ |
| acres | square meters | 4047 | $2.471 \times 10^{-4}$ |
| acres | square miles | $1.5625 \times 10^{-3}$ | 640 |
| ampere-hours | coulombs | 3600 | $2.778 \times 10^{-4}$ |
| ampere-turns | gilberts | 1.257 | 0.7958 |
| ampere-turns per centimeter | ampere-turns per inch | 2.54 | 0.3937 |
| angstrom units | inches | $3.937 \times 10^{-9}$ | $2.54 \times 10^{8}$ |
| angstrom units | meters | $10^{-10}$ | $10^{10}$ |
| ares | square meters | 102 | $10^{-2}$ |
| atmospheres | feet of water | 33.90 | 0.02950 |
| atmospheres | inch of mercury at $0^{\circ} \mathrm{C}$ | 29.92 | $3.342 \times 10^{-2}$ |
| atmospheres | kilogram per square meter | $1.033 \times 10^{4}$ | $9.678 \times 10^{-5}$ |
| atmospheres | millimeter of mercury at $0^{\circ} \mathrm{C}$ | 760 | $1.316 \times 10^{-3}$ |
| atmospheres | pascals | $1.0133 \times 10^{5}$ | $0.9869 \times 10^{-5}$ |
| atmospheres | pounds per square inch | 14.70 | 0.06804 |
| barns | square centimeters | $10^{-24}$ | $10^{24}$ |
| bars | atmospheres | $9.870 \times 10^{-7}$ | 1.0133 |
| bars | dynes per square centimeter | $10^{6}$ | $10^{-6}$ |
| bars | pascals | $10^{5}$ | $10^{-5}$ |
| bars | pounds per square inch | 14.504 | $6.8947 \times 10^{-2}$ |
| board feet | cubic meters | $2.3597 \times 10^{-3}$ | $4.238 \times 10^{2}$ |
| Btu | ergs | $1.0548 \times 10^{10}$ | $9.486 \times 10^{-11}$ |
| Btu | foot-pounds | 778.3 | $1.285 \times 10^{-3}$ |
| Btu | joules | 1054.8 | $9.480 \times 10^{-4}$ |
| Btu | kilogram-calories | 0.252 | 3.969 |
| But per hour | horsepower-hours | $3.929 \times 10^{-4}$ | 2545 |
| bushels | cubic feet | 1.2445 | 0.8036 |
| bushels | cubic meters | $3.5239 \times 10^{-2}$ | 28.38 |
| calories, gram | joules | 4.185 | 0.2389 |
| carats (metric) | grams | 0.2 | 5 |
| Celsius | Fahrenheit | $\left({ }^{\circ} \mathrm{C} \times 9 / 5\right)+32={ }^{\circ} \mathrm{F}$ | $\left({ }^{\circ} \mathrm{F}-32\right) \times 5 / 9={ }^{\circ} \mathrm{C}$ |

TABLE 2-8 Cont.
Conversion Factors

| To convert | Into | Multiply by | Conversely, multiply by |
| :---: | :---: | :---: | :---: |
| Celsius | kelvin | ${ }^{\circ} \mathrm{C}+273.1=\mathrm{K}$ | $\mathrm{K}-273.1={ }^{\circ} \mathrm{C}$ |
| chains (surveyor's) | feet | 66 | $1.515 \times 10^{-2}$ |
| circular mils | square centimeters | $5.067 \times 10^{-6}$ | $1.973 \times 10^{5}$ |
| circular mils | square mils | 0.7854 | 1.273 |
| cords | cubic meters | 3.625 | 0.2758 |
| cubic feet | cords | $7.8125 \times 10^{-3}$ | 128 |
| cubic feet | gallons (liquid U.S.) | 7.481 | 0.1337 |
| cubic feet | liters | 28.32 | $3.531 \times 10^{-2}$ |
| cubic inches | cubic centimeters | 16.39 | $6.102 \times 10^{-2}$ |
| cubic inches | cubic feet | $5.787 \times 10^{4}$ | 1728 |
| cubic inches | cubic meters | $1.639 \times 10^{-5}$ | $6.102 \times 10^{4}$ |
| cubic inches | gallons (liquid U.S.) | $4.329 \times 10^{-3}$ | 231 |
| cubic meters | cubic feet | 35.31 | $2.832 \times 10^{-2}$ |
| cubic meters | cubic yards | 1.308 | 0.7646 |
| cups | cubic centimeter | $2.366 \times 10^{2}$ | 4.227 |
| curies | becquerels | $3.7 \times 10^{10}$ | $2.7 \times 10^{-11}$ |
| cycles per second | hertz | 1 | 1 |
| degrees (angle) | mils | 17.45 | $5.73 \times 10^{-2}$ |
| degrees (angle) | radians | $1.745 \times 10^{-2}$ | 57.3 |
| dynes | pounds | $2.248 \times 10^{-6}$ | $4.448 \times 10^{5}$ |
| electron volts | joules | $1.602 \times 10^{-19}$ | $0.624 \times 10^{1 \times}$ |
| ergs | foot-pounds | $7.376 \times 10^{-8}$ | $1.356 \times 10^{7}$ |
| ergs | joules | $10^{-7}$ | $10^{7}$ |
| ergs per second | watts | $10^{-7}$ | $10^{7}$ |
| ergs per square centimeter | watts per square centimeter | $10^{-3}$ | $10^{3}$ |
| Fahrenheit | kelvin | $\left({ }^{\circ} \mathrm{F}+459.67\right) / 1.8$ | 1.8K-459.67 |
| Fahrenheit | Rankine | ${ }^{\circ} \mathrm{F}+459.67={ }^{\circ} \mathrm{R}$ | ${ }^{\circ} \mathrm{R}-459.67={ }^{\circ} \mathrm{F}$ |
| faradays | ampere-hours | 26.8 | $3.731 \times 10^{-2}$ |
| fathoms | feet | 6 | 0.16667 |
| fathoms | meters | 1.8288 | 0.5467 |
| feet | centimeters | 30.48 | $3.281 \times 10^{-2}$ |
| feet | meters | 0.3048 | 3.281 |
| feet | mils | $1.2 \times 10^{4}$ | $8.333 \times 10^{-6}$ |
| feet of water at $4^{\circ} \mathrm{C}$ | inches of mercury at $0^{\circ} \mathrm{C}$ | 0.8826 | 1.133 |
| feet of water at $4^{\circ} \mathrm{C}$ | kilogram per square meter | 304.8 | $3.281 \times 10^{-3}$ |
| feet of water at $4^{\circ} \mathrm{C}$ | pascals | $2.989 \times 10^{3}$ | $3.346 \times 10^{-4}$ |
| fermis | meters | $10^{-15}$ | $10^{15}$ |
| foot candles | lux | 10.764 | 0.0929 |
| foot lamberts | candelas per square meter | 3.4263 | 0.2918 |
| foot-pounds | gram-centimeters | $1.383 \times 10^{4}$ | $1.235 \times 10^{-5}$ |
| foot-pounds | horsepower-hours | $5.05 \times 10^{--}$ | $1.98 \times 10^{6}$ |
| foot-pounds | kilogram-meters | 0.1383 | 7.233 |
| foot-pounds | kilowatt-hours | $3.766 \times 10^{-7}$ | $2.655 \times 10^{6}$ |
| foot-pounds | ounce-inches | 192 | $5.208 \times 10^{-3}$ |
| gallons | meters per second | 9.807 | 0.102 |
| gallons (liquid U.S.) | cubic meters | $3.785 \times 10^{-3}$ | 264.2 |
| gallons (liquid U.S.) | gallons (liquid British Imperial) | 0.8327 | 1.201 |

TABLE 2-8 Cont.
Conversion Factors

| To convert | Into | Multiply by | Conversely, multiply by |
| :---: | :---: | :---: | :---: |
| gammas | teslas | 10" | $10^{\prime \prime}$ |
| gausses | lines per square centimeter | 1.0 | 1.0 |
| gausses | lines per square inch | 6.452 | 0.155 |
| gausses | teslas | $10^{-4}$ | $10^{4}$ |
| gausses | webers per square inch | $6.452 \times 10^{*}$ | $1.55 \times 10^{7}$ |
| gilberts | amperes | 0.7958 | 1.257 |
| grads | radians | $1.571 \times 10^{-2}$ | 63.65 |
| grams | dynes | 980.7 | $1.02 \times 10^{-3}$ |
| grams | grains | 15.43 | $6.481 \times 10^{-2}$ |
| grams | ounces (avdp) | $3.527 \times 10^{\circ}$ | 28.35 |
| grams | poundals | $7.093 \times 10^{-2}$ | 14.1 |
| grams per centimeter | pounds per inch | $5.6 \times 10^{-3}$ | 178.6 |
| grams per cubic centimeter | pounds per cubic inch | $3.613 \times 10^{-2}$ | 27.68 |
| grams per square centimeter | pounds per square foot | 2.0481 | 0.4883 |
| hectares | acres | 2.471 | 0.4047 |
| horscpower | Btu per minute | 42.418 | $2.357 \times 10^{-2}$ |
| horsepower | foot-pounds per minute | $3.3 \times 10^{4}$ | $3.03 \times 10^{-4}$ |
| horscpower | foot-pounds per second | 550 | $1.182 \times 10^{-3}$ |
| horsepower | horsepower (metric) | 1.014 | 0.9863 |
| horsepower | kilowatts | 0.746 | 1.341 |
| horsepower (metric) | Btu per minute | 41.83 | $2.390 \times 10^{-2}$ |
| horsepower (metric) | kilogram-calories per minute | 10.54 | $9.485 \times 10^{-2}$ |
| horsepower (metric) | watts | $7.355 \times 10=$ | 745.7 |
| inches | centimeters | 2.54 | 0.3937 |
| inches | feet | $8.333 \times 10^{-2}$ | 12 |
| inches | meters | $2.54 \times 10^{-2}$ | 39.37 |
| inches | miles | $1.578 \times 10^{*}$ | $6.336 \times 10^{4}$ |
| inches | mils | $10^{\text {? }}$ | $10^{-3}$ |
| inches | yards | $2.778 \times 10^{-2}$ | 36 |
| inches of mercury at $0^{\circ} \mathrm{C}$ | pascals | $3.386 \times 10^{7}$ | $2.953 \times 10^{-4}$ |
| inches of mercury at $0^{\circ} \mathrm{C}$ | pounds per square inch | 0.4912 | 2.036 |
| inches of water at $4^{\circ} \mathrm{C}$ | inches of mercury | $7.355 \times 10^{-2}$ | 13.60 |
| inches of water at $4^{\circ} \mathrm{C}$ | kilograms per square meter | 25.40 | $3.937 \times 10^{-2}$ |
| inches of water at $15.6^{\circ}{ }^{\circ}$ | pascals | $2.488 \times 10^{2}$ | $4.02 \times 10^{-3}$ |
| joules | foot-pounds | 0.7376 | 1.356 |
| joules | watt-hours | $2.778 \times 10^{-4}$ | 3600 |
| kilogram-calories | kilogram-meters | 426.9 | $2.343 \times 10^{-3}$ |
| kilograms | tonnes | $10^{\prime}$ | $10^{-3}$ |
| kilograms | tons (long) | $9.842 \times 10^{-4}$ | 1016 |
| kilograms | tons (short) | $1.102 \times 10^{-3}$ | 907.2 |
| kilograms | pounds (avdp) | 2.205 | 0.4536 |
| kilograms per square meter | pounds per square foot | 0.2048 | 4.882 |

TABLE 2-8 Cont.
Conversion Factors

| To convert | Into | Multiply by | Conversely, multiply by |
| :---: | :---: | :---: | :---: |
| kilometers | feet | 3281 | $3.408 \times 10^{-4}$ |
| kilometers | inches | $3.937 \times 10^{4}$ | $2.54 \times 10^{-4}$ |
| kilometers | light years | $1.0567 \times 10^{-17}$ | $9.4637 \times 10^{12}$ |
| kilometers per hour | feet per minute | 54.68 | $1.829 \times 10=$ |
| kilometers per hour | knots | 0.5396 | 1.8532 |
| kilowatt-hours | Btu | 3413 | $2.93 \times 10^{-4}$ |
| kilowatt-hours | foot-pounds | $2.655 \times 10^{6}$ | $3.766 \times 10^{=}$ |
| kilowatt-hours | horsepower-hours | 1.341 | 0.7457 |
| kilowatt-hours | joules | $3.6 \times 10^{6}$ | $2.778 \times 10^{-8}$ |
| kilowatt-hours | kilogram-calories | 860 | $1.163 \times 10^{-3}$ |
| kilowatt-hours | kilogram-meters | $3.671 \times 10^{\text {a }}$ | $2.724 \times 10^{\text {\% }}$ |
| kilowatt-hours | pounds water evaporated from and at $212^{\circ} \mathrm{F}$ | 3.53 | 0.284 |
| kilowatt-hours | watt-hours | $10^{2}$ | $10^{-3}$ |
| knots | feet per second | 1.688 | 0.5925 |
| knots | meters per minute | 30.87 | 0.0324 |
| knots | miles per hour | 1.1508 | 0.869 |
| lamberts | candles per square centimeter | 0.3183 | 3.142 |
| lamberts | candles per square inch | 2.054 | 0.4869 |
| leagues | miles | 3 | 0.33 |
| links | chains | 0.01 | 100 |
| links (surveyor's) | inches | 7.92 | 0.1263 |
| liters | bushels (dry U.S.) | $2.838 \times 10^{-2}$ | 35.24 |
| liters | cubic centimeters | $10^{3}$ | $10^{-3}$ |
| liters | cubic inches | 61.02 | $1.639 \times 10=$ |
| liters | cubic meters | $10^{-3}$ | 10: |
| liters | gallons (liquid U.S.) | 0.2642 | 3.785 |
| liters | pints (liquid U.S.) | 2.113 | 0.4732 |
| $\log _{\mathrm{c}} N$ | $\log _{\text {ge }} N$ | 0.4343 | 2.303 |
| lumens per square foot | foot-candles | 1 | 1 |
| lumens per square meter | foot-candles | 0.0929 | 10.764 |
| lux | foot-candles | 0.0929 | 10.764 |
| maxwells | kilolines | $10^{\text {- }}$ | $10^{\text {: }}$ |
| maxwells | megalines | $10 *$ | $10^{5}$ |
| maxwells | webers | 10-* | $10^{*}$ |
| meters | feet | 3.28 | $30.48 \times 10^{-2}$ |
| meters | inches | 39.37 | $2.54 \times 10$ : |
| meters | miles | $6.214 \times 10^{-4}$ | 1609.35 |
| meters | yards | 1.094 | 0.9144 |
| meters per minute | feet per minute | 3.281 | 0.3048 |
| meters per minute | kilometers per hour | 0.06 | 16.67 |
| Mhos | siemens | 1 | 1 |
| miles (nautical) | fcet | 6076.1 | $1.646 \times 10^{4}$ |
| miles (nautical) | meters | 1852 | $5.4 \times 10^{-4}$ |
| miles (statute) | feet | 5280 | $1.894 \times 10=$ |
| miles (statute) | kilometers | 1.609 | 0.6214 |
| miles (statute) | light years | $1.691 \times 10^{19}$ | $5.88 \times 10^{12}$ |
| miles (statute) | miles (nautical) | 0.869 | 1.1508 |
| miles (statute) | yards | 1760 | $5.6818 \times 10^{-4}$ |
| miles per hour | feet per minute | 88 | $1.136 \times 10^{=}$ |

# Handbook of Electronics Tables and Formulas 

TABLE 2-8 Cont.
Conversion Factors

| To convert | Into | Multiply by | Conversely, multiply by |
| :---: | :---: | :---: | :---: |
| miles per hour | feet per second | 1.467 | 0.6818 |
| miles per hour | kilometers per hour | 1.609 | 0.6214 |
| miles per hour | kilometers per minute | $2.682 \times 10^{-2}$ | 37.28 |
| miles per hour | knots | 0.8684 | 1.152 |
| millimeters | inches | $3.937 \times 10^{-2}$ | 25.4 |
| millimeters | microns | $10^{3}$ | $10^{-3}$ |
| mils | meters | $2.54 \times 10^{-5}$ | $3.94 \times 10^{4}$ |
| mils | minutes | 3.438 | 0.2909 |
| minutes (angle) | degrees | $1.666 \times 10^{-2}$ | 60 |
| minutes (angle) | radians | $2.909 \times 10^{-4}$ | 3484 |
| nepers | decibels | 8.686 | 0.1151 |
| newtons | dynes | $10^{\text {s }}$ | $10^{-5}$ |
| newtons | kilograms | 0.1020 | 9.807 |
| newtons per square meter | pascals | 1 | 1 |
| newtons | pounds (avdp) | 0.2248 | 4.448 |
| oersteds | amperes per meter | $7.9577 \times 10$ | $1.257 \times 10^{-2}$ |
| ohms | ohms (international) | 0.99948 | 1.00052 |
| ohms circular-mil per foot | ohms per square millimeter per meter | $1.66 \times 10^{-3}$ | $6.024 \times 10^{2}$ |
| ohms per foot | ohms per meter | 0.3048 | 3.281 |
| ounces (fluid) | quarts | $3.125 \times 10^{-2}$ | 32 |
| ounces (avdp) | pounds | $6.25 \times 10^{-2}$ | 16 |
| pints | quarts (liquid U.S.) | 0.50 | 2 |
| poundals | dynes | $1.383 \times 10^{4}$ | $7.233 \times 10^{-3}$ |
| poundals | pounds (avdp) | $3.108 \times 10^{-2}$ | 32.17 |
| pounds | grams | 453.6 | $2.205 \times 10^{-3}$ |
| pounds (force) | newtons | 4.4482 | 0.2288 |
| pounds carbon oxidized | Btu | 14,544 | $6.88 \times 10^{-5}$ |
| pounds carbon oxidized | horsepower-hours | 5.705 | 0.175 |
| pounds carbon oxidized | kilowatt-hours | 4.254 | 0.235 |
| pounds of water (dist) | cubic feet | $1.603 \times 10^{-2}$ | 62.38 |
| pounds of water (dist) | gallons | 0.1198 | 8.347 |
| pounds per foot | kilograms per meter | 1.488 | 0.6720 |
| pounds per square inch | dynes per square centimeter | $6.8946 \times 10^{4}$ | $1.450 \times 10^{-5}$ |
| pounds per square inch | pascals | $6.895 \times 10^{3}$ | $1.45 \times 10^{-4}$ |
| quadrants | degrees | 90 | $11.111 \times 10^{-2}$ |
| quadrants | radians | 1.5708 | 0.637 |
| quarts (U.S. dry) | cubic centimeters | 1101.4 | $9.9079 \times 10^{-4}$ |
| quarts (U.S. liquid) | cubic centimeters | 946.4 | $1.057 \times 10^{-3}$ |
| radians | mils | $10^{3}$ | $10^{-3}$ |
| radians | minutes | $3.438 \times 10^{3}$ | $2.909 \times 10^{-4}$ |
| radians | seconds | $2.06265 \times 10^{5}$ | $4.848 \times 10^{-6}$ |
| revolutions per minute | degrees per second | 6.0 | 0.1667 |
| revolutions per minute | radians per second | 0.1047 | 9.549 |
| revolutions per minute | revolutions per second | $1.667 \times 10^{-2}$ | 60 |
| rods | feet | 16.5 | $6.061 \times 10^{-2}$ |
| rods | miles | $3.125 \times 10^{-3}$ | 320 |
| rods | yards | 5.5 | 0.1818 |
| roentgens | coulombs per kilogram | $2.58 \times 10^{-4}$ | $3.876 \times 10^{3}$ |

TABLE 2-8 Cont.
Conversion Factors

| To convert | Into | Multiply by | Conversely, multiply by |
| :---: | :---: | :---: | :---: |
| slugs | kilograms | 1.459 | 0.6854 |
| slugs | pounds (avdp) | 32.174 | $3.108 \times 10^{-2}$ |
| square feet | square centimeters | 929.034 | $1.076 \times 10^{-3}$ |
| square feet | square inches | 144 | $6.944 \times 10^{-3}$ |
| square feet | square meters | $9.29 \times 10^{-2}$ | 10.764 |
| square feet | square miles | $3.587 \times 10^{-8}$ | $27.88 \times 10^{6}$ |
| square feet | square yards | $11.11 \times 10^{-2}$ | 9 |
| square inches | circular mils | $1.273 \times 10^{6}$ | $7.854 \times 10^{-}$ |
| square inches | square centimeters | 6.452 | 0.155 |
| square inches | square mils | $10^{\circ}$ | $10^{-6}$ |
| square inches | square millimeters | 645.2 | $1.55 \times 10^{-3}$ |
| square kilometers | square miles | 0.3861 | 2.59 |
| square meters | square yards | 1.196 | 0.8361 |
| square miles | acres | 640 | $1.562 \times 10^{-3}$ |
| square miles | square yards | $3.098 \times 10^{6}$ | $3.228 \times 10^{-7}$ |
| square millimeters | circular mils | 1973 | $5.067 \times 10^{-4}$ |
| square mils | circular mils | 1.273 | 0.7854 |
| steres | cubic meters | 1 | 1 |
| stokes | square meter per second | $10^{-4}$ | $10^{-4}$ |
| tablespoons | cubic centimeters | 14.79 | $6.761 \times 10^{-2}$ |
| teaspoons | cubic centimeters | 4.929 | 0.203 |
| tonnes | kilograms | $10^{3}$ | $10^{-3}$ |
| tonnes | pounds | 2204.63 | $4.536 \times 10^{-4}$ |
| tons (long) | pounds (avdp) | 2240 | $4.464 \times 10^{-4}$ |
| tons (metric) | kilograms | $10^{3}$ | $10^{-3}$ |
| tons (short) | pounds | 2000 | $5 \times 10^{-4}$ |
| torrs | newtons per square meter | 133.32 | $7.5 \times 10^{-3}$ |
| varas | feet | 2.7777 | 0.36 |
| watts | Btu per hour | 3.413 | 0.293 |
| watts | Btu per minute | $6.589 \times 10^{-2}$ | 17.58 |
| watts | foot-pounds per minute | 44.26 | $2.26 \times 10^{-2}$ |
| watts | foot-pounds per second | 0.7378 | 1.356 |
| watts | horsepower | $1.341 \times 10^{-3}$ | 746 |
| watts | kilogram-calories per minute | $1.433 \times 10^{-2}$ | 69.77 |
| watt-seconds | gram-calories (mean) | 0.2389 | 4.186 |
| watt-seconds | joules | 1 | 1 |
| webers | maxwells | $10^{\text {F }}$ | $10^{-s}$ |
| webers per square meter | gausses | $10^{4}$ | $10^{-4}$ |
| yards | feet | 3 | 0.3333 |
| yards | varas | 1.08 | 0.9259 |

## STANDARD FREQUENCIES AND TIME SIGNALS

## WWV, WWVH, and WWVB

Time signals and audiofrequencies are
broadcast continuously day and night from WWV, operated by the National Bureau of Standards at Fort Collins, Colorado 80521. The WWV broadcast frequencies are $2.5,5$, 10 , and 15 MHz and the 1 -s marker tone consists of a $5-\mathrm{ms}$ pulse at 1000 Hz . A simi-
lar station, WWVH, is located at Kekaha, Kauai, Hawaii. It broadcasts on frequencies $2.5,5,10$, and 15 MHz and the 1 -s marker tone consists of a 5 -ms pulse at 1200 Hz .

The broadcasts of WWV may also be heard by the use of the telephone by dialing (303) 499-7111, Boulder, Colorado. WWVH may be heard by dialing (808) 335 4363. Neither is a toll free number. The telephone user will hear the live broadcasts from the station called. With the instabilities and variable delays of propagation, the accuracy of the telephone time signals will not be better than 30 ms . This service is automatically limited to 3 minutes per call.

Station WWVB broadcasts on a frequency of 60 kHz . The station broadcasts a time code continuously. No voice announcements are broadcast from WWVB.

WWV and WWVH broadcast frequencies are consistent with the internationally agreed time scale Coordinated Universal Time (UTC). These changes became effective January 1, 1972. This coordination provides a more uniform system of time and frequency transmission throughout the world. It also aids in the solution of many scientific and technical problems such as radio communications, geodesy, navigation, and artificial-satellite tracking. At WWV and WWVH, the carrier and modulation frequencies are derived from cesium-controlled oscillators. These broadcasts are in conformity with the international Radio Consultation Committee. The frequency offset of UTC was made permanently zero, effective 0000 hours UTC January 1, 1972.

The hourly broadcast of WWV and WWVH is shown in Fig. 2-2. Standard audiofrequencies of 440,500 , and 600 Hz are broadcast on each radio carrier frequency by WWV and WWVH. The $600-\mathrm{Hz}$ tone is broadcast during the odd minutes by WWV and during even minutes by WWVH.

The $500-\mathrm{Hz}$ tone is broadcast during alternate minutes unless voice announcements or silent periods are scheduled. The $440-\mathrm{Hz}$ tone is broadcast beginning 2 minutes after the hour at WWV and 1 minute after the hour at WWVH. The $440-\mathrm{Hz}$ tone period is omitted during the first hour of the UTC day. The duration of each transmitted tone is approximately 45 seconds, as indicated in Fig. 2-2.

The frequencies transmitted from WWV and WWVH are accurate to within one part of $10^{12}$.

There are no audiotones or special announcements during the semisilent period from either station. The period for WWV is from 45 to 50 minutes after the hour and from 15 to 20 minutes after the hour from WWVH.

A voice announcement of Coordinated Universal Time is given during the last 7.5 seconds of every minute. The announcement is as follows: "At the tone ___ hours ___ minutes Coordinated Universal Time." A voice announcement at WWVH occurs during the period 45 seconds to 52.5 seconds after the minute. The voice announcement at WWVH precedes that of WWV by 7.5 seconds. However, the tone markers referred to in both announcements occur simultaneously, but they may not be received at the same time due to propagation effects.

Before January 1, 1972, time signals broadcast from WWV and WWVH were kept in close agreement with UT2 (astronomical time) by making step adjustments of 100 ms when necessary. On December 1, 1971, at 23 hours 59 minutes 60.107600 seconds UTC (i.e., GMT), UTC (NBS) "was retarded 0.107600 second" to give the new UTC scale an initial difference of 10 seconds late with respect to International Atomic Time (IAT) as maintained by the

## Constants and Standards

The 59th second puise omitted
Beginning of each hour identified by 0.8 sec . long 1500 Hz tone (WWV \& WWVH).


The 29th Second pulse omitted.
Beginning of each minute identified by
08 sec long I 200 Hz tone
Fig. 2-2

Bureau International de l'Heure (BIH) in Paris, France.

Since the new UTC rate became effective January 1, 1972, the need of periodic adjustment to agree with the earth's rotation is not needed. UTC departs from the UT1 (earth's rotation time), gaining about $1 \mathrm{sec}-$ ond each year. To prevent this difference from exceeding 0.7 second, it is necessary to make 1 -second adjustments each year.

Corrections are made at the rate of about 1 second each year and are adjusted by 1 second exactly when required, on either December 31 or June 30 when BIH determines they are needed to keep broadcast time signals within $\pm 0.9$ second astronomical time UT1. Fig. 2-3 illustrates how the second is added. The second is inserted between the end of the 60th second of the last minute of the last day of a month and the beginning of the next minute. It is analogous to adding the extra day in the leap year. BIH will announce this occurrence of adding to the second two months in advance.

The WWV timing code shown in Fig. 2-4 was initially broadcast on July 1, 1971.

It now is transmitted continuously, both by WWV and WWVH, on a $100-\mathrm{Hz}$ subcarrier. This time code provides a standardized time base for use when scientific observations are being made at two widely separated locations. Accurate time markers, to an accuracy of 10 ms , are available for satellite telemetric signals and other scientific data. The code format is a modified IRIGH time code that produces a 1 -pps rate and is carried on the $100-\mathrm{Hz}$ modulation. Minute, hour, and day of year are contained in this UTC time-of-year information. The second information is obtained by counting the pulses. The code is synchronous with the frequency and time signals.

The code binary-coded decimal (bcd) as shown in Fig. 2-5 contains the time-of-year information. The minute contains seven bcd groups, two groups for minutes, two groups for hours, and three groups for the day of year. The complete time frame is 1 min . The "on time" occurs at the positive-going leading edge of all pulses.

The binary-to-decimal weighting scheme is $1-2-4-8$ with the least significant binary


Fig. 2-3

## Constants and Standards


$P_{0} \cdot P_{5}$ Position Identiflers (0 0770 Second Duration)
W Weighted Code Digit io 470 Second Durationt
C Weighted Control Element (0.470 Second Duration) Control Function \#
Binary One During "Dayight" Yime Binary Zero During "Standard" Time

UTC at Point $A=173$ Days. 21 Hours. 10 Minutes $U_{1}$ At Point $A=173$ Days, 21 Hours. 10 Mrrutes. 0.3 Second

Duration of index Markers. Unweighted Code. and Unweighted Contros Elements $=0.170$ Second
Note: Beginning of pulse is represented by positive going edge
Fig. 2-4
digit always transmitted first. The binary groups and their basic decimal equivalents are shown in Table 2-9. The decimal equivalent of a bcd group is derived by multiplying each binary digit times the weight factor of its respective column and adding the four products together.

Example. The binary sequence 1010 in the 1-2-4-8 scheme means $(1 \times 1)+(0 \times 2)+(1 \times 4)+$ $(0 \times 8)=1+0+4+0=5$. If fewer than nine decimal digits are needed, one or more of the binary columns may be omitted.

In the standard IRIG-H code, a binary 0 pulse consists of exactly 20 cycles of $100-\mathrm{Hz}$ amplitude modulation ( $200-\mathrm{ms}$ duration), whereas a binary 1 consists of 50 cycles of 100 Hz ( $500-\mathrm{ms}$ duration). In the WWV/

TABLE 2-9
Binary and Decimal Equivalents

|  | Binary group |  | Decimal <br> equivalent |  |
| :---: | :---: | :---: | :---: | :---: |
| $\boldsymbol{1}$ | 2 | 4 | $\boldsymbol{8}$ | 0 |
| 0 | 0 | 0 | 0 | 1 |
| 1 | 0 | 0 | 0 | 2 |
| 0 | 1 | 0 | 0 | 3 |
| 1 | 1 | 0 | 0 | 4 |
| 0 | 0 | 1 | 0 | 5 |
| 1 | 0 | 1 | 0 | 6 |
| 0 | 1 | 1 | 0 | 7 |
| 1 | 1 | 1 | 0 | 8 |
| 0 | 0 | 0 | 1 | 9 |
| 1 | 0 | 0 | 1 |  |

WWVH broadcast format, however, all tones are suppressed briefly while the seconds pulses are transmitted.

Because the tone suppression applies also to the $100-\mathrm{Hz}$ subcarrier frequency, it has the effect of deleting the first $30-\mathrm{ms}$ portion of each binary pulse in the time code. Thus, a binary 0 contains only 17 cycles of
$100-\mathrm{Hz}$ amplitude modulation ( $170-\mathrm{ms}$ duration) and a binary 1 contains 47 cycles of 100 Hz (470-ms duration). The leading edge of every pulse coincides with a positive-going zero crossing of the $100-\mathrm{Hz}$ subcarrier,
 Yo obtain the coressponding $\mathrm{UT}_{1}$ scale reading subtract 41 milliseconds.


Fig. 2-5
but it occurs 30 ms after the beginning of the second.

Within a time frame of 1 min , enough pulses are transmitted to convey in bcd language the current minute, hour, and day of year. Two bcd groups are needed to express the hour ( 00 through 23); three groups are needed to express the day of year (001 through 366). When representing units, tens, or hundreds, the basic 1-2-4-8 weights are simply multiplied by 1,10 , or 100 as appropriate. The coded information always refers to time at the beginning of the 1 -min frame. Seconds may be determined by counting pulses within the frame.

Each frame starts with a unique spacing of pulses to mark the beginning of a new minute. No pulse is transmitted during the first second of the minute. Instead, a 1-s space or hole occurs in the pulse train at that time. Because all pulses in the time code are 30 ms late with respect to UTC, each minute actually begins 1030 ms (or 1.03 s ) prior to the leading edge of the first pulse in the new frame.

For synchronization purposes, every 10 s a so-called position identifier pulse is transmitted. Unlike the bod data pulses, the position identifiers consist of 77 cycles of 100 Hz (770-ms duration).

UT1 corrections to the nearest 0.1 s are broadcast via bed pulses during the final 10 s of each frame. The coded pulses that occur between the 50th and 59th seconds of each frame are called control functions. Control function No. 1, which occurs at 50 s , tells whether the UT1 correction is negative or positive. If control function No. I is a binary 0 , the correction is negative; if it is a binary 1 , the correction is positive. Control functions No. 7, 8, and 9, which occur, respectively, at 56,57 , and 58 s , specify the amount of UTI correction. Because the UT1 corrections are expressed in tenths of a
second, the basic binary-to-decimal weights are multiplied by 0.1 when applied to these control functions.

Control function No. 6, which occurs at 55 s , is programmed as a binary 1 throughout those weeks when Daylight Saving Time is in effect and as a binary 0 when Standard Time is in effect. The setting of this function is changed at 0000 UTC on the date of change. Throughout the U.S. mainland, this schedule allows several hours for the function to be received before the change becomes effective locally (i.e., at 2:00 am local time). Thus, control function No. 6 allows clocks or digital recorders operating on local time to be programmed to make an automatic 1-hr adjustment in changing from Daylight Saving Time to Standard Time and vice versa.

Figure 2-4 shows one frame of the time code as it might appear after being rectified, filtered, and recorded. In this example, the leading edge of each pulse is considered to be the positive-going excursion. The pulse train in the figure is annotated to show the characteristic features of the time code format. The six position identifiers are denoted by symbols $\mathrm{P}_{1}, \mathrm{P}_{2}, \mathrm{P}_{3}, \mathrm{P}_{4}, \mathrm{P}_{5}$, and $\mathrm{P}_{40}$. The minutes, hours, days, and UT1 sets are marked by brackets, and the applicable weighting factors are printed beneath the coded pulses in each bcd group. With the exception of the position identifiers, all uncoded pulses are set permanently to binary 0.

The first 10 s of every frame always include the 1.03 -s hole followed by eight uncoded pulses and the position identifier $\mathrm{P}_{1}$. The minutes set follows $P_{1}$ and consists of two bed groups separated by an uncoded pulse. Similarly, the hours set follows $P_{2}$. The days set follows $P$, and extends for two pulses beyond $P_{4}$ to allow enough elements to represent three decimal digits. The UT1
set follows $\mathrm{P}_{\mathrm{c}}$, and the last pulse in the frame is always $\mathrm{P}_{0}$.

In Fig. 2-4, the least significant digit of the minutes set is $(0 \times 1)+(0 \times 2)+$ $(0 \times 4)+(0 \times 8)=0$; the most significant digit of that set is $(1 \times 10)+(0 \times 20)+(0$ $\times 40)=10$. Hence, at the beginning of the 1.03 -s hole in that frame, the time was exactly 10 min past the hour. By decoding the hours set and the days set, the time of day is in the 21 st hour on the 173 rd day of the year. The UT1 correction is +0.3 s . Therefore, at point A , the correct time on the UT1 scale is 173 days, 21 hours, 10 minutes, 0.3 second.

Weather information about major storms in the Atlantic and Pacific areas is broadcast from WWV and WWVH. Times of broadcast are $0500,1100,1700$, and 2300 UTC by WWV and $0000,0600,1200$, and 1800 UTC by WWVH. These broadcasts are given in voice during the 8th, 9 th, and 10th minute from WWV and during the 48th, 49th, and 50th minute from WWVH.

Omega Navigation System status reports are broadcast in voice from WWV at 16 minutes after the hour and from WWVH at 47 minutes after the hour. The International Omega Navigation System is a very low frequency (VLF) radio navigation aid operating in the $10-$ to $14-\mathrm{kHz}$ frequency band. Eight stations operate around the world. Omega, like other radio navigation systems, is subject to signal degradation caused by ionospheric disturbances at high latitudes. The Omega announcements on WWV and WWVH are given to provide users with immediate notification of such events and other information on the status of the Omega system.

Station identifications are made by voice every 30 min by WWV and WWVH.

Station WWVB broadcasts a continuous binary coded decimal (bcd) signal, which is synchronized with the $60-\mathrm{kHz}$ car-
rier signal. WWVB uses a level-shift carrier time code. The signal consists of 60 markers each minute, as shown in Fig. 2-5, with one marker occurring each second.

When a marker is generated, the carrier power is reduced by 10 dB at the beginning of the corresponding second and restored 0.2 s later for an uncoded marker or binary $0,0.5 \mathrm{~s}$ later for a binary 1 , and 0.8 s later for a 10 -s position marker or for a minute reference marker.

The bcd are set up in groups. The 1st and 2 nd bcd groups specify the minute of the hour; the 3rd and 4th bed groups specify the hour of the day; the 5th, 6th, and 7th bcd groups specify the day of the year; and the $9 \mathrm{th}, 10 \mathrm{th}$, and 11th bcd groups specify the number of milliseconds to be added or subtracted from the code time in order to obtain UT1 (astronomical time). The 8th bcd group specifies if the UT1 is fast or slow with the respect to the code time.

If UT1 is slow, a binary 1 labeled sub (subtract) will be broadcast during the 38th second of the minute. If UT1 is fast, binary l's labeled ADD will be broadcast during the 37 th and 39 th seconds of the minute. The 12 th bcd group is not used to convey information.

## CHU

The National Research Council of Ottawa, Ontario, Canada, broadcasts time signals that can be heard throughout North America and many other parts of the world. The frequencies are 3330,7335 , and 14,670 kHz , and the transmission is continuous on all frequencies. The transmitter has a power output of 3 kW at frequencies of 3330 and $14,670 \mathrm{kHz}$ and a power output of 10 kW at 7335 kHz .

The frequencies and time signals are derived from a cesium atomic clock that is ac-
curate to within a few microseconds per year.

A chart of the broadcast signal is shown in Fig. 2-6. The seconds pips consist of 300 cycles of a $1000-\mathrm{Hz}$ tone. The seconds pips are broadcast continuously except for the 29th and the 51st to the 59th pips, which are omitted each minute. In addition, the 1st to 10th pips are omitted during the first minute of the hour. The beginning of the pip marks the exact second. The zero pip of each minute has a duration of 0.5 s , and the zero pip of each hour has a duration of 1 s . The remaining seconds pips have a duration of 0.3 s. An FSK time code is inserted after 10 cycles on the 31st to 39th seconds.

A voice announcement of the time is given each minute during the 10 -s interval between the 50 th and 60 th second when the pips are omitted. The announcement is as follows: "CHU, Dominion Observatory Canada, Eastern Standard Time, hours, $\qquad$ minutes." The time given refers to the beginning of the minute pip that follows and is on the $24-\mathrm{hr}$ system.

## Other Standards Stations

Throughout the world, there are many other stations that broadcast similar data. Table 2-10 lists some of them as well as some other data about stations operating on the standards frequencies. It also lists some other stations in the low frequency (LF) and very low frequency (VLF) bands, which
broadcast similar data, but not on the frequencies assigned for standard-frequency operation.

## WORLD TIME CONVERSION CHART

The standard time in any time zone can be converted to Greenwich Mean Time (GMT) (i.e., UTC) or to any time zone in other parts of the world by using the chart in Fig. 2-7. To use this chart, visualize the horizontal line as making a complete circle. From one time zone, trace horizontally to the right (counterclockwise); it will be tomorrow when passing through midnight and yesterday when passing the international date line. Moving to the left (clockwise), it will be yesterday when passing midnight and tomorrow when passing the international date line. There is no date change when passing both the international date line and midnight, moving in one direction. Always trace in the shortest direction between time zones.

Example. At 9 PM in Ncw York Eastern Standard Time, it is 4 am tomorrow in Moscow, Russia (moving left, clockwise).

At 10 Am in the Philippines, it will be 4 PM yesterday in Hawaii (moving right, counterclockwise).

At 7 am Chicago Central Standard Time, it is 10 PM in Tokyo, Japan the same day (moving left, clockwise).


Fig. 2-6

|  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0000 | 1 AM | 2 AM | 3 AM | $\triangle A M$ | 5 AM | 6 AM | 7 AN | 8 AM | $9 \hat{M}$ | 10 AM | $11 \sim M$ |
| 0100 | 2 AM | 3 AM | 4 AM | 5 AM | $\sigma$ AM | 7 AM | 8 AM | 9 AM | $10 A M$ | 11 AM | Noon |
| 0200 | 3 AM | 4 AM | 5 AM | $6 A M$ | 7 AM | 8 AM | $4 A M$ | $\because A M$ | 11 AM | Nown | 1 PM |
| $0300$ | 4 AM | 5 AM | 6 AM | 7 AM | 8 AM | 9 AM | 10 AM | 11 Am | Noon | 1 PM | $2 \text { PM }$ |
| $0400$ | $5 A M$ | $O A M$ | $7 \mathrm{AM}$ | $8 \mathrm{AM}$ | $9 \mathrm{AM}$ | 10 AM | 11 AM | Noon | $1 P M$ | 2 PM | 3 PM |
| 0500 | $\sigma$ AM | 7 AM | 8 AM | 9 AM | $10 A M$ | 11 AM | Noon | 1 PM | 2 PM | 3 PM | 4 PM |
| － | － | －－－ |  |  |  |  | －－ | － | －－ |  |  |
| 0600 | 7 AM | 8 AM | 9 AM | 10 AM | 11 A M | Noon | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM |
| 0700 | 8 AM | 9 AM | 10 AM | 11 AM | Noon | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM |
| 0800 | $9 A M$ | 10 AM | 11 AM | Noun | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM |
| 0900 | $10.4 M$ | $11) A M$ | Noon | 1 PM | 2 PM | 3 PM | $4 P M$ | 5 PM | 6 PM | 7 PM | 8 PM |
| 1000 | 11 AM | Noon | 1 PM | $2 P M$ | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM |
| 1100 | Noun | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM |
| 1200 | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM |
| 1300 | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Mid－ night |
| 1400 | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Mid－ night | 1 AM |
| 1500 | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Mid－ night | 1 AM | 2 AM |
| 1600 | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Mid－ night | 1 AM | 2 AM | 3 AM |
| 1700 | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Mid－ night | 1 AM | 2 AM | 3 AM | 4 AM |
| 1800 | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Mid． night | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM |
| 1900 | 8 PM | 9 PM | 10 PM | $\\|$ PM | Mid－ night | 1 AM | 2 AM | 3 AM | $\triangle A M$ | 5 AM | 6 AM |
| 2000 | 9 PM | 10 PM | 11 PM | Mid－ night | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | 6 AM | 7 AM |
| 2100 | 10 PM | 11 PM | Mid－ night | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | 6 AM | 7 AM | 8 AM |
| 2200 | 11 PM | Mid－ night | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | 6 AM | 7 AM | 8 AM | 9 AM |
| 2300 | Mid－ night | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | 6 AM | 7 AM | 8 AM | 9 AM | 10 AM |

Fig．2－7

|  |  |  |  |  |  |  |  |  | $\begin{aligned} & \dot{\circ} \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | \% \% 0 $\chi$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Nocn | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM |
| 1 PM | $2 P M$ | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Midnight |
| 2 PM | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Mid. night | 1 AM |
| 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Midnight | $1 A M$ | 2 AM |
| 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Mid. night | $1 A M$ | 2 AM | 3 AM |
| 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Midnight | 1 AM | 2 AM | 3 AM | 4 AM |
| 6 PM | 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Mid. night | 1 AM | 2 AM | 3 AM | $\triangle$ AM | 5 AM |
| 7 PM | 8 PM | 9 PM | 10 PM | 11 PM | Mid. nigh $\dagger$ | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | 6 AM |
| 8 PM | 9 PM | 10 PM | 11 PM | Mid. night | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | $\bigcirc$ AM | 1 AM |
| 9 PM | 10 PM | 11 PM | Midnight | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | $\sigma$ AM | 7 AM | $8 A M$ |
| 10 PM | 11 PM | Midnight | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | 6 AM | 7 AM | 8 AM | 9 AM |
| 11 PM | Midnight | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | 6 AM | 7 AM | 8 AM | 9 AM | 10 AM |
| Midnight | 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | O AM | 7 AM | 8 AM | 9 AM | 10 AM | 11 AM |
| 1 AM | 2 AM | 3 AM | 4 AM | 5 AM | 6 AM | 7 AM | 8 AM | 9 AM | 10 AM | $11 A M$ | Noon |
| 2 AM | 3 AM | $\triangle$ AM | 5 AM | 6 AM | 7 AM | 8 AM | 9 AM | 10 AM | 11 AM | Noon | 1 PM |
| 3 AM | 4 AM | 5 AM | $\bigcirc$ AM | 7 AM | 8 AM | 9 AM | 10 AM | 11 AM | Noon | 1 PM | 2 PM |
| 4 AM | 5 AM | 6 AM | 7 AM | 8 AM | 9 AM | 10 AM | 11 AM | Noon | 1 PM | 2 PM | 3 PM |
| 5 AM | 6 AM | 7 AM | 8 AM | 9 AM | 10 AM | 11 AM | Noon | 1 PM | 2 PM | 3 PM | 4 PM |
| 6 AM | 7 AM | 8 AM | 9 AM | 10 AM | 11 AM | Noon | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM |
| 7 AM | 8 AM | 9 AM | 10 AM | 11 AM | Noon | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM |
| 8 AM | 9 AM | 10 AM | 11 AM | Noon | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM |
| 9 AM | 10 AM | 11 AM | Noon | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM |
| 10 AM | 11 AM | Noon | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM |
| 11 AM | Noon | 1 PM | 2 PM | 3 PM | 4 PM | 5 PM | 6 PM | 7 PM | 8 PM | 9 PM | 10 PM |

TABLE 2-10
Other Standards Stations

| Station | Location | Frequency (kHz) | Schedule (UT) |
| :---: | :---: | :---: | :---: |
| ATA | Greater Kailash | 5000 | 12 h 30 m to 3 h 30 m |
|  | New Dehli | 10,000 | continuous |
|  | India | 15,000 | 3 h 30 m to $12 \mathrm{~h} \mathrm{30m}$ |
| BPM | Pucheng | 5000 | 14h to 24h |
|  | China | 10,000 | continuous |
|  |  | 15,000 | 0 h to 14 h |
| BSF | Chung-Li | 5000 | continuous (except interruption between 35 m |
|  | Taiwan | 10,000 | and 40m) |
|  | China |  |  |
| DAM | Elmshorn | 8638.5 | 11 h 55 m to 12 h 06 m |
|  | Germany, F.R. | 16,980.4 |  |
|  |  | 4265 | 23 h 55 m to 24 h 06 m from 21 October to 29 March |
|  |  | 8638.5 |  |
|  |  | 6475.5 | 23 h 55 m to 24 h 06 m from 30 March to 20 October |
|  |  | 12,763.5 |  |
| DAN | Osterloog | 2614 | 11h 55 m to 12 h 06 m |
|  | Germany, F.R. |  | 23 h 55 m to 24 h 06 m |
| DAO | Kiel | 2775 | 11 h 55 m to 12 h 06 m |
|  | Germany, F.R. |  | 23h 55 m to 24 h 06 m |
| DCF77 | Mainflingen | 77.5 | continuous |
|  | Germany, F.R. |  |  |
| DGI | Oranienburg | 182 | 5h 59 m 30 s to 6 h 00 m |
|  | Germ. Dem. Rep. |  | 11 h 59 m 30 s to 12 h 00 m |
|  |  |  | 17 h 59 m 30 s to 18 h 00 m advanced 1 h in summer |
| EBC | San Fernando | 12,008 | 10 h 00 m to 10 h 25 m |
|  | Spain | 6840 | 10 h 30 m to 10 h 55 m |
| FFH | Ste Assise | 2500 | continuous from 8 h to 16 h 25 m except on Sunday |
|  | France |  |  |
| FTH42 | Ste Assise | 7428 | at 9 h and 21 h |
| FTK77 | France | 10,775 | at 8 h and 20h |
| FTN87 |  | 13,873 | at $9 \mathrm{~h} 30 \mathrm{~m}, 13 \mathrm{~h}, 22 \mathrm{~h} 30 \mathrm{~m}$ (may be cancelled) |
| GBR | Rugby | 16 | 2h 55m to 3h 00m |
|  | United Kingdom |  | 8 h 55 m to 9 h 00 m |
|  |  |  | 14 h 55 m to 15 h 00 m |
|  |  |  | 20 h 55 m to 21 h 00 m |
| HBG | Prangins | 75 | continuous |
|  | Switzerland |  |  |

TABLE 2-10 Cont.
Other Standards Stations

| Station | Location | Frequency ( $\mathbf{k H z}$ ) | Schedule (UT) |
| :---: | :---: | :---: | :---: |
| HLA | Taedok | 5000 | Ih to 8h |
|  | Rep. of Korea |  | Monday to Friday |
| IAM | Rome | 5000 | 7h 30 m to 8 h 30 m |
|  | Italy |  | 10 h 30 m to 11 h 30 m |
|  |  |  | except Saturday afternoon, Sunday, and national holidays; advanced 1 h in summer |
| IBF | Torino | 5000 | during 15 m preceding $7 \mathrm{~h}, 9 \mathrm{~h}, 10 \mathrm{~h}, 11 \mathrm{~h}, 12 \mathrm{~h}, 13 \mathrm{~h}$, |
|  | Italy |  | $14 \mathrm{~h}, 15 \mathrm{~h}, 16 \mathrm{~h}, 17 \mathrm{~h}, 18 \mathrm{~h}$, advanced by 1 h in summer |
| JG2AS | Sanwa | 40 | continuous, except interruptions during |
|  | Ibaraki |  | communications |
|  | Japan |  |  |
| JJY | Sanwa | 2500 | continuous, except interruption between 35 m and |
|  | Ibaraki | 5000 | 39m |
|  | Japan | 8000 |  |
|  |  | 10,000 |  |
|  |  | 15,000 |  |
| L.OL. 1 | Buenos-Aires | 5000 | Ilh to $12 \mathrm{~h}, 14 \mathrm{~h}$ to $15 \mathrm{~h}, 17 \mathrm{~h}$ to $18 \mathrm{~h}, 20 \mathrm{~h}$ to $2 \mathrm{lh}, 23 \mathrm{~h}$ |
|  | Argentina | 10,000 | to 24 h |
|  |  | 15,000 |  |
| LOL 2 | Buenos-Aires | 4856 | 1h, 13h, 21h |
| LOL3 | Argentina | 8030 |  |
|  |  | 17,180 |  |
| MSF |  | 60 |  |
|  | United Kingdom |  | maintenance from 10 h 0 m to 14 h 0 m on the first Tuesday in each month |
| MSF | Rugby | 2500 | between minutes 0 and 5, 10 and 15, 20 and 25, |
|  | United Kingdom | 5000 | 30 and 35,40 and 45,50 and 55 |
|  |  | 10,000 |  |
| OLB5 | Poděbrady | 3170 | continuous except from 6 h to 12 h on the first |
|  | Czechoslovakia |  | Wednesday of every month |
| OMA | Liblice | 50 | continuous except from 6 h to 12 h on the first |
|  | Czechoslovakia |  | Wednesday of every month emitted from Poděbrady with reduced power |
| OMA | Liblice | 2500 | continuous except from 6 h to 12 h on the first |
|  | Czechoslovakia |  | Wednesday of every month |
| PPE | Rio-de-Janeiro | 8721 | Oh $30 \mathrm{~m}, 11 \mathrm{~h} 30 \mathrm{~m}, 13 \mathrm{~h} 30 \mathrm{~m}, 19 \mathrm{~h} 30 \mathrm{~m}, 20 \mathrm{~h} 30 \mathrm{~m}$, |
|  | Brazil |  | $23 \mathrm{~h} \mathrm{30m}$ |

TABLE 2-10 Cont.
Other Standards Stations

| Station | Location | Frequency (kHz) | Schedule (LT) |
| :---: | :---: | :---: | :---: |
| PPR | Rio-de-Janeiro Brazil | 435 4244 8634 13,105 $17,194.4$ 22,603 | 1h $30 \mathrm{~m}, 14 \mathrm{~h} 30 \mathrm{~m}, 2 \mathrm{~h} 30 \mathrm{~m}$ |
| RBU | Moscow U.S.S.R. | $66^{2 / 3}$ | continuous |
| RCH | Tashkent U.S.S.R. | $\begin{array}{r} 2,500 \\ 10,000 \end{array}$ | between minutes 0 m and $10 \mathrm{~m}, 30 \mathrm{~m}$ and 40 m 0 h to $3 \mathrm{~h} 40 \mathrm{~m}, 5 \mathrm{~h} 30 \mathrm{~m}$ to 23 h 40 m <br> 5 h 00 m to 13 h 10 m <br> 10 h to 13 h 10 m |
| RID | Irkutsk U.S.S.R. | $\begin{array}{r} 5004 \\ 10,004 \\ 15,004 \end{array}$ | the station simultaneously operates on three frequencies between minutes 20 m and $30 \mathrm{~m}, 50 \mathrm{~m}$ and 60 m |
| RTA | Novosibirsk U.S.S.R. | $\begin{aligned} & 10,000 \\ & 15,000 \end{aligned}$ | between 0 m and $10 \mathrm{~m}, 30 \mathrm{~m}$ and 40 m 0 h to 5 h 10 m <br> 14h to 23 h 40 m <br> 6 h 30 m to 13 h 10 m |
| RTZ | Irkutsk U.S.S.R. | 50 | between 0 m and 5 m , <br> from 0 h to 20 h 5 m , ending 22 h to 23 h 5 m in winter from 0 h to 19 h 5 m and 21 h to 23 h 5 m in summer |
| RWM | Moscow U.S.S.R. | $\begin{array}{r} 4996 \\ 9996 \\ 14,996 \end{array}$ | the station simultaneously operates on three frequencies between 10 m and $20 \mathrm{~m}, 40 \mathrm{~m}$ and 50 m |
| UNW3 | Molodechno U.S.S.R. | 25 | from 7 h 43 m to 7 h 52 m and 19 h 43 m to 19 h 52 m in winter <br> from 7 h 43 m to 7 h 52 m and 20 h 43 m to 20 h 52 m in summer |
| UPD8 | Arkhangelsk U.S.S.R. | 25 | from 8 h 43 m to 8 h 52 m and 11 h 43 m to 11 h 52 m |
| UQC3 | Chabarovsk U.S.S.R. | 25 | from 0 h 43 m to $0 \mathrm{~h} 52 \mathrm{~m}, 6 \mathrm{~h} 43 \mathrm{~m}$ to 6 h 52 m , and 17 h 43 m to 17 h 52 m in winter from 2 h 43 m to $2 \mathrm{~h} 52 \mathrm{~m}, 6 \mathrm{~h} 43 \mathrm{~m}$ to 6 h 52 m , and 18 h 43 m to 18 h 52 m in summer |
| USB2 | Frunze U.S.S.R. | 25 | from 4 h 43 m to $4 \mathrm{~h} 52 \mathrm{~m}, 9 \mathrm{~h} 43 \mathrm{~m}$ to 9 h 52 m , and 21 h 43 m to 21 h 52 m in winter <br> from 4 h 43 m to $4 \mathrm{~h} 52 \mathrm{~m}, 10 \mathrm{~h} 43 \mathrm{~m}$ to 10 h 52 m , and 22 h 43 m to 22 h 52 m in summer |

## Constants and Standards

TABLE 2-10 Cont.
Other Standards Stations

| Station | Incation | Frequency (kHz) | Schedule (UT) |
| :---: | :---: | :---: | :---: |
| UTR3 | Gorki <br> U.S.S.R. | 25 | from 5 h 43 m to $5 \mathrm{~h} 52 \mathrm{~m}, 13 \mathrm{~h} 43 \mathrm{~m}$ to 13 h 52 m , and 18 h 43 m to 18 h 52 m in winter from 7 h 43 m to $7 \mathrm{~h} 52 \mathrm{~m}, 14 \mathrm{~h} 43 \mathrm{~m}$ to 14 h 52 m , and 19 h 43 m to 19 h 52 m in summer |
| VNG | Lyndhurst <br> Australia | $\begin{array}{r} 4500 \\ 7500 \\ 12,000 \end{array}$ | 9 h 45 m to 21 h 30 m continuous except 22 h 30 m to 22 h 45 m 21 h 45 m to 9 h 30 m |
| Y 3S | Nauen <br> Germ. Dem. Rep. | 4525 | continuous except from 8 h 15 m to 9 h 45 m for maintenance if necessary |
| YVTO | Caracas <br> Venezuela | 6100 | continuous |
| 7.UO | Olifantsfontein South Africa | $\begin{aligned} & 2500 \\ & 5000 \end{aligned}$ | 18h to 4 h continuous |
| ZUO | Johannesburg South Africa | 100,000 | continuous |

## FREQUENCY AND POWER OPERATING TOLERANCES

## AM Broadcast

The operating frequency tolerance of each station shall be maintained within $\pm$ 20 Hz of the assigned frequency.

The operating power of each AM broadcast station shall be maintained as near as practicable to the licensed power and shall not exceed the limits of $5 \%$ above and $10 \%$ below the licensed power except in emergencies.

## FM Broadcast

Operating frequency tolerance of each station shall be maintained within $\pm 2000$ Hz of the assigned center frequency.

The operating power of each station shall be maintained as near as practicable to
the authorized operating power and shall not exceed the limits of $5 \%$ above and $10 \%$ below the authorized power except in emergencies.

## TV Broadcast

The carrier frequency of the visual transmitter shall be maintained within $\pm$ 1000 Hz of the authorized carrier frequency.

The center frequency of the aural transmitter shall be maintained $4.5 \mathrm{MHz} \pm 1000$ Hz above the visual carrier frequency.

The peak power shall be monitored by a peak-reading device that reads proportionally to voltages, current, or power in the radiofrequency line. The operating power as so monitored shall be maintained as near as practicable to the authorized operating power and shall not exceed the limits of $10 \%$ above and $20 \%$ below the authorized power except in emergencies.

The operating power of the aural transmitter shall be maintained as near as practicable to the authorized operating power and shall not exceed the limits of $10 \%$ above and $20 \%$ below the authorized power except in emergencies.

## TABLE 2-11

Power Limits of Personal Radio Services Stations

| Class of station | Maximum <br> transmitter <br> output power (W) |
| :--- | :---: |
| general mobile radio service <br> remote control (R/C) <br> service- 27.255 MHz | 50 |
| remote control (R/C) |  |
| service-26.995-27.195 | $25^{*}$ |
| MHz <br> remote control (R/C) <br> service-72-76 MHz <br> citizens band (CB) radio <br> service-carrier (where <br> applicable) | 4 |
| citizens band (CB) radio <br> service-peak envelope <br> power (where applicable) | 0.75 |

*A maximum transmitter output of 25 W is permitted on 27.255 MHz only.

TABLE 2-12
Frequency Tolerances of Personal Radio Services Stations

|  | Frequency tolerance (\%) |  |
| :---: | :---: | :---: |
| Class of station | Fixed and base | Mobile |
| general radio service <br> remote control (R/C) <br> service <br> citizens band (CB) service | 0.00025 | 0.0005 |

[^2]
## Industrial Radio Service

The carrier frequency of stations operating below 220 MHz in the Industrial Radio Service shall be maintained within $\pm$ $0.01 \%$ of the authorized power for stations of 3 W or less and within $\pm 0.005 \%$ for stations with an authorized power of more than 3 W . The frequency tolerance of Industrial Radio Service stations operating between 220 and 1000 MHz is specified in the station authorization.

## Personal Radio Service (CB)

The maximum power at the transmitter output terminals and delivered to the antenna, antenna transmission line, or other impedance-matched radiofrequency load shall not exceed the values in Table 2-11 under any condition of modulation.

The carrier frequency of a station in this service shall be maintained within the percentages of authorized frequency shown in Table 2-12.

The assigned channel frequencies and upper and lower tolerance limits for citizens band (CB) radio service are listed in Table 2-13.

## COMMERCIAL OPERATOR LICENSES

## Types of Licenses

Currently, the FCC issues six types of commercial radio licenses and two types of endorsements. They are:

1. Restricted Radiotelephone Operator
Permit. A Restricted Radiotelephone

## TABLE 2-13 <br> Citizens Band Frequencies and Upper and Lower Tolerances

| Channel | Assigned <br> frequency <br> (MHz) | Lower <br> limit <br> (MHz) | Upper <br> limit <br> (MHz) |
| :---: | :---: | :---: | :---: |
| 1 | 26.965000 | 26.963651 | 26.966348 |
| 2 | 26.975000 | 26.973651 | 26.976348 |
| 3 | 26.985000 | 26.983650 | 26.986349 |
| 4 | 27.005000 | 27.003649 | 27.006350 |
| 5 | 27.015000 | 27.013649 | 27.016450 |
| 6 | 27.025000 | 27.023648 | 27.026351 |
| 7 | 27.035000 | 27.033648 | 27.036351 |
| 8 | 27.055000 | 27.053647 | 27.056352 |
| 9 | 27.065000 | 27.063646 | 27.066353 |
| 10 | 27.075000 | 27.073646 | 27.076353 |
| 11 | 25.085000 | 27.083645 | 27.086354 |
| 12 | 27.105000 | 27.103644 | 27.106355 |
| 13 | 27.115000 | 27.113644 | 27.116356 |
| 14 | 27.125000 | 27.123643 | 27.126356 |
| 15 | 27.135000 | 27.133643 | 27.136356 |
| 16 | 27.155000 | 27.153642 | 27.156357 |
| 17 | 27.165000 | 27.163641 | 27.166358 |
| 18 | 27.175000 | 27.173641 | 27.176359 |
| 19 | 27.185000 | 27.183640 | 27.186359 |
| 20 | 27.205000 | 27.203639 | 27.206360 |
| 21 | 27.215000 | 27.213639 | 27.216360 |
| 22 | 27.225000 | 27.223638 | 27.226361 |
| 23 | 27.255000 | 27.253637 | 27.256363 |
| 24 | 27.235000 | 27.233638 | 27.236362 |
| 25 | 27.245000 | 27.243637 | 27.246362 |
| 26 | 27.265000 | 27.263636 | 27.266364 |
| 27 | 27.275000 | 27.273636 | 27.276364 |
| 28 | 27.285000 | 27.283635 | 27.286365 |
| 29 | 27.295000 | 27.293635 | 27.296365 |
| 30 | 27.305000 | 27.303634 | 27.306366 |
| 31 | 27.315000 | 27.313634 | 27.316366 |
| 32 | 27.325000 | 27.323633 | 27.326366 |
| 33 | 27.335000 | 27.333633 | 27.336367 |
| 34 | 27.345000 | 27.343632 | 27.346368 |
| 35 | 27.355000 | 27.353632 | 27.356368 |
| 36 | 27.365000 | 27.363631 | 27.36369 |
| 37 | 27.375000 | 27.373631 | 27.376369 |
| 38 | 27.385000 | 27.383630 | 27.38369 |
| 39 | 27.395000 | 27.393639 | 27.39370 |
| 40 | 27.405000 | 27.403629 | 27.406370 |
|  |  |  |  |
|  |  |  |  |

Operator Permit allows operation of most aircraft and aeronautical ground
stations, maritime radiotelephone stations on pleasure vessels (other than those carrying more than six passengers for hire), and most VHF marine coast and utility stations. It is the only type of license required for transmitter operation, repair, and maintenance (including acting as chief operator) of all types of AM, FM, TV, and international broadcast stations.

There is no examination for this license. To be eligible for it you must:

Be at least 14 years old
Be a legal resident of (eligible for employment in) the U.S. or (if not so eligible) hold an aircraft pilot certificate valid in the U.S. or an FCC radio station license in your name

Be able to speak and hear
Be able to keep at least a rough written log

Be familiar with provisions of applicable treaties, laws, and rules that govern the radio station you will operate

A Restricted Radiotelephone Operator License is normally valid for the lifetime of the holder.
2. Marine Radio Operator Permit. A Marine Radio Operator Permit is required to operate radiotelephone stations on board certain vessels sailing the Great Lakes, any tidewater, or the open sea. It is also required to operate certain aviation radiotelephone stations, and certain maritime coast radiotelephone stations. It does not
authorize the operation of AM, FM, or TV broadcast stations.

To be eligible for this license, you must:

Be a legal resident of (eligible for employment in) the U.S.

Be able to receive and transmit spoken messages in English

Pass a written examination covering basic radio law and operating procedures

The Marine Operator Permit is normally valid for a renewable fiveyear term.
3. General Radiotelephone Operator License. A General Radiotelephone Operator License is required for persons responsible for internal repairs, maintenance, and adjustment of FCC licensed radiotelephone transmitters in the Aviation, Maritime, and International Public Fixed radio services. It is also required for operation of maritime land radio transmitters operating with more than 1500 W of peak envelope power and maritime mobile (ship) and aeronautical transmitters with more than 1000 W of peak envelope power.

To be eligible for this license, you must:

Be a legal resident of (eligible for employment in) the U.S.

Be able to receive and transmit spoken messages in English

Pass a written examination covering basic radio law, operating procedures, and basic electronics

The General Radiotelephone

Operator License is normally valid for the lifetime of the operator.
4. Third Class Radiotelegraph Operator Certificate. A Third Class Radiotelegraph Operator Certificate is required to operate certain coast radiotelegraph stations. It also conveys all the authority of both the Restricted Radiotelephone Operator Permit and the Marine Radio Operator Permit.

To be eligible for this license, you must:

Be a legal resident of (eligible for employment in) the U.S.

Be able to receive and transmit spoken messages in English

Pass Morse code examinations at 16 code groups per minute and 20 words per minute plain language (receive and transmit by hand)

Pass a written examination covering basic radio law, basic operating procedures (telephony), and basic operating procedures (telegraphy)

The Third Class Radiotelegraph Operator Certificate is normally valid for a renewable five-year term.
5. Second Class Radiotelegraph Operator Certificate. A Second Class Radiotelegraph Operator Certificate is required to operate ship and coast radiotelegraph stations in the maritime services and to take responsibility for internal repairs, maintenance, and adjustments of any FCC-licensed radiotelegraph transmitter other than an amateur radio transmitter. It also conveys all of the authority of the Third Class Radiotelegraph Operator Certificate.

To be eligible for this license, you must:

Be a legal resident of (eligible for employment in) the U.S.

Be able to receive and transmit spoken messages in English

Pass Morse code examinations at 16 code groups per minute and 20 words per minute plain language (receive and transmit by hand)

Pass a written examination covering basic radio law, basic operating procedures (telephony), basic operating procedures (telegraphy), and electronics technology as applicable to radiotelegraph stations

The Second Class Radiotelegraph Operator Certificate is normally valid for a renewable five-year term.

## 6. First Class Radiotelegraph Operator

 Certificate. A First Class Radiotelegraph Operator Certificate is required only for those who serve as the chief radio operator on U.S. passenger ships. It also conveys all of the authority of the Second Class Radiotelegraph Operator Certificate.To be eligible for this license, you must:

Be at least 21 years old
Have at least one year of experience in sending and receiving public correspondence by radiotelegraph at ship stations, coast stations, or both

Be a legal resident of (eligible for employment in) the U.S.

Be able to receive and transmit spoken messages in English

Pass Morse code examinations at 20 code groups per minute and 25 words per minute plain language (receive and transmit by hand)

Pass a written examination covering basic radio law, basic operating procedures (telephony), basic operating procedures (telegraphy), and electronics technology as applicable to radiotelegraph stations

The First Class Radiotelegraph Operator Certificate is normally valid for a renewable five-ycar term.
7. Ship Radar Endorsement. The Ship Radar Endorsement is required to service and maintain ship radar equipment.

To be eligible for this endorsement, you must:

Hold a valid First or Second Class Radiotelegraph Operator Certificate or a General Radiotelephone Operator License

Pass a written examination covering the technical fundamentals of radar and radar maintenance techniques
8. Six-Months Service Endorsement. The Six-Months Service Endorsement is required to permit the holder to serve as the sole radio operator on board large U.S. cargo ships.

To be eligible for this endorsement, you must:

> Hold a valid First Class or Second Class Radiotelegraph Operator Certificate

Have at least six months of satisfactory service as a radio officer on board a ship (or ships) of the U.S. equipped with a radiotelegraph station in compliance with Part II of Title III of the Communications Act of 1934

Have held a valid First Class or Second Class Radiotelegraph Operator Certificate while obtaining the six months of service

Have been licensed as a radio officer by the U.S. Coast Guard, in accordance with the Act of May 12, 1948 (46 U.S.C. 229 a-h), while obtaining the six months of service

## Discontinued Licenses

The FCC no longer issues the Radiotelephone First or Second Class Operator Licenses, the Radiotelephone Third Class Operator Permit, the Broadcast Endorsement or the Aircraft Radiotelegraph Endorsement. Holders of such licenses should follow the following instructions pertaining to the license held when it is time to renew their license.

1. Radiotelephone First Class Operator License. The Radiotelephone First Class Operator License have been abolished and the requirements for holding such licenses to operate and maintain broadcast transmitters have been eliminated. Persons holding such a license will be issued a General Radiotelephone Operator License when they apply at renewal.
2. Radiotelephone Second Class Operator License. The Radiotelephone Second Class Operator License has been
renamed the General Radiotelephone Operator License. Persons holding the Radiotelephone Second Class Operator License will be issued a General Radiotelephone Operator License when they apply for renewal.
3. Radiotelephone Third Class Operator Permit. The Radiotelephone Third Class Operator Permit has been converted to the Marine Radio Operator Pemit. The requirement for its use with a Broadcast Endorsement has been abolished.

If you are employed as a radio operator aboard vessels or aeronautical stations where its use is required, request issuance of a Marine Radio Operator Permit at time of renewal. (No examination is necessary if your Radiotelephone Third Class Operator Permit expired not more than five years before application.)

If you hold a Radiotelephone Third Class Operator Permit With Broadcast Endorsement for operating a broadcast station, apply for a Restricted Radiotelephone Operator Permit at time for renewal.

If you operate stations that require you to hold a Marine Operator Permit and you also operate the transmitter of an AM, FM, or TV broadcast station, you should apply for both a Marine Operator Permit and a Restricted Radiotelephone Operator Permit at time of renewal.
4. Broadcast Endorsement. The Broadcast Endorsement to the Radiotelephone Third Class Operator Permit formerly required for operations of some classes of broadcast transmitter has been abolished along with the requirement
for a Radiotelephone Third Class Operator Permit. Holders of this type of license and endorsement who have been using it for broadcast transmitter operation should apply for a Restricted Radiotelephone Operator Permit during the last year of the license term.
5. Aircraft Radiotelegraph Endorsement. The use of radiotelegraphy aboard aircraft has been discontinued and the Aircraft Radiotelegraph Endorsement has been abolished. If you hold a license with such an endorsement, the endorsement will be eliminated at renewal.

## Examination Elements

Written examinations are composed of questions from various categories called elements. These elements, and the types of questions in cach, are:

Element 1. Basic Marine Radio Law. Provisions of laws, treaties, and regulations with which every operator in the maritime radio services should be familiar.

Element 2. Busic Operating Practice. Radio operating procedures and practices generally followed or required in communicating by radiotelephone in the maritime radio services.

## Element 3. General Radiotelephone.

 Provisions of laws, treatics, and regulations with which every radio operator in the maritime radio service should be familiar. Radio operating practices generally followed or required in communicating by radiotelephone in the maritime radio services. Technical matters including fundamentals of electronics technology and maintenance techniques as necessary for repair and maintenance of radio transmitters and receivers.Element 4. Radiotelegraph Operating Practice. Radio-operating procedure and practices generally followed or required in operation of shipboard radiotelegraph stations.

Element 5. Advanced Radiotelegraph. Technical, legal, and other matters, including clectronics technology and radio maintenance and repair techniques applicable to all classes of radiotelegraph stations.

Element 6. Ship Radar Techniques. Specialized theory and practice applicable to the proper installation, servicing, and maintenance of ship radar equipment.

## AMATEUR OPERATOR PRIVILEGES

## Examination Elements

Examinations for amateur operator privileges are composed of questions from various catcgories, called elements. The various elements and their requirements are:

Element 1(A). Beginner's Code Test. Code test at 5 words per minute.

Element 1(B). General Code Test. Code test at 13 words per minute.

Element 1(C). Expert's Code Test. Code test at 20 words per minute.

Element 2. Basic Law. Rules and regulations essential to beginners' operation, including sufficient elementary radio theory to understand these rules.

Element 3. General Regulations. Amateur radio operation and apparatus and provisions of treaties, statutes, and rules and regulations affecting all amatcur stations and operators.

Element 4(A). Intermediate Amateur Practice. Involving intermediate level for general
amateur practice in radio theory and operation as applicable to modern amateur techniques, including-but not limited to-radiotelephony and radiotelegraphy.

Element 4(B). Advanced Amateur Practice. Advanced radio theory and operation applicable to modern amateur techniques, including-but not limited to-radiotelephony, radiotelegraphy, and transmission of energy for (1) measurements and observations applied to propagation, (2) radio control of remote objects, and (3) similar experimental purposes.

## Examination Requirements

An applicant for an original license must be a U.S. citizen or other U.S. national and will be required to pass examinations as follows:

1. Amateur Extra Class. Elements 1(C), 2, 3, 4(A), and 4(B).
2. Advanced Class. Elements $1(\mathrm{~B}), 2,3$, and 4(A).
3. General Class. Elements 1(B), 2, and 3.
4. Technician Class. Elements 1 (A), 2, and 3.
5. Novice Class. Elements 1(A) and 2.

Note. Since January 1, 1985 all examinations for amateur radio licenses are given by volunteer amateur examiners. Complete details are given in the FCC rules.

## AMATEUR ("HAM") BANDS

The frequency bands for various amateur licenses follow.

1. Amateur Extra Class. All amateur bands, including these privileged frequencies:

$$
\begin{gathered}
3500-3525 \mathrm{kHz} \\
3775-3800 \mathrm{kHz} \\
7000-7025 \mathrm{kHz} \\
14,000-14,025 \mathrm{kHz} \\
14,150-14,175 \mathrm{kHz} \\
21,000-21,025 \mathrm{kHz} \\
21,200-21,225 \mathrm{kHz}
\end{gathered}
$$

2. Advanced Class. All amateur bands except those frequencies reserved for Amateur Extra Class, including these privileged frequencies:

$$
\begin{gathered}
3800-3890 \mathrm{kHz} \\
7150-7225 \mathrm{kHz} \\
14,175-14,350 \mathrm{kHz} \\
21,225-21,300 \mathrm{kHz}
\end{gathered}
$$

3. General Class. All amateur bands except those frequencies reserved for Amateur Extra Class and Advanced Class.
4. Technician Class. All authorized privileges on amatcur frequency bands above 50 MHz and those assigned to the Novice Class.
5. Novice Class. The following selected bands, using only Type A1 emission.

$$
\begin{aligned}
& 3700-3750 \mathrm{kHz} \\
& 7100-7150 \mathrm{kHz} \\
& 21.10-21.20 \text { and } 28.1-28.2 \mathrm{MHz}
\end{aligned}
$$

The DC power input to the stage supplying power to the antenna shall not exceed 250 W , and the transmitter shall be crystal controlled.

The various bands of frequencies used by amateur radio operators ("hams") are usually referred to in meters instead of the actual frequencies. The number of meters approximates the wavelength at the band of frequencies being designated. The meter

TABLE: 2-14
"Ham" Bands

| Frequency band limits | Types of emission | Band |
| :---: | :---: | :---: |
| $1800-2000 \mathrm{kHz}$. | A1, A3 | 160 |
| $3500-4000 \mathrm{kHz}$ | A1 | 80 |
| $3500-3750 \mathrm{kHz}$ | F1 | 80 |
| $3750-4000 \mathrm{kHz}$. | A3, A4, A5, F3, F4, F5 | 80 |
| 5167.5 kHz | A3A, A3J | 80 |
| $7000-7300 \mathrm{kHz}$ | Al | 40 |
| $7000-7150 \mathrm{kHz}$ | F1 | 40 |
| $7075-7100 \mathrm{kHz}$ | A3, F3 | 40 |
| $7150-7300 \mathrm{kHz}$ | A3, A4, A5, F3, F4, F5 | 40 |
| $10,100-10,109 \mathrm{kHz}$. | A1, FI | 30 |
| 10, 115-10, 150 kHz | A1, FI | 30 |
| $14,000-14,350 \mathrm{kHz}$. | A1 | 20 |
| $14,000-14,150 \mathrm{kHz}$ | F1 | 20 |
| $14,150-14,350 \mathrm{kHz}$ | A3, A4, A5, F3, F4, F5 | 20 |
| $21.000-21.450 \mathrm{MHz}$ | A1 | 15 |
| $21.000-21.200 \mathrm{MHz}$ | F1 | 15 |
| $21.200-21.450 \mathrm{MHz}$ | A3, A4, A5, F3, F4, F5 | 15 |
| $28.000-29.700 \mathrm{MHz}$ | A1 |  |
| $28.000-28.500 \mathrm{MHz}$ | F1 |  |
| $28.500-29.700 \mathrm{MHz}$ | A3, A4, A5, F3, F4, F5 |  |
| $50.000-54.000 \mathrm{MHz}$. | A2, A3, A4, A5, F1, F2, F3, F4, F5 |  |
| $51.000-54.000 \mathrm{MHz}$ | A0, FO |  |
| $144-140 \mathrm{MHz}$ | A1 | 2 |
| $144.100-148.000) \mathrm{MHz}$ | A0, A2, A3, A4, A5, F0, F1, F2, F3, F4, F5 | 2 |
| $220-225 \mathrm{MHz}$ | A0, A1, A2, A3, A4, A5, F0, F1, F2, F3, F4, F5 | $11 / 4$ |
| $420-450 \mathrm{MHz}$ | $\mathrm{A} 0, \mathrm{~A} 1, \mathrm{~A} 2, \mathrm{~A} 3, \mathrm{~A} 4, \mathrm{~A} 5, \mathrm{~F} 0, \mathrm{~F}, \mathrm{~F} 2, \mathrm{~F} 3, \mathrm{~F} 4, \mathrm{~F} 5$ | $3 / 4$ |
| $1215-1300 \mathrm{MHz}$ | $\mathrm{A} 0, \mathrm{~A} 1, \mathrm{~A} 2, \mathrm{~A} 3, \mathrm{~A} 4, \mathrm{~A} 5, \mathrm{~F} 0, \mathrm{~F} 1, \mathrm{~F} 2, \mathrm{~F} 3, \mathrm{~F} 4, \mathrm{~F} 5$ |  |
| $2300-2450 \mathrm{MHz}$ | A0, A1, A2, A3, A4, A5, F0, F1, F2, F3, F4, F5 |  |
| $3300-3500 \mathrm{MHz}$ | A0, A1, A2, A3, A4, A5, F0, F1, F2, F3, F4, F5, P |  |
| $5650-5925 \mathrm{MHz}$ | A0, A1, A2, A3, A4, A5, F0, F1, F2, F3, F4, F5, P |  |
| $10.0-10.5 \mathrm{GHz}$ | A0, A1, A2, A3, A4, A5, F0, F1, F2, F3, F4, F5 |  |
| $24.0-24.25 \mathrm{GHz}$ | A0, A1, A2, A3, A4, A5, F1, F2, F3, F4, F5, P |  |
| 48-50, $71-76 \mathrm{GHz}$ | A0, A1, A $2, \mathrm{~A} 3, \mathrm{~A} 4, \mathrm{~A} 5, \mathrm{~F} 0, \mathrm{~F} 1, \mathrm{~F} 2, \mathrm{~F} 3, \mathrm{~F} 4, \mathrm{~F} 5, \mathrm{P}$ |  |
| Above 300 GHz | A0, A1, A2, A3, A4, A5, F0, F1, F2, F3, F4, F5, P |  |

bands and their frequency limits are given in Table 2-14.

Note. Frequencies between 220 and 225 MHz are sometimes referred to as $11 / 4 \mathrm{~m}$ and between 420 and 450 MHz as $3 / 4 \mathrm{~m}$.

The maximum DC plate input power in watts for the $160-\mathrm{m}$ band ( $1.8-2.0 \mathrm{MHz}$ ) is shown in Table 2-15 for all states and U.S. possessions.

## TYPES OF EMISSIONS

Emissions are classified according to their modulation, type of transmission, and supplementary characteristics. These classifications are given in Table 2-16. When a full designation of the emissions-including bandwidth-is necessary, the symbols in Table 2-16 are prefixed by a number indicating the bandwidth in kilohertz. Below 10 kHz , this number is given to two significant figures.

TABLE 2-15
Maximum Power for the $160-\mathrm{m}$ Band

Maximum DC: plate input power in watts

|  | $\begin{gathered} 1800-1825 \\ k H z \end{gathered}$ | $\begin{gathered} 1825-1850 \\ k H z \end{gathered}$ | $\begin{gathered} 1850-1875 \\ \mathrm{kHz} \end{gathered}$ | $\begin{gathered} 1875-1900 \\ k H z \end{gathered}$ | $\begin{gathered} 1900-1925 \\ k H z \end{gathered}$ | $\begin{gathered} 1925-1950 \\ k H z \end{gathered}$ | $\begin{gathered} 1950-1975 \\ \mathrm{kHz} \end{gathered}$ | $\begin{gathered} 1975-2000 \\ k H z \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Area | Day/Vight | Day/Night | Day/Night | Day/Night | Day/Night | Day/Vight | Day/Night | Day/Night |
| Alabama | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 100/25 | 500/100 |
| Alaska | 1000/200 | 500/100 | 500/100 | 100/25 | 0 | 0 | 0 | 0 |
| Arizona | 1000/200 | 500/100 | 500/100 | 0 | 0 | 0 | 0 | 0 |
| Arkansas | 1000/200 | 500/100 | 100/25 | 0 | 0 | 100/25 | 100/25 | 500/100 |
| California | 1000/200 | 500/100 | 500/100 | 100/25 | 0 | 0 | 0 | 0 |
| Colorado | 1000/200 | 500/100 | 200/50 | 0 | 0 | 0 | 0 | 200/50 |
| Connecticut | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 0 |
| Delaware | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 100/25 |
| District of Columbia | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 100/25 |
| Florida | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 100/25 | 500/100 |
| Georgia | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 200/50 |
| Hawaii | 0 | 0 | 0 | 0 | 200/50 | 100/25 | 100/25 | 500/100 |
| Idaho | 1000/200 | 500/100 | 500/100 | 100/25 | 100/25 | 100/25 | 100/25 | 500/100 |
| Illinois | 1000/200 | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 200/50 |
| Indiana | 1000/200 | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 200/50 |
| Iowa | 1000/200 | 500/100 | 200/50 | 0 | 0 | 100/25 | 100/25 | 500/100 |
| Kansas | 1000/200 | 500/100 | 100/25 | 0 | 0 | 100/25 | 100/25 | 500/100 |
| Kentucky | 1000/200 | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 200/50 |
| Louisiana | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 100/25 | 500/100 |
| Maine | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 0 |
| Maryland | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 100/25 |
| Massachusetts | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 0 |
| Michigan | 1000/200 | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 100/25 |
| Minnesota | 1000/200 | 500/100 | 500/100 | 100/25 | 100/25 | 100/25 | 100/25 | 500/100 |
| Mississippi | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 100/25 | 500/100 |
| Missouri | 1000/200 | 500/100 | 100/25 | 0 | 0 | 100/25 | 100/25 | 500/100 |
| Montana | 1000/200 | 500/100 | 500/100 | 100/25 | 100/25 | 100/25 | 100/25 | 500/100 |
| Nebraska | 1000/200 | 500/100 | 200/50 | 0 | 0 | 100/25 | 100/25 | 500/100 |
| Nevada | 1000/200 | 500/100 | 500/100 | 100/25 | 0 | 0 | 0 | 0 |
| New Hampshire | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 0 |
| New Jersey | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 0 |
| New Mexico | 1000/200 | 500/100 | 100/25 | 0 | 0 | 100/25 | 500/100 | 1000/200 |
| New York | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 0 |
| North Carolina | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 100/25 |
| North Dakota | 1000/200 | 500/100 | 500/100 | 100/25 | 100/25 | 100/25 | 100/25 | 500/100 |
| Ohio | 1000/200 | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 100/25 |
| Oklahoma | 1000/200 | 500/100 | 100/25 | 0 | 0 | 100/25 | 100/25 | 500/100 |
| Oregon | 1000/200 | 500/100 | 500/100 | 100/25 | 0 | 0 | 0 | 0 |
| Pennsylvania | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 0 |
| Rhode Island | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 0 |
| South Carolina | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 200/50 |
| South Dakota | 1000/200 | 500/100 | 500/100 | 100/25 | 100/25 | 100/25 | 100/25 | 500/100 |
| Tennessee | 1000/200 | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 200/50 |
| Texas | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 200/50 |
| Utah | 1000/200 | 500/100 | 500/100 | 100/25 | 100/25 | 0 | 0 | 100/25 |
| Vermont | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 0 |
| Virginia | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 100/25 |

## Constants and Standards

TABLE 2-15 Cont.
Maximum Power for the $\mathbf{1 6 0}-\mathrm{m}$ Band

| Area | Maximum DC plate input power in watts |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} 1800-1825 \\ k H z \end{gathered}$ | $\begin{gathered} 1825-1850 \\ k H z \end{gathered}$ | $\begin{gathered} 1850-1875 \\ k H z \end{gathered}$ | $\begin{gathered} 1875-1900 \\ k H z \end{gathered}$ | $\begin{gathered} 1900-1925 \\ k H z \end{gathered}$ | $\begin{gathered} 1925-1950 \\ \mathrm{kHz} \end{gathered}$ | $\begin{gathered} 1950-1975 \\ k H z \end{gathered}$ | $\begin{gathered} 1975-2000 \\ k H z \end{gathered}$ |
|  | Day/Night | Day/Night | Day/Night | Day/Night | Day/Night | Day/Night | Day/Night | Day/Night |
| Washington | 1000/200 | 500/100 | 500/100 | 100/25 | 0 | 0 | 0 | 0 |
| West Virginia | 1000/200 | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 100/25 |
| Wisconsin | 1000/200 | 500/100 | 200/50 | 0 | 0 | 0 | 0 | 200/50 |
| Wyoming | 1000/200 | 500/100 | 500/100 | 100/25 | 100/25 | 0 | 0 | 200/50 |
| Puerto Rico | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 200/50 |
| Virgin Islands | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 200/50 |
| Swan Island | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 100/25 | 500/100 |
| Serrana Bank | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 100/25 | 500/100 |
| Roncador Key | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 100/25 | 500/100 |
| Navassa Island | 500/100 | 100/25 | 0 | 0 | 0 | 0 | 0 | 200/50 |
| Baker, Canton, Enderbury, Howland | 100/25 | 0 | 0 | 100/25 | 100/25 | 0 | 0 | 100/25 |
| Guam, Johnston, Midway | 0 | 0 | 0 | 0 | 100/25 | 0 | 0 | 100/25 |
| American Samoa | 200/50 | 0 | 0 | 200/50 | 200/50 | 0 | 0 | 200/50 |
| Wake | 100/25 | 0 | 0 | 100/25 | 0 | 0 | 0 | 0 |
| Palmyra, Jarvis | 0 | 0 | 0 | 0 | 200/50 | 0 | 0 | 200/50 |

TABLE 2-16
Types of Emission

| Type of modulation | Type of transmission | Supplementary characteristics | Symbol |
| :---: | :---: | :---: | :---: |
| 1. amplitude | absence of any modulation | - | A0 |
|  | telegraphy without the use of modulating audiofrequency (on-off keying) | - | A1 |
|  | telegraphy by the keying of a modulating audiofrequency or audiofrequencies or by the keying of the modulated emission (special case: an unkeyed modulated emission) | - | A2 |
|  |  | double sideband, full carrier | A3 |
|  | telephony | single sideband, reduced carrier | A3a |
|  |  | two independent sidebands, reduced carrier | A3b |
|  | facsimile | - | A4 |
|  | television | - | A5 |

## TABLE 2-16 Cont.

Types of Emission

| Type of modulation | Type of transmission | Supplementary characteristics | Symbol |
| :---: | :---: | :---: | :---: |
| 1. amplitude | composite transmissions, and cases not covered by the above | - | A9 |
|  | composite transmissions | reduced carrier | A9c |
| 2. frequency (or phase) modulated | absence of any modulation | - | F0 |
|  | telegraphy without the use of modulating audiofrequency (frequency shift keying) | - | F1 |
|  | telegraphy by the keying of a modulating audiofrequency or audiofrequencies or by the keying of the modulated emission (special case: an unkeyed emission modulated by audiofrequency) | - | F2 |
|  | telephony | - | F3 |
|  | facsimile | - _-_-.... - | F4 |
|  | television | - | F5 |
|  | composite transmissions and cases not covered by the above | - | F9 |
| 3. pulsed emissions | absence of any modulation-carrying information | - | P0 |
|  | telcgraphy without the use of modulating audiofrequency | - | P1 |
|  | telegraphy by the keying of a modulating audiofrequency or of the modulated pulse (special casc: an unkeyed modulated pulse) | audiofrequency or audiofrequencies modulating the pulse in amplitude | P2d |
|  |  | audiofrequency or audiofrequencies modulating the width of the pulse | P2c |
|  |  | audiofrequency or audiofrequencies modulating the phase (or position) of the pulse | P2f |
|  |  | amplitude-modulated pulse | P3d |
|  | telephony | width-modulated pulse | P3e |
|  |  | phase-(or position-)modulated pulse | P3f |
|  | composite transmissions and cases not covered by the above | - | P9 |

## TELEVISION SIGNAL STANDARDS

The signal standards for television broadcasting are given in Fig. 2-8.

Note. The standards given here are for color transmission. For monochrome transmission, the standards are the same except the color burst signal is omitted.

## Constants and Standards



B

Reference While Level


Detall Between 3.3 in $B$
C

Horizontal Dimensions Not to Scale in A, B and C

Fig. 2-8. Television signal standards.


Detail Between 44 in $B$
D


E

## NOTES

1. $H=$ time from start of one line to stort of next tine.
2. $V=$ Time from stort of one field to start of next field.
3. Leading and railing edges of vertical blanking should be compiere in less than 0.1 H .
4. Leading and trailing slopes of horizontal blanking must be steep enough to preserve minimum and maximum values of $(x-y)$ and ( $z$ ) under all conditions of picture content
5. Dimensions marked with asterisk indicate that tolerances given are permitted only for long time variations and not for successive cycles.
6. Equalizing pulse area shall be between 0.45 and 0.5 of area of a horizontal sync pulse.
7. Color burst follows each horizontal pulse, but is omitted following the equalizing pulses and during the brood vertical pulses.
8. Color burst to be omitted during monochrome transmissions
9. The burst frequency shall be 3.579545 MHz . The tolerance on the frequency shall be $\pm 0.0003 \%$ with a maximum rate of change of frequency nor to exceed $1 / 10 \mathrm{~Hz}$ per secand.
10. The horizontal scanning frequency shall be $2 / 455$ times the burst frequency.
11. The dimensions specified for the burst determine the times of storting and stopping the burst but not its phose. The color burst consists of amplitude moduration of a continuous sine wave.
12. Dimension " $P$ " represents the peak excursion of the luminance signal at blanking level but does not include the chrominance signal. Dimension " $S$ " is the sync amplitude above blanking level. Dimension " C " is the peak corrier amplitude.

Fig. 2-8. Television signal standards. Cont.

## TELEVISION CHANNEL FREQUENCIES

Table 2-17 lists the broadcast frequency limits of all television channels and the fre-
quency of the video, color, and sound carriers of each channel. The frequencies of the signals are altered on most cable systems. Table 2-18 lists the cable channel frequency assignments generally used.

TABLE 2-17
Television Channel Frequencies*

| Channel no. | Freq range | Carriers |  |  | Channel no. | Freq range | Carriers |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $1{ }^{\text {ideo }}$ | Color | Sound |  |  | Video | Color | Sound |
| 2 | 54-60 | 55.25 | 58.83 | 59.75 | 43 | 644-650 | 645.25 | 648.83 | 649.75 |
| 3 | 60-66 | 61.25 | 64.83 | 65.75 | 44 | 650-656 | 651.25 | 654.83 | 655.75 |
| 4 | 66-72 | 67.25 | 70.83 | 71.75 | 45 | 656-662 | 657.25 | 660.83 | 661.75 |
| 5 | $76-82$ | 77.25 | 80.83 | 81.75 | 46 | 662-668 | 663.25 | 666.83 | 667.75 |
| 6 | 82-88 | 83.25 | 86.83 | 87.75 | 47 | 668-674 | 669-25 | 672.83 | 673.75 |
| 7 | 174-180 | 175.25 | 178.83 | 179.75 | 48 | 674-680 | 675.25 | 678.83 | 679.75 |
| 8 | 180-186 | 181.25 | 184.83 | 185.75 | 49 | 680-686 | 681.25 | 684.83 | 685.75 |
| 9 | 186-192 | 187.25 | 190.83 | 191.75 | 50 | 686-692 | 687.25 | 690.83 | 691.75 |
| 10 | 192-198 | 193.25 | 196.83 | 197.75 | 51 | 692-698 | 693.25 | 696.83 | 697.75 |
| 11 | 198-204 | 199.25 | 202.83 | 203.75 | 52 | 698-704 | 699.25 | 702.83 | 703.75 |
| 12 | 204-210 | 205.25 | 208.83 | 209.75 | 53 | 704-710 | 705.25 | 708.83 | 709.75 |
| 13 | 210-216 | 211.25 | 214.83 | 215.75 | 54 | 710-716 | 711.25 | 714.83 | 715.75 |
| 14 | 470-476 | 471.25 | 474.83 | 475.75 | 55 | 716-722 | 717.25 | 720.83 | 721.75 |
| 15 | 476-482 | 477.25 | 480.83 | 481.75 | 56 | 722-728 | 723.25 | 726.83 | 727.75 |
| 16 | 482-488 | 483.25 | 486.83 | 487.75 | 57 | 728-734 | 729.25 | 732.83 | 733.75 |
| 17 | 488-494 | 489.25 | 492.83 | 493.75 | 58 | 734-740 | 735.25 | 738.83 | 739.75 |
| 18 | 494-500 | 495.25 | 498.83 | 499.75 | 59 | 740-746 | 741.25 | 744.83 | 745.75 |
| 19 | 500-506 | 501.25 | 504.83 | 505.75 | 60 | 746-752 | 747.25 | 750.83 | 751.75 |
| 20 | 506-512 | 507.25 | 510.83 | 511.75 | 61 | 752-758 | 753.25 | 756.83 | 757.75 |
| 21 | 512.518 | 513.25 | 516.83 | 517.75 | 62 | 758-764 | 759.25 | 762.83 | 763.75 |
| 22 | 518-524 | 519.25 | 522.83 | 523.75 | 63 | 764-770 | 765.25 | 768.83 | 769.75 |
| 23 | 524-530 | 525.25 | 528.83 | 529.75 | 64 | 770-776 | 771.25 | 774.83 | 775.75 |
| 24 | 530-536 | 531.25 | 534.83 | 535.75 | 65 | 776-782 | 777.25 | 780.83 | 781.75 |
| 25 | 536-542 | 537.25 | 540.83 | 541.75 | 66 | 782-788 | 783.25 | 786.83 | 787.75 |
| 26 | 542-548 | 543.25 | 546.83 | 547.75 | 67 | 788-794 | 789.25 | 792.83 | 793.75 |
| 27 | 548-554 | 549.25 | 552.83 | 553.75 | 68 | 794-800 | 795.25 | 798.83 | 799.75 |
| 28 | 554-560 | 555.25 | 558.83 | 559.75 | 69 | 800-806 | 801.25 | 804.83 | 805.75 |
| 29 | 560-566 | 561.25 | 564.83 | 565.75 | $70^{\dagger}$ | $806-812$ | 807.25 | 810.83 | 811.75 |
| 30 | 566-572 | 567.25 | 570.83 | 571.75 | $71^{1}$ | 812-818 | 813.25 | 816.83 | 817.75 |
| 31 | 572-578 | 573.25 | 576.83 | 577.75 | $72^{\dagger}$ | 818-824 | 819.25 | 822.83 | 823.75 |
| 32 | 578-584 | 579.25 | 582.83 | 583.75 | $73^{1}$ | 824-830 | 825.25 | 828.83 | 829.75 |
| 33 | 584-590) | 585.25 | 588.83 | 589.75 | 74 | 830-836 | 831.25 | 834.83 | 835.75 |
| 34 | 590-596 | 591.25 | 594.83 | 595.75 | $75^{\prime}$ | 836-842 | 837.25 | 840.83 | 841.75 |
| 35 | 596-602 | 597.25 | 600.83 | 601.75 | 761 | 842-848 | 843.25 | 846.83 | 847.75 |
| 36 | 602-608 | 603.25 | 606.83 | 607.75 | 771 | 848-854 | 849.25 | 852.83 | 853.75 |
| 37 | 608-614 | 609.25 | 612.83 | 613.75 | 781 | 854-860 | 855.25 | 858.83 | 859.75 |
| 38 | 614-620 | 615.25 | 618.83 | 619.75 | 791 | 860-866 | 861.25 | 864.83 | 865.75 |
| 39 | 620-626 | 621.25 | 624.83 | 625.75 | $80^{\dagger}$ | 866-872 | 867.25 | 870.83 | 871.75 |
| 40 | 626-632 | 627.25 | 630.83 | 631.75 | $81^{1}$ | 872-878 | 873.25 | 876.83 | 877.75 |
| 41 | 632-638 | 633.25 | 636.83 | 637.75 | $82^{1}$ | 878-884 | 879.25 | 882.83 | 883.75 |
| 42 | 638-644 | 639.25 | 642.83 | 643.75 | $83^{1}$ | 884-890 | 885.25 | 888.83 | 889.75 |

[^3]
## FREQUENCY SPECTRUM— SOUND AND <br> ELECTROMAGNETIC RADIATION

The spectrum of electromagnetic waves, shown in Fig. 2-9, covers a range of $10^{*} \mathrm{~m}$ to
about $10^{-5} \mathrm{~nm}$. The sound or audiofrequencics start about 8 Hz and the top of the range is around 20 kHz . The FCC allocation chart starts just below 10 kHz and ends at about 100 GHz . All of the different classes of radiowaves are in this region. Following the allocation chart frequencies are infrared

TABLE 2-18
Cable TV Channel Frequencies*

| Channel no. | Freq range | Carriers |  |  | Channel no. | Freq range | Carriers |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Video | Color | Sound |  |  | Video | Color | Sound |
| $\mathrm{T}-7$ | 5.75-11.75 | 7 | 10.58 | 11.5 | 28 | 246-252 | 247.25 | 250.83 | 251.75 |
| T-8 | 11.75-17.75 | 13 | 16.58 | 17.5 | 29 | 252-258 | 253.25 | 256.83 | 257.75 |
| '「-9 | 17.75-23.75 | 19 | 22.58 | 23.5 | 30 | 258-264 | 259.25 | 262.83 | 263.75 |
| $\mathrm{T}-10$ | 23.75-29.75 | 25 | 34.58 | 35.5 | 31 | 264-270 | 265.25 | 268.83 | 269.75 |
| T-11 | 29.75-35.75 | 31 | 40.58 | 41.5 | 32 | 270-276 | 271.25 | 274.83 | 275.75 |
| T-12 | 35.75-41.75 | 37 | 40.58 | 41.5 | 33 | 276-282 | 277.25 | 280.83 | 281.75 |
| T-13 | 41.75-47.55 | 43 | 46.58 | 47.5 | 34 | 282-288 | 283.25 | 286.83 | 287.75 |
| 2 | 54-60 | 55.25 | 58.83 | 59.75 | 35 | 288-294 | 289.25 | 292.83 | 293.75 |
| 3 | 60-66 | 61.25 | 64.83 | 65.75 | 36 | 294-300 | 295.25 | 298.83 | 299.75 |
| 4 | 66-72 | 67.25 | 70.83 | 71.75 | 37 | 300-306 | 301.25 | 304.83 | 305.75 |
| 5 | 76-82 | 77.25 | 80.83 | 81.75 | 38 | 306-312 | 307.25 | 310.83 | 311.75 |
| 6 | 82-88 | 83.25 | 86.83 | 87.75 | 39 | 312-318 | 313.25 | 316.83 | 317.75 |
| 7 | 174-180 | 175.25 | 178.83 | 179.75 | 40 | 318-324 | 319.25 | 322.83 | 323.75 |
| 8 | 180-186 | 181.25 | 184.83 | 185.75 | 41 | 324-330 | 325.25 | 328.83 | 329.75 |
| 9 | 186-192 | 187.25 | 190.83 | 191.75 | 42 | 330-336 | 331.25 | 334.83 | 335.75 |
| 10 | 192-198 | 193.25 | 196.83 | 197.75 | 43 | 336-342 | 337.25 | 340.83 | 341.75 |
| 11 | 198-204 | 199.25 | 202.83 | 203.75 | 44 | 342-348 | 343.25 | 346.83 | 347.75 |
| 12 | 204-210 | 205.25 | 208.83 | 209.75 | 45 | 348-354 | 349.25 | 352.83 | 353.75 |
| 13 | 210-216 | 211.25 | 214.83 | 215.75 | 46 | 354-360 | 355.25 | 358.83 | 359.75 |
| FM | 88-108 | , | - | - | 47 | 360-366 | 361.25 | 364.83 | 365.75 |
| 14 | 120-126 | 121.25 | 124.83 | 125.75 | 48 | 366-372 | 367.25 | 370.83 | 371.75 |
| 15 | 126-132 | 127.25 | 130.83 | 131.75 | 49 | 372-378 | 373.25 | 376.83 | 377.75 |
| 16 | 132-138 | 143.25 | 136.83 | 137.75 | 50 | 378-384 | 379.25 | 382.83 | 383.75 |
| 17 | 138-144 | 139.25 | 142.83 | 143.75 | 51 | 384-390 | 385.25 | 388.83 | 389.75 |
| 18 | 144-150 | 145.25 | 148.83 | 149.75 | 52 | 390-396 | 391.25 | 394.83 | 395.75 |
| 19 | 150-156 | 151.25 | 154.83 | 155.75 | 53 | 396-402 | 397.25 | 400.83 | 401.75 |
| 20 | 156-162 | 157.25 | 160.83 | 161.75 | 54 | 72-78 | 73.25 | 76.83 | 77.75 |
| 21 | 162-168 | 163.25 | 166.83 | 167.75 | 55 | 78.84 | 79.25 | 82.83 | 83.75 |
| 22 | 168-174 | 169.25 | 172.83 | 173.75 | 56 | 84-90 | 85.25 | 88.83 | 89.75 |
| 23 | 216-222 | 217.25 | 220.83 | 221.75 | 57 | $90-96$ | 91.25 | 94.83 | 95.75 |
| 24 | 222-228 | 223.25 | 226.83 | 227.75 | 58 | 96-102 | 97.25 | 100.83 | 101.75 |
| 25 | 228-234 | 229.25 | 232.83 | 233.75 | 59 | 102-108 | 103.25 | 106.83 | 107.75 |
| 26 | 234-240 | 235.25 | 238.83 | 239.75 | 60 | 108-114 | 109.25 | 112.83 | 113.75 |
| 27 | 240-246 | 241.25 | 244.83 | 245.75 | 61 | 114-120 | 115.25 | 118.83 | 119.75 |

* All frequencies in megahertz.
frequencies, visible light frequencies, Xrays, and gamma rays. Little is known beyond the gamma-ray frequencies. These are known as cosmic rays. The visible light spectrum covers a very small area, but thousands of color frequencies are present in this region.


## AUDIOFREQUENCY SPECTRUM

The audiofrequency spectrum is generally accepted as extending from 15 to 20,000 Hz . Figure 2-10 presents the frequencies for each tone of the standard organ keyboard, based on the current musical pitch of $\mathrm{A}=$ 440 Hz . Figure 2-11 shows the frequency range of various musical instruments and of other sounds. The frequency range shown for each sound is the range needed for faithful reproduction and includes the fundamental frequency and the necessary harmonic frequencies. The frequency range of the human ear and the various broadcasting and recording media are also included in Fig. 2-11.

Unisons have a 1:1 frequency ratio, and octaves have a $2: 1$ frequency ratio. The perfect fifth has a $3: 2$ frequency ratio, and its complement (the perfect fourth) has a 4:3 frequency ratio. The additive numerical measure for intervals is a logarithmic function wherein the octave is divided into 1200 cents:

Cents $=\frac{1200}{\log 2} \times \log$ of frequency ratio

Example. The ratio and cents for the perfect fifth are $3: 2$ and 701.955. For the major third, they are 5:4 and 386.314.

All musical intervals are based on ratios of products of the prime numbers 2,3 , and 5. The prevailing musical temperament is the result of a long history of experimentation with various temperaments (an infinite spectrum is possible), and further evolution can be anticipated.

## RADIOFREQUENCY SPECTRUM

The radiofrequency spectrum of 3 kHz to $3,000,000 \mathrm{MHz}$ is divided into the various bands shown in Table 2-19 for easier identification.

TABLE 2-19
Frequency Classification

| Frequency | Band no. | Classification | Abbreviation |
| :---: | :---: | :---: | :---: |
| $30-300 \mathrm{~Hz}$. | 2 | extremely low frequencies | FI.F |
| $300-3000 \mathrm{~Hz}$ | 3 | voice frequencies | VF |
| $3-30 \mathrm{kHz}$ | 4 | very low frequencies | VLF |
| $30-300 \mathrm{kHz}$. | 5 | low frequencies | I.F |
| $300-3000 \mathrm{kH} /$ | 6 | medium frequencies | MF |
| $3-30 \mathrm{MHz}$ | 7 | high frequencies | HF |
| $30-300 \mathrm{MH} \%$ | 8 | very high frequencies | VHF |
| 300-3000 MH\% | 9 | ultrahigh frequencies | UHF |
| 3-30 $\mathrm{CH}_{2}$ | 10 | super-high frequencies | SHF |
| $30-300 \mathrm{CHz}$ | 11 | extremely high frequencies | EHF |
| $300 \mathrm{GHz}-3 \mathrm{TH} \%$ | 12 | - | - |



Fig. 2-9

Constants and Standards


Fig. 2-10


Fig. 2-11

## NOAA WEATHER FREQUENCIES

The FCC has allocated three frequencies to the U.S. Department of Commerce, National Occanic and Atmospheric Administration (NOAA), National Weather Serv-
ice for the dissemination of weather information to the public. The frequencics assigned arc:
162.40 MHz
162.475 MHz
162.55 MHz .

## Chapter 3

## Symbols and Codes

## INTERNATIONAL Q SIGNALS

The international Q signals were first adopted to enable ships at sea to communicate with each other or to contact foreign shores without experiencing language difficulties. The signals consist of a series of three-letter groups starting with Q and hav-
ing the same meaning in all languages. Today, Q signals serve as a convenient means of abbreviation in communications between amateurs. Each Q signal has both an affirmative and an interrogative meaning. The question is designated by the addition of the question mark after the Q signal. The most common $Q$ signals are listed in Table 3-1.

TABLE 3-1
Q Signals
Signals

## Question

Answer or advice

QRA What station are you?
QRB How far are you from me?
QRD Where are you headed and from where?
QRE What is your estimated time of arrival?
QRF Are you returning to ___ ?
QRG What is my exact frequency?
QRH Does my frequency vary?
QRI How is the tone of my transmission?
QRJ Do you receive me badly?
QRK How do your read my signals?
QRI. Are you busy?
QRM Are you being interfered with?
QR.N Are you troubled by static?
QRO Shall I increase power?
QRP Shall I decrease power?
QRQ Shall I speak faster?
QRS Shall I speak slower?
QRT Shall I stop transmitting?

My station name is ___.
I am $\qquad$ from your station.
I am headed for $\qquad$ from $\qquad$ .
My ETA is $\qquad$ hours.
I am returning to $\qquad$ .
Your exact frequency is $\qquad$ kHz .
Your frequency varies.
Your tone is $\qquad$ _.
I cannot receive you. Your signals are too weak.
The legibility of your signal is $\qquad$ _.
I am busy (or I am busy with $\qquad$ ). Do not interfere.
I am being interfered with.
I am troubled by static.
Increase power.
Decrease power.
Speak faster.
Speak slower.
Stop sending.

TABLE 3-1 Cont.
Q Signals
Signals Question $\quad$ Answer or advice

QRU Have you anything for me?
QRV Are you ready?
QRU Shall I inform $\qquad$ that you are calling him on $\qquad$ kHz ?
QRX When will you call me again?
QRY What is my turn?
QRZ Who is calling me?
QSA What is the strength of my signals?
QSB Are my signals fading?
QSD Are my signals mutilated?
QSG Shall I send ___ messages at a time?
QSK Can you hear me between your signals?
QSL Will you send me a confirmation of our communication?
QSM Shall I repeat the last message?
QSN Did you hear me on ___ kHz ?
QSO Can you communicate with $\qquad$ direct or by relay?
QSP Will you relay to ___ free of charge?
QSQ Have you a doctor aboard?
QRR Have the distress calls from $\qquad$ been cleared?
QSU Shall I send reply on this frequency or on $\qquad$ kHz ?
QSV Shall I send a series of Vs on this frequency?
QSW Will you send on this frequency?
QSX Will you listen to $\qquad$ on $\qquad$ kHz ?
QSY Shall I change to transmission on another frequency?
QSZ Shall 1 send each word or group more than once?
QTA Shall I cancel message number?
QTB Do you agree with my counting words?
QTC How many messages do you have for me?
QTE What is my true bearing from you?
QTF Will you give me the position of my station according to the bearings of your direction finding station?
QTG Will you send two dashes of ten seconds each followed by our call sign-repeated $\qquad$ times on kHz ?
QTH What is your location in latitude and longitude?
QTI What is your true track -in degrees?
QTJ What is your true speed?
QTL What is your truc heading-in degrees?
QTM Send signals to enable me to fix my bearing and distance.
QTN At what time did you depart from $\qquad$ ?
QTO Have you left port/dock?
QTO Are you going to enter port/dock?

I have nothing for you.
1 am ready.
Please tell $\qquad$ that lam calling him on
$\qquad$
Wait kHz .

Your turn is I will call you at $\qquad$ hours.

You are being called by $\qquad$ .

The strength of your signals is $\qquad$ $-$
Your signals are fading.
Your keying is incorrect; your signals are bad.
Send $\qquad$ messages.
I can hear you.
I give you acknowledgment of receipt.
Repeat the last telegram you have sent me.
I heard you on $\qquad$ kHz .
I can communicate with $\qquad$ direct
(or through the medium of _____).
I will relay.
Yes. Or no, we have no doctor.
Distress calls from $\qquad$ have cleared.
Reply on this frequency, or reply on $\qquad$ kHz .

Send a series of Vs.
Yes, I will send on this frequency.
I will listen to ___ on ___ kHz .
Change to transmission on ___ kHz without
changing the type of wave.
Say each word or group of words twice or __._ times.
Cancel message number $\qquad$ as if not sent.
I agree, or word count is $\qquad$ —.
I have $\qquad$ messages for you.
True bearing from me is $\qquad$ degrees.
Your bearing is $\qquad$ .

I am sending two dashes of ten seconds each with my call sign $\qquad$ times on $\qquad$ kHz at __hours.
My location is $\qquad$ .
My true track is $\qquad$ degrees.
My true speed is $\qquad$ -.
My true heading is ___ degrees.
Fix your bearing and distance on my radio signal.
I departed from $\qquad$ (place) at $\qquad$ hours.
I left port at $\qquad$ hours.
I am entering port.

TABLE 3-1 Cont. Q Signals

Signals

QTQ Can you communicate with my station by means of the International Code of Signals?
QTR What is the correct time?
QTS Will you send your call sign for $\qquad$ minutes now, or at $\qquad$ hours on $\qquad$ kHz so that your frequency may be measured?
QTU During what hours is your station open?
QTV Shall I stand guard for you on $\qquad$ kHz ?

QTX Will you keep your station open for further communication with me for $\qquad$ hours?

QTY Are you proceeding to the position of incident and if so when do you expect to arrive?
QTZ Are you continuing the search?
QUA Do you have news of $\qquad$ ?

QUB Can you give me, in the following order, information concerning visibility, height of clouds, direction and velocity of ground wind at ___ (place of observation)?
QUC What is the number (or other) of the last message you received from me?
QUD Have you received the urgency signal sent by _._._?
QUF Have you received the distress signal sent by ____?
QUG Will you be forced to alight (or land)?
QUH Will you give me the present barometric pressure at sea level?
QUJ Will you indicate the true course for me to follow?
QUM Is the distress traffic ended?
QRRR (Official ARRI. land distress call)

I will communicate with you by International Code of Signals.
The correct time is $\qquad$ hours.
I will send your call sign for $\qquad$ now, or at ___ hours on ___ kHz so you can measure my frequency.
My station is open from $\qquad$ to $\qquad$ hours.
Listen for me on channel $\qquad$ (from $\qquad$ to hours).
I will keep my station open for further communication with you until further notice (or until $\qquad$ hours).
I am proceeding to the position of incident and expect to arrive at $\qquad$ hours.
I am continuing the search for $\qquad$ _. 1 have news of
Information desired follows: visibility is $\qquad$ clouds are $\qquad$ wind is $\qquad$ knots from __ at $\qquad$ latitude $\qquad$ longitude.

The number of my last message to you is
$\qquad$ -

I have urgency signal sent by $\qquad$ -.

I have received the distress signal sent by $\qquad$ -.

I must land now.
Barometric pressure at sea level is now $\qquad$ .

Follow course $\qquad$ degrees true.

Distress traffic is ended.
This is a special signal, and if you hear it keep off the frequency except to listen, unless you are in a position to help. It is the official ARRL land distress call, for emergency use only. It is the equivalent of SOS as used by ships at sea and must receive the same attention and priority.

## Handbook of Electronics Tables and Formulas

## Z-SIGNALS

The Z-code signals shown in Table 3-2
are used to communicate at sea. The U.S. military also uses these codes.

TABLE 3-2
Z Code for Point-to-Point Service*

| Signal | Message | Signal | Message |
| :---: | :---: | :---: | :---: |
| *ZAA | A | *ZBQ | When and on what frequency was message |
|  | YOU ARE NOT OBSERVING CIRCUIT |  | received. |
|  | DISCIPLINE. | ZBR | Break circuit. Retuning. |
| *ZAB | YOUR SPEED KEY IMPROPERLY | *ZBR | Shall I send by ___ (method). |
|  | ADJUSTED. | ZBS | Blurring Signals. (1) Dots heavy, (2) Dots |
| ZAC | Advise (Call sign of) frequency you are reading. | *ZBT | light. <br> Count $\qquad$ as $\qquad$ groups. |
| * ZAC | Cease using speed key. | *ZBU | Report when in communication with |
| *ZAD | Signal (1) Not understood, (2) Not held. |  |  |
| *ZAE | Unable to receive you, try, via __. | *Z.BV | Answer on ___ MHz. |
| *ZAF | Reroute the circuit by patching. | *ZBW |  |
| * ZAH | Unable to relay. We file. | ZBY | Pull Back your tape one Yard. |
| *ZAI | Run (foxes, RYs, mk, etc.). |  | C |
| *ZAJ | Have been unable to break you. | ZCA | Circuit affected. Make readable signals. |
| ZAL. | Alter your wavelength. | ZCB | Circuit broken. Signal unheard. |
| *ZAL | Closing down, due to | ZCC | Collate code. |
| ZAN | WE CAN RECEIVE ABSOLUTELY | ZCD | Your Collation is Different. |
|  | NOTHING. | ZCF | CHECK YOUR CENTER FREQUENCY, |
| *ZAN | Transmit only messages of above |  | PLEASE. |
|  | precedence | Z.CI | Circuit Interrupted. Running and available. |
| * ZAO | CAN'T UNDERSTAND VOICE. USE | ZCK | Check Keying. |
|  | TELEGRAPH. | ZCL | TRANSMIT CALI. LETTERS |
| ZAP | ACKNOWLEDGE, PLEASE. |  | INTELLIGIBIY. |
| *ZAP | Work (simplex, duplex, mux, sb). | ZCO | Your Collation Omitted. |
| * ZAQ | Last word received (sent) was | ZCP | Conditions poor, increase to maximum. |
| ZAR | Revert to Automatic Relay. | ZCR | Using concentrator, make warning signals. |
| *ZAS | Rerun tapes run on ___ since | ZCS | Cease Sending. |
| *ZAT | Punching tape for transmission. | ZCT | Send Code Twice. |
| *ZAV | Send blind until advised. | ZCW | Are you in direct Communication With |
| *ZAX | You are causing interference. |  |  |
| *ZAY | Send on $\qquad$ $(\mathrm{kHz})$. Will confirm later. | *ZDA | Hr. formal message, priority |
| *ZBA | Cause of delay is | * Z DB | Expedite reply to my |
| *ZBD | Following was sent ___ (time). | ZDC | Diagnosing Circuit faults, will advise. |
| *ZBE | Retransmit message ___ to | Z.DE | Message undelivered. (1) Will keep trying, |
| *ZBG | You are sending uppercase. |  | (2) Advise disposal, (3) Canceling, |
| * ZBH | Make call before transmitting traffic. |  | (4) Btr, ads. |
| *ZBI | Listen for telephony. | *ZDE | Message ___ undelivered. |
| *ZBL | Do not use break-in. | ZDF | Frequency is Drifting to degree indicated, |
| *ZBM | Put ___ (specd opr.) this frequency. |  | 1-5. |
| ZBN | Break and go ahead with New slip. | *ZDF | Message ___ received by addressee |
| * 2 ZBN | Your tape reversed. |  | ___ (time). |
| *ZBO | 1 HAVE TRAFFIC. | *ZDG | Accuracy of following doubtful. |
| *'ZBP | (1) Characters indistinct, (2) Spacing bad. | ZDH | Your Dots are too Heavy (long). |

TABLE 3-2 Cont.
Z Code for Point-to-Point Service*

| Signal | Message | Signal | Message |
| :---: | :---: | :---: | :---: |
| ZDL | Your Dots are too Light (short). | H |  |
| ZDM | Your Dots are Missing. | ZHA | How are conditions for Auto reception? |
| *ZDM | This is a multiple-address message. | ZHC | HOW ARE YOUR RECEIVING |
| *ZDN | Report disposal of message |  | CONDITIONS? |
| *ZDQ | Message $\qquad$ relayed to $\qquad$ at $\qquad$ by $\qquad$ . | $\begin{aligned} & \text { ZHM } / \mathrm{x} \\ & \text { ZHS } \end{aligned}$ | Harmonic radiation from transmitter. Send High Speed auto $\qquad$ wpm. |
| *ZDS | Message just transmitted erroneous. Correct version is $\qquad$ _. | Z.HY | We are Holding Your $\qquad$ I |
| ZDT | Following transmitters running dual. | ZIM | Industrial or Medical interference, 1-5. |
| *ZDT | Don't transmit exercise messages until | 7.1P | Increase Power. |
|  | advised. | Z.IR | You have strong Idle Radiation. |
| ZDV | Your Dots Varying length, please remedy. | ZIS | Atmospheric Interference, 1-5. |
| *ZDV | Private message received for __. |  | J |
|  | Advise. | 7.JF | Frequency Jumping to degree indicated, |
| *ZDY | No private messages until ordered. E |  |  |
| *ZEC | Have you received message ___? | *ZKA | Who is controlling station? or I am |
| ZED | We are Experiencing Drop-outs, 1-5. | *ZKB | Permission necessary before transmitting |
| ZEF | We are Experiencing Fill-ins, 1-5. |  | messages. |
| ZEG | We are Experiencing Garbles, 1-5. | *ZKD | Take control of net ____ or shall I |
| *ZEI | Accuracy of heading doubtful. | *ZKE | I (or___) reports into circuit (net). |
| *ZEK | No answer required. | *ZKF | Station leaves net temporarily. |
| *ZEL | This message is correction to | *ZKJ | Closing down (until ___ ). |
| * Z.EN | This message is classified. | ZKO | REVERT TO ON-OFF KEYING. |
| *ZEP | Parts marked ZEP coming later. | ZKQ | Say when ready to resume. |
| *ZEU | Exercise $\qquad$ (drill message). | $\begin{gathered} * \mathrm{ZKS} \\ \text { ZKW } \end{gathered}$ | What Stations Keeping watch on $\qquad$ ? <br> Keying weight is $\qquad$ (percent). |
| ZFA | Failing Auto. | L |  |
| *ZFA | Message intercepted or copied blind. | ZLB | Give Long Breaks, please. |
| ZFB | SIGNALS ARE FADING BADLY. | ZLD | We are getting L.ong Dash from you. |
| *ZFB | Pass this message to __. | ZLL | Distorted Land Line control signals. |
| ZFC | Check your FSK shift, please. | ZLP | Low (minimum) Power. |
| ZFD | Depth of Fading is as indicated, 1-5. | ZLS | WE ARE SUFFERING FROM |
| *ZFD | This message is a suspected duplicate. | LIGHTNING ${ }_{\text {M }}$ |  |
| *ZFF | Advise when message received by |  |  |
| *ZFH | Message for (1) Action, (2) Info, | ZMG | Magnetic activity. |
|  | (3) Comment. | ZMO | STAND BY MOMENT. |
| * ZFI | Reply message? There is no reply. | ZMP | MisPunch or Perforator failures. |
| ZFK | Revert to FSK. | ZMQ | Stand by for __. |
| ZFO | SIGNALS FADED OUT. | ZMU/x | MUltipath making ___ mark bias. |
| 7.FQ/x | Frequency shift your signal is __ Hz. | N |  |
| ZFR | Rapidity of Fading is as indicated, 1-5. | ZNB | No Breaks, we send twice. |
| *ZFR | Cancel transmission __. | *ZNB | Authentication is |
| ZFS | Signals are Fading Slightly. | ZNC | NO COMMUNICATIONS WITH |
|  | G | * ZNC | All stations authenticate. |
| *ZGB | Send ___ (answer). | *ZND | You are misusing authenticator. |
| ZGF | ___ signals Good For ___ wpm. | ZNG | Receiving conditions No Good for code. |
| *ZGF | Make call signs more distinctly. | ZNI | NO CALL LETTERS |
| ZGP | Please Give Priority. |  | (IDENTIFICATION) HEARD. |
| ZGS | YOUR SIGNALS GETTING | ZNN | ALL CLEAR OF TRAFFIC. |
|  | STRONGER. | ZNO | Not On the air. |
| ZGW | YOUR SIGNALS GETTING WEAKER. | ZNR | Not Received. |

TABLE 3-2 Cont.
Z Code for Point-to-Point Service*

| Signal | Message | Signal | Message |
| :---: | :---: | :---: | :---: |
| ZNS | Here New Slip. | ZSH | STATIC HEAVY HERE. |
|  |  | ZSI/x | Please furnish Signal Intensity. |
| ZOA | Have checked (call letters) ___ OK. | ZSM/x | Microvolt input to receiver is |
| *ZOC | Relay to your substations. - | ZSN | Give SINPO report on |
| ZOD | Observing ___ will transfer when better. |  | S Signal strength. |
| *ZOD | Act as radio link between me and |  | 1 Interference. |
| *ZOE | Can you accept message? (or) Give me message. |  | N Noise. |
|  |  |  | P Propagation. |
| *ZOF | Relay this message. |  | O Overall readability. |
| * 7 OOG | Transmit your message (give info.). | ZSO | Transmit Slips Once. |
| ZOH | What traffic have you On Hand? | ZSR | YOUR SIGNALS STRONG AND |
| ZOK | WE ARE RECEIVING OK. |  | READABLE. |
| *ZOK | Relay this message via | ZSS | Send Slower. |
| ZOL | OK. On Line. | ZST | Transmit Slips Twice. |
| *ZOM | Mail delivery permissible. | ZSU | YOUR SIGNALS ARE UNREADABLE. |
| ZOR | Transmit Only Reversals. | ZSV | Your Speed Varying. |
| *ZOU | Give instructions for routing traffic. |  | T |
| * ZOZ | Obtain retransmission of message $\qquad$ P | ZTA | Transmit by Auto. |
|  |  | ZTH | Transmit by Hand. |
| ZPA | Printer line Advance not received. | ZTI | Transmission temporarily Interrupted. |
| * ZPA | Your speech distorted. |  | U |
| ZPC | Printer Carriage-return not received. | ZUA | Conditions Unsuitable for Automatic |
| * ZPC | Signals fading, 1-5. |  | recording. |
| ZPE | Punch Everything. | *ZUA | Timing signal will be transmitted. |
| 7.PF | Printer motor Fast. | ZUB | WE HAVE BEEN UNABLE TO |
| ZPO | Send Plain Once. |  | BREAK YOU. |
| ZPP | Punch Plain only. | ZUC | UNABLE TO COMPLY. WILL DO SO |
| ZPR | Reruns slip at Present Running. |  | AT |
| ZPS | Printer motor Slow. | *ZUE | Affirmative (Yes). |
| ZPT | Send Plain Twice. | *ZUG | Negative (No). |
|  |  | *ZUH | Unable to comply. |
| 7RA | Reverse Auto tape. | *ZUJ | Wait. Stand by. |
| * ZRA | My frequency OK? Your frequency is |  | V |
|  |  | ZVB | Varying Bias. |
| ZRB | Relayed signal Bad, adjust receiver. | 7.VF | Signals Varying in Frequency. |
| *7RB | Check your frequency on this circuit. | ZVP | Send Vs Please. |
| ZRC | Can you Receive Code? | * ZVR | Pass at once to substations. |
| * ZRC | Shall I, or tune your transmitter to . | ZVS | Signals Varying in intensity. |
| * ZRE | Hear you best on ___ (kHz). |  | W |
| * 7RF | Send tuning signals on present frequency. | *ZWB | Name of operator on watch. |
| ZRK | Reversed Keying. | ZWC | Wipers or Clicks here. |
| ZRI. | Rerun slip before one now running. | ZWO | SEND WORDS ONCE. |
| ZRM | Plase Remove Modulation from ... | ZWR | YOUR SIGNALS WEAK BUT |
| *ZRM | I receive___ (usb, lsb, isb). |  | READABLE. |
| ZRN | ROUGH NOTE. | ZWS | Wavelength (frequency) is Swinging, 1-5. |
| ZRO | ARE YOU RECEIVING OK? | ZWT | SEND WORDS TWICE. |
| ZRR | Run Reversals. |  | Y |
| 7.RS | Rerun message No. | ZYS | WHAT IS YOUR SPEED OF |
| ZRT | Revert to Traffic. |  | TRANSMISSION? |
| 7RY | Run test slip, please. |  | Z |
|  | S | *ZZF | Incorrect. |
| ZSF | SEND FASTER. | *ZZG | You are correct. |

TABLE 3-2 Cont.
Z Code for Point-to-Point Service*

| Signal | Message | Signal | Message |
| :---: | :---: | :---: | :---: |
| *ZZH | TRY AGAIN. Multiplex | ZXA | Radiophoto and Facsimile Adjust to receive speeds $\qquad$ |
| ZYA | Cease traffic; send As on A channel. | ZXC | PIX ___ Conditionally accepted. |
| ZYC | Cycling on ARQ , errors stored your end. | ZXD | Send Dashes, please. |
| ZYK | Check Your Keying on channel | ZXF | You are Floating Fast. |
| ZYM | Change from single printer to Multiplex. | ZXH | Limits High, reduce ___ Hz. |
| ZYN | Make bias Neutral. | ZXJ | You are Jumping out of phase. |
| ZYP | Change from multiplex to single Printer. | ZXK | Is your synchronizing correct? |
| ZYR | Please put ___ on MUX revolutions. | ZXL | Limits are Low, increase __ Hz. |
| ZYT | Check Your Thyratrons. | ZXO | Last run defaced due to - |
| ZYX/x | Revert to MUX frames ____ channels. | ZXP | Go ahead with Pix. |
|  |  | ZXS | You are floating Slow. |
|  |  | ZXV | Your modulation is Varying. |

*Asterisk indicates U.S. military usage. Numbers 1-5 following the " 2 " signal mean: (1) very slight, (2) slight, (3) moderate, (4) severe, (5) extreme.

Sources: Cable and Wireless Ltd., L.S. Army Communications Manual SIG 439-2, ACP-131 (A), Allied Communication Procedures, W3AFM.

## 10-Signals

Numerous versions of 10 -signals are in use. The one in Table 3-3, adopted by the Associated Public Safety Communications Officers, Inc. (APCO), is the result of an indepth study to develop a uniform code that could be used by all radio services. Containing only 34 signals, it is easier to memorize than the others, yet most of the needed sig-
nals are included. Two other versions, one used primarily by CBers and the other by police agencies, are given in Tables 3-4 and 3-5.

## 11-CODE SIGNALS

Table 3-6 is the 11-code, also sometimes used by law enforcement agencies.

TABLE 3-3
APCO 10-Signals

| Number | Meaning | Number | Meaning | Number | Meaning |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10-1 | signal weak | 10-13 | existing conditions | 10-25 | report to (meet) |
| 10-2 | signal good | 10-14 | message information | 10-26 | estimated arrival time |
| 10-3 | stop transmitting | 10-15 | message delivered | 10-27 | license/permit |
| 10-4 | affirmative (OK) | 10-16 | reply to message |  | information |
| 10-5 | relay (to) | 10-17 | enroute | 10-28 | ownership information |
| 10-6 | busy | 10-18 | urgent | 10-29 | records check |
| 10-7 | out of service | 10-19 | (in) contact | 10-30 | danger/caution |
| 10-8 | in service | 10-20 | location | 10-31 | pick-up |
| 10-9 | say again | 10-21 | call (___ ) by phone | 10-32 | ..-.... units needed |
| 10-10 | negative | 10-22 | disregard |  | specify/number/type |
| 10-11 | $\ldots$ on duty | 10-23 | arrived at scene | 10-33 | help me quick |
| 10-12 | stand by (stop) | 10-24 | assignment completed | 10-34 | time |

TABLE 3-4
CBers 10-Code

| Number | Meaning | Number | Meaning |
| :---: | :---: | :---: | :---: |
| 10-1 | Receiving poorly; signal weak. | 10-39 | Your message delivered. |
| 10-2 | Receiving well; signal good. | 10-41 | Please tune to channel |
| 10-3 | Stop transmitting. | 10-42 | Traffic accident at |
| 10-4 | OK, message received; acknowledgment. | 10-43 | Traffic tie-up at |
| 10-5 | Relay message; or relay to ___. | 10-44 | I have a message for you (or ___ ). |
| 10-6 | Busy, stand by. | 10-45 | All units within range, please report. |
| 10-7 | Out of service (leaving air). | 10-46 | Assist motorist. |
| 10-8 | In service (subject to call). | 10-50 | Break channel. |
| 10-9 | Repeat, or repeat message. | 10-51 | Wrecker needed. |
| 10-10 | Transmission completed; standing by. | 10-52 | Ambulance needed. |
| 10-11 | Transmitting (talking) too rapidly. | 10-60 | What is next message number? |
| 10-12 | Visitors (or officials) present. | 10-62 | Unable to copy, use phone. |
| 10-13 | Weather and/or road conditions. | 10-63 | Net directed to -. |
| 10-16 | Make pickup at ___. | 10-64 | Net clear. |
| 10-17 | Urgent business. | 10-65 | Awaiting your next message/assignment. |
| 10-18 | Anything (message) for us? | 10-67 | All units comply. |
| 10-19 | Nothing for you, return to base. | 10.70 | Fire at |
| 10-20 | Location. | 10-71 | Proceed with transmission in sequence. |
| 10-21 | Call ___ by phone; or number | 10-73 | Speed trap at __. |
| 10-22 | Report in person to __. | 10-75 | You are causing interference. |
| 10-23 | Stand by. | 10-77 | Negative contact. |
| 10-24 | Completed last assignment. | 10-81 | Reserve hotel room for |
| 10-25 | Can you contact ___ ? | 10-82 | Reserve lodging (room). |
| 10-26 | Disregard last information. | 10-84 | Telephone number. |
| 10-27 | I am moving to channel __. | 10-85 | My address is ._._. |
| 10-28 | Identify your station. | 10-89 | Radio repairmen needed at ___ . |
| 10-29 | Time is up for contact. | 10-90 | I have TVI. |
| 10-30 | Does not conform to FCC Rules. | 10-91 | Talk closer to mike. |
| 10-32 | I will give you a radio check. | 10-92 | Your transmitter is out of adjustment. |
| 10-33 | Emergency traffic at this station. | 10-93 | Frequency check. |
| 10-34 | Trouble at this station, need help. | 10-94 | Please give me a long count. |
| 10-35 | Confidential information. | 10-95 | Transmit dead carrier for 5 seconds. |
| 10-36 | Correct time. | 10-99 | Mission completed, all units secure. |
| 10-37 | Wrecker needed at | 10-100 | Rest room pause. |
| 10-38 | Ambulance needed at | 10-200 | Police needed at |

TABLE 3-5
Police 10-Code

| Number | Meaning | Number | Meaning |
| :---: | :---: | :---: | :---: |
| 10-0 | Caution. | 10-49 | Traffic light out. |
| 10-1 | Unable to copy, change location. | 10-50 | Accident ___ (F, PI, PD). |
| 10-2 | Signal good. | 10-51 | Wrecker needed. |
| 10-3 | Stop transmitting. | 10-52 | Ambulance needed. |
| 10-4 | Acknowledgment. | 10-53 | Road blocked. |
| 10-5 | Relay (to). | 10-54 | Livestock on highway. |
| 10-6 | Busy, stand by unless urgent. | 10-55 | Intoxicated driver. |
| 10-7 | Out of service (give location). | 10-56 | Intoxicated pedestrian. |
| 10-8 | In service. | 10-57 | Hit and run. |
| 10-9 | Repeat. | 10-58 | Direct traffic. |
| 10-10 | Fight in progress. | 10-59 | Convoy or escort. |
| 10-11 | Dog case. | 10-60 | Squad in vicinity. |
| 10-12 | Stand by. | 10-61 | Personnel in area. |
| 10-13 | Weather and road report. | 10-62 | Reply in message. |
| 10-14 | Report of prowler. | 10-63 | Prepare to make written copy. |
| 10-15 | Civil disturbance. | 10-64 | Message for local delivery. |
| 10-16 | Domestic trouble. | 10-65 | Net message assignment. |
| 10-17 | Meet complainant. | 10-66 | Message cancellation. |
| 10-18 | Complete assignment quickly. | 10-67 | Clear to read next message. |
| 10-19 | Nothing for you, return to _-. | 10-68 | Dispatch information. |
| 10-20 | Location. | $10-70$ | Fire alarm. |
| 10-21 | Call___ by phone. | 10-71 | Advise nature of fire. |
| 10-22 | Disregard. | 10-72 | Report progress on fire. |
| 10-23 | Arrived at scene. | 10-73 | Smoke report. |
| 10-24 | Assignment completed. | 10-74 | Negative. |
| 10-25 | Report in person to | 10-75 | In contact with. |
| 10-26 | Detaining subject, expedite. | 10-76 | Enroute. |
| 10-27 | Drivers license information. | 10-77 | ETA (Estimated Time of Arrival). |
| 10-28 | Vehicle registration information. | 10-78 | Need assistance. |
| 10-29 | Check records for wanted. | 10-79 | Notify coroner. |
| 10-30 | Illegal use of radio. | 10-80 | Chase in progress. |
| 10-31 | Crime in progress. | 10-81 | Breathalizer report. |
| 10-32 | Man with gun. | 10-82 | Reserve lodging. |
| 10-33 | Emergency. | 10-83 | Work school crossing at |
| 10-34 | Riot. | 10-84 | If meeting, advise ETA. |
| 10-35 | Major crime alert. | 10-85 | Delayed, due to |
| 10-36 | Correct time. | 10-86 | Officer/operator on duty. |
| 10-37 | Investigate suspicious vehicle. | 10-87 | Pick up/distribute checks. |
| 10-38 | Stopping suspicious vehicle. | 10-88 | Advise present telephone number. |
| 10-39 | Urgent-use light and siren. | 10-89 | Bomb threat. |
| 10-40 | Silent run, no light and siren. | 10-90 | Bank alarm at |
| 10-41 | Beginning tour of duty. | 10-91 | Pick up prisoner/subject. |
| 10-42 | Ending tour of duty. | 10-92 | Improperly parked vehicle. |
| 10-43 | Information. | 10-93 | Blockade. |
| 10-44 | Request permission to leave patrol | 10-94 | Drag racing. |
|  | for _-_. | 10-95 | Prisoners/subject in custody. |
| 10-45 | Animal carcass in ___ lane at __ | 10-96 | Mental subject. |
| 10-46 | Assist motorist. | 10-97 | Check (test) signal. |
| 10-47 | Emergency road repairs needed, | 10-98 | Prison/jail break. |
| 10-48 | Traffic standard needs repair. | 10-99 | Records indicate wanted or stolen. |

TABLE 3-6
Law Enforcement 11-Code

| Signal |  | Meaning | Signal |
| :--- | :--- | :--- | :--- |
| $11-6$ | Illegal discharge of firearms. | Meaning |  |
| $11-7$ | Prowler. | $11-43$ | Doctor required. |
| $11-8$ | Person down. | $11-44$ | Coroner required. |
| $11-10$ | Take a report. | $11-45$ | Attempted suicide. |
| $11-12$ | Dead animal. | $11-46$ | Death report. |
| $11-13$ | Injured animal. | $11-47$ | Injured person. |
| $11-14$ | Animal bite. | $11-48$ | Provide transportation. |
| $11-15$ | Ball game in street. | $11-65$ | Traffic signal light out. |
| $11-17$ | Wires down. | $11-66$ | Traffic signal out of order. |
| $11-24$ | Abandoned vehicle. | $11-70$ | Fire alarm. |
| $11-25$ | Vehicle-traffic hazard. | $11-71$ | Fire report. |
| $11-25 X$ | Female motorist needs assistance. | $11-79$ | Traffic accident-ambulance sent. |
| $11-27$ | Subject has felony record but is not | $11-80$ | Traffic accident-serious injury. |
|  | wanted. | $11-81$ | Traffic accident-minor injury. |
| $11-28$ | Rush vehicle registration information | $11-82$ | Traffic accident-no injury. |
|  | driver is being detained. | $11-83$ | Traffic accident-no details. |
| $11-29$ | Subject has no record and is not wanted. | $11-84$ | Direct traffic. |
| $11-30$ | Incomplete phone call. | $11-85$ | Dispatch tow truck. |
| $11-31$ | Person calling for help. | $11-86$ | Special detail. |
| $11-40$ | Advise if ambulance is needed. | Assist other unit. |  |
| $11-41$ | Request ambulance. | $11-98$ | Meet officer. |
| $11-42$ | Ambulance not required. | $11-99$ | Officer needs help. |

## THE INTERNATIONAL CODE

| A | didah |
| :--- | :--- |
| B | dahdididit |
| C | dahdidahdit |
| D | dahdidit |
| E | dit |
| F | dididahdit |
| G | dahdahdit |
| H | didididit |
| I | didit |


| $\mathbf{J}$ | didah dah dah |
| :--- | :--- |
| $\mathbf{K}$ | dah didah |
| $\mathbf{L}$ | didah didit |
| $\mathbf{M}$ | dah dah |
| $\mathbf{N}$ | dah dit |
| O | dah dah dah |
| $\mathbf{P}$ | didah dah dit |
| $\mathbf{Q}$ | dah dah di dah |
| $\mathbf{R}$ | di dah dit |


| S | dididit |
| :--- | :--- |
| T | dah |
| U | dididah |
| V | didididah |
| W | didahdah |
| X | dah dididah |
| Y | dah didah dah |
| Z | dah dah di dit |


| 1 | di dah dah dah dah | 6 | dah di di di dit |
| :--- | :--- | :--- | :--- |
| 2 | di di dah dah dah | 7 | dah dah di di dit |
| 3 | di di di dah dah | 8 | dah dah dah di dit |
| 4 | di di di di dah | 9 | dah dah dah dah dit |
| 5 | di di didi dit | 0 | dah dah dah dah dah |

question mark
error
wait
di di dah dah di dit
di di di di di di di dit
di dah di di dit
period
comma end of message
di dah di dah di dah dah dah di di dah dah di dah di dah dit

## Symbols and Codes

## SINPO RADIO-SIGNAL REPORTING CODE

SINPO is an acronym for Signal Strength, Interference, Noise, Propagation, and $\mathbf{O v e r a l l}$ merit. The code has a five number rating scale, as shown in Table 3-7, and provides a rapid and fairly accurate means for evaluating and reporting the quality of a received radio signal.

## GREEK ALPHABET

The Greek alphabet is given in Table $3-8$. The items for which each letter is a symbol are listed in Table 3-9.

TABLE 3-8
Greek Alphabet

| Letter |  | Name | Letter |  | Name |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Small | Capital |  | Small | Capital |  |
| $\alpha$ | A | alpha | $\nu$ | N | nu |
| $\beta$ | B | beta | $\xi$ | $\pm$ | xI |
| $\gamma$ | $\Gamma$ | gamma | $o$ | 0 | omicron |
| $\delta$ | $\Delta$ | delta | $\pi$ | $\Pi$ |  |
| $\epsilon$ | E | epsilon | e | P | rho |
| $\zeta$ | Z | zeta | $\sigma$ | $\Sigma$ | sigma |
| $\eta$ | H | eta | $\tau$ | T | tau |
| $\theta$ | $\Theta$ | theta | $v$ | $\Upsilon$ | upsilon |
| $\bullet$ | I | iota | $\phi$ | $\Phi$ | phi |
| ${ }^{*}$ | K | kappa | $\chi$ | X | chi |
| $\lambda$ | $\Lambda$ | lambda | $\psi$ | $\Psi$ | psi |
| $\mu$ | M | mu | $\omega$ | $\Omega$ | omega |

TABLE 3-7
SINPO Signal-Reporting Code

|  | $\mathbf{S}$ | $\mathbf{I}$ | $\mathbf{N}$ | $\mathbf{P}$ | $\mathbf{O}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Degrading effect of |  |  |

TABLE 3-9
Greek Symbol Designations

| Symbol | Designates | Symbol | Designates |
| :---: | :---: | :---: | :---: |
| $\alpha$ | angles, angular acceleration, coefficients, absorptance, linear current density | $\lambda_{\text {c }}$ | critical wavelengths |
|  |  | $\lambda_{1}$ | wavelength in a guide |
| $\beta$ | angles, phase coefficient, transfer ratio | $\lambda_{i}$ | resonance wavelength |
| B | magnetic induction | A | logarithmic decrement, magnetic flux |
| $\gamma$ | electrical conductivity, propagation |  | linkage |
|  | coefficient, specific quantity | ${ }^{\mu}$ | amplification factor, Poisson's ratio, |
| $\Gamma$ | reciprocal inductance, propagation |  | permeability |
|  | constant | $\mu$ | magnetic susceptibility |
| $\Gamma_{\text {c }}$ | electric constant | $\mu_{0}$ | initial (relative) permeability |
| $\Gamma_{\text {m }}$ | magnetic constant | $\mu_{\text {r }}$ | relative (magnetic) permeability |
| $\delta$ | density, damping coefficient, angles, sign | $\mu_{\text {, }}$ | permeability of vacuum |
|  | of variation | $\nu$ | frequency, Poisson's ratio, reluctivity |
| $\Delta$ | permittivity, determinant | $\mathrm{N}_{1}$ | Avogadro's constant |
| $\epsilon$ | linear strain, capacitivity, permittivity, | $\xi$ | coordinates |
|  | base of natural logarithms | $\pi$ | 3.1416 . . (circumference divided by |
| $\epsilon_{\mathrm{b}}$ | complex dielectric constant |  | diameter) |
| $\epsilon_{\mathrm{r}}$ | relative capacitivity, relative permittivity, dielectric constant | Q | volume density of charge, resistivity, cylindrical coordinates |
| $\epsilon_{\text {t }}$ | total emissivity | $\varrho_{0}$ | thermal resistivity |
| $\epsilon_{1}$ | electric susceptibility | $\sigma$ | wavenumber, normal stress, surface |
| $\epsilon_{1}$ | emissivity (a function of wavelength) |  | density of charge |
| E | energy, electric field strength | $\Sigma$ | sign of summation |
| ${ }_{\text {Z }}^{0}$ | coordinate, coefficients | $\tau$ | time constant, shear stress, transmittance |
|  | characteristic impedance, surge | $1 / \tau$ | signaling speed |
|  | impedance | $\phi$ | angle (plane), electrostatic potential, |
| $\eta$ | permeability, efficiency, modulation |  | phase angle |
|  | index (FM) | $\Phi$ | heat flow, radiant power, luminous flux, |
| H | magnetic field strength |  | magnetic flux |
| $\theta$ | temperature, volume strain, angular | $\Phi$, | radiant power |
|  | phase displacement, angle | $\Phi^{*}$ | luminous flux |
| $\iota$ | length | $\chi$ | cartesian coordinate |
| * | thermal conductivity, coupling | $\chi_{\text {\% }}$ | electric susceptibility |
|  | cocfficient, Boltzmann's constant, | $\chi_{\text {m }}$ | magnetic susceptibility |
|  | circular and angular wave number | $\psi$ | angle (plane) |
| $\chi_{\text {c }}$ | eddy-current coefficient | $\pm$ | electric flux |
| $\chi_{1}$ | form factor | $\omega$ | angle, angular frequency, angular velocity |
| $\chi_{\text {n }}$ | hysteresis coefficient | $\omega_{\text {s }}$ | critical angular frequency |
| K | electric field strength, luminous | $\omega^{\prime}$ | synchronous angular frequency |
|  | efficiency, susceptibility | $\omega_{\text {r }}$ | resonance angular frequency |
| $\lambda$ | conductivity, wavelength, linear density charge | $\Omega$ | resistance in ohms, angles (solid) |

## LETTER SYMBOLS AND ABBREVIATIONS

Although letter symbols are often regarded as being abbreviations, each has a separate and distinct use. A symbol represents a unit or quantity, and is the same in all languages. An abbreviation is a letter or a combination of letters (with or without punctuation marks) that represent a word or name in a particular language. An abbreviation, therefore, may be different for different languages. Letter symbols, with few exceptions, are restricted to the Greek and English alphabets. Unit symbols are most commonly written in lowercase letters except when the unit name is derived from a proper name. The distinction between capital and lowercase letters is part of the symbol and should be followed. The terms marked with an asterisk (*) in the following list are not the preferred unit in SI. They have been included because they are used frequently. The preferred SI unit may be included in parentheses ( ) following the previously used unit.

## Letter Symbols

A-ampere; ampere turn
Ah-ampere-hour
$\mathbf{A} / \mathbf{m}$-ampere per meter
A-angstrom* (micrometer)
a-atto ( $10^{-18}$ )
B-bel
b-bit; barn
Bd-baud
$\mathbf{B q}$-becquerel
Btu-British thermal unit
C-coulomb
${ }^{\circ} \mathbf{C}$-degree Celsius
c-centi ( $10^{-2}$ ); cycle
cd-candela
$\mathbf{c d} / \mathbf{m}^{2}$-candela per square meter

Ci-curie* (becquerel)
cm-centimeter
$\mathrm{cm}^{3}$-cubic centimeter
cmil-circular mil
c/s-cycle per second* (hertz)
d-deci ( $10^{-1}$ ); day
da-deka (10)
dB-decibel
dyn-dyne* (newton)
E-exa (10 $0^{19}$ )
erg-erg* (joule)
$\mathbf{e V}$-electronvolt
F-farad
${ }^{\circ} \mathbf{F}$-degree Fahrenheit
f—femto ( $10^{-15}$ )
fc-footcandle* (lux)
fL-footlambert* (candela per square meter)
ft -foot
$\mathbf{f t}^{2}-$ square foot
$\mathrm{ft}^{3}$-cubic foot
ft ${ }^{3 / 2}$ min-cubic foot per minute
$\mathrm{ft}^{3 / 3}$-cubic foot per second
$\mathrm{ft} / \mathbf{m i n}$-foot per minute
$\mathrm{ft} / \mathrm{s}$-foot per second
$\mathrm{ft} / \mathrm{s}^{2}$ - foot per second squared
ft-lbf-foot-pound (force)
G-giga ( $10^{\circ}$ ); gauss* (tesla)
g-gram
$\mathrm{g} / \mathrm{cm}^{3}$-gram per cubic centimeter
gal-gallon
Gb-gilbert* (ampere turn)
GeV -gigaelectronvolt
GHz-gigahertz
gr-gram
Gy-gray
H-henry
h -hecto ( $10^{2}$ ); hour
hp-horsepower* (watt)
Hz -hertz
in-inch
in $^{2}$-square inch
in $^{3}$-cubic inch
in/s-inch per second
J-joule
$\mathbf{J} / \mathbf{K}$ - joule per kelvin
$\mathbf{K}$-kelvin
k—kilo (10 ${ }^{\text {² }}$
kg—kilogram
$\mathbf{k H z}$-kilohertz
$k \Omega$-kilohm
$\mathbf{k m}$-kilometer
$\mathbf{k m} / \mathbf{h}$-kilometer per hour
kV —kilovolt
kVA-kilovoltampere
kW - kilowatt
$\mathbf{k W h}$-kilowathour
L-liter; lambert* (candela per square meter)
lb-pound
Im-lumen
$\mathbf{I m} / \mathbf{m}^{2}$-lumen per square meter
lm/w-lumen per watt
Im-s-lumen second
lx—lux ( $\mathrm{lm} / \mathrm{m}^{2}$ )
M—mega (10')
$\mathbf{M e V}$-megaelectronvolt
$\mathbf{M H z}$-megahertz
M $\Omega$-megohm
Mx—maxwell* (Weber)
My—myria* ( $10^{4}$ )
$\mathbf{m}$-meter; milli $\left(10^{-3}\right)$
$\mathbf{m}^{\mathbf{2}}$-square meter
$\mathbf{m}^{3}$-cubic meter
$\mathbf{m}^{3 / s}$-cubic meter per second
$\mathbf{m A}$-milliampere
mH-millihenry
mho-mho* (siemens)
$\mathbf{m L}$-milliliter
mm-millimeter
ms-millisecond
$\mathbf{m V}$-millivolt
$\mathbf{m W}$-milliwatt
$\mathbf{m i} / \mathbf{h}$-mile per hour
mil—mil (0.001 in)
min-minute (time)
mol-mole
$\mathbf{N}$-newton
n-nano (10-")
$\mathbf{N} \cdot \mathbf{m}$-newton-meter
$\mathbf{N} / \mathbf{m}^{\mathbf{2}}$-newton per square meter* (pascal)
$\mathrm{N} \cdot \mathrm{s} / \mathrm{m}^{2}$-newton-second per square meter
nA-nanoampere
$\mathbf{n F}$-nanofarad
nm-nanometer
ns-nanosecond
Oe-oersted* (ampere per meter)
$\mathbf{P}$ —peta ( $10^{\prime \prime}$ ); poise* (pascal second)
$\mathbf{P a}$-pascal
p-pico (10-12)
pF—picofarad
pt—pint
pW-picowatt
qt -quart
$\mathbf{R}$-roentgen
${ }^{\circ} \mathbf{R}$-degree Rankine
rad—radian
rd—rad* (gray)
r/min-revolutions per minute
$r / s$-revolutions per second
$\mathbf{S}$-siemens ( $\Omega^{-1}$ )
$s$-second time
sr-steradian
T-tera ( $10^{12}$ ); tesla
u-(unified) atmoic mass unit
V-volt
V/A-voltampere
$\mathbf{V} / \mathbf{m}$-volt per meter
var-var
W-watt
$\mathbf{W} /(\mathbf{m} \cdot \mathbf{K})$-watt per meter kelvin
$\mathbf{W} / \mathbf{s r}$-watt per steradian
$\mathbf{W} /\left(\mathrm{sr} \cdot \mathrm{m}^{2}\right.$ ) - watt per steradian-square meter
Wb-weber (V•s)
Wh-watt-hour
yd-yard
$\mathbf{y d}^{2}$-square yard
yd $^{3}$-cubic yard
$\mu$-micro ( $10^{-6}$ )
$\mu \mathbf{A}$-microampere
$\mu \mathbf{F}$-microfarad
$\mu \mathbf{H}$-microhenry
$\mu \mathrm{m}$-micrometer
$\mu s$-microsecond
${ }^{\circ}$-degree (plane angle)
'-minute (plane angle)
"-second (plane angle)

## Abbreviations

AC-alternating current
AF-audiofrequency
AFC-automatic frequency control
AGC-automatic gain control
AM—amplitude modulation
amm-ammeter
amp-ampere
$\mathbf{a m p} \mathbf{~ h r}$-ampere hour
ampl-amplifier
ampid-amplitude
ANL-automatic noise limiter
ant-antenna
APC-automatic phase control
ASCII-American Standard Code for
Information Interchange
assy-assembly
atten-attenuation; attenuator
aud-audible; audio
auto-automatic; automobile
aux-auxiliary
AVC—automatic volume control
avg-average
AWG-American Wire Gage
BA - Buffer amplifier
bal-balance
BC—broadcast
BFO-beat frequency oscillator
bnd-band
BO-blocking oscillator
bp-bandpass
buz-buzzer
bw-bandwidth
byp-bypass
B\&S—Brown \& Sharpe Wire Gage
Btu-British thermal unit
cal-calibrate
cap-capacitor
carr-carrier
cath-cathode
CB-common base
CC-color code
CCW-counterclockwise
CE-common emitter
cermet-ceramic metal element
$\mathbf{C F}$-cathode follower
chan-channel
ckt-circuit
CRT-cathode-ray tube
c/s-cycle per second
CT-center tap
C to C-center to center
CW - continuous wave; clockwise
cy-cycle
C-capacitance; capacitor; collector; coulomb
${ }^{\circ} \mathbf{C}$-Celsius temperature scale
DB-double break
dblr-doubler
dB-decibel
DC-direct current; double contact
DCC-double cotton-covered
deg-degree
degusg-degaussing
demod-demodulator
det-detail; detach
DF - direction finder
disc-disconnect
disch-discharge
DL-delay line
dly-delay
dmgz - demagnetize
dmr-dimmer
DP-double-pole
DPBC-double-pole, back-connected
DPDT - double-pole, double-throw
DPFC-double-pole, front-connected
dplxr-duplexer
DPST-double-pole, single-throw
DPSW-double-pole switch
DSB-double-sideband
DSC-double silk-covered
DSSB - double single-sideband
DT-double throw

DTVM-differential thermocouple voltmeter
dty cy-duty cycle
dyn-dynamo
dynm-dynamotor
dynmt-dyamometer
D-drain; duty factor; electric flux density
EBCDIC-extended binary-coded decimal interchange code
EC-enamel covered
ECO-electronic checkout
EDT-electronic discharge tube
EF-emitter follower
elctd-electrode
elec-electric
elek-electronic
elex-electronics
EM—electromagnetic-epitaxial mesa
EMF-electromotive force
emsn-emission
EMT-electrical metallic tubing
emtr-emitter
engy-energy
env-envelope
EP-epitaxial planar
ER-electrical resistance
ERP-effective radiated power
es-electrostatic
EVM-electronic voltmeter
EVOM-electronic voltohmmeter
exctr-exciter
E—east; emitter; voltage
f-frequency; force
FATR-fixed autotransformer
FB-fuse block
fdbk-feedback
FF-flip-flop
fil-filament
FM-frequency modulation
foc-focus
freq chg-frequency changer
freq con-frequency converter
freqm-frequency meter
FSC-full scale
fu-fuse
fubx-fuse box
fuhlr-fuse holder
FV-full voltage
FW-full wave
${ }^{\circ} \mathbf{F}$-Fahrenheit temperature scale
FET—field-effect transistor
g-grounded
ga-gage; graphic ammeter
galvnm-galvanometer
gdlk-grid leak
glpg-glowplug
gnd-ground
G-gain; gate
GMT-Greenwich mean time
hdst-headset
HF - high frequency
HFO-high-frequency oscillator
hifi-high fidelity
hkp-hook-up
hndst-handset
hp-high pass; high pressure; horsepower
HSD-hot side
HT-high tension
HV-high voltage
HVR-high-voltage regulator
hyb-hybrid
hyp-hypotenuse
ID-inside diameter
IF-intermediate frequency
illum-illuminate
impd-impedance
imprg-impregnate
incand-incandescent
incr-increase, increment
ind-indicate
ind $\mathbf{l p}$-indicating lamp
inf-infinite; infinity
inp-input
insp-inspect
inst-install; installation
instm-instrumentation
instr-instrument
insul-insulate; insulation
intercom-intercommunicating; intercommunication
inv-inverter
I/O-input-output
IR-insulation resistance
IT-insulating transformer
I-current
IC-integrated circuit
IGFET - insulated-gate field-effect transistor
JB-junction box
jet-junction
jk-jack
JAN-Joint Army-Navy
JANAF - Joint Army-Navy-Air Force
JFET-junction field-effect transistor
K-dielectric constant
kn sw-knife switch
KO-knock out
$\mathbf{k W h m}$ - kilowatt-hour meter
I -length; inductance; inductor; luminance
lam-laminate
lc-line-carrying
LF-low frequency
LFO-low-frequency oscillator
LH—left hand
lim-limit
lim sw-limit switch
LIRLY - load-indicating relay
Ikg—leakage
Ikrot-locked rotor
Ilres-load-limiting resistor
LO-local oscillator
loff-leakoff
$\mathbf{L P}$-low pass
LPO-low power output
LR-load resistor (relay)
LSB - lower sideband
LSR-load-switching resistor
It sw-light switch
lyr-layer
LSHI-large-scale hybrid integration
LSI-large-scale integration
m—magnaflux; mode
MA - mecury arc
mag - magnet; magnetic
mag amp-magnetic amplifier
mag mod - magnetic modulator
MC-momentary contact; multichip
mdl-module
melec-microelectronics
MF—microfilm
mg - magnetic armature
mgn-magneto; magnetron
mic-microphone
mom-momentary
mt-mount
MOS—metal-oxide semiconductor
MOSFET - metal-oxide semiconductor field-
effect transistor
NC—No coil; no connection; normally closed
nelec-nonelectric
neut-neutral
$\mathbf{N F}$ —noise figure; noise frequency
nfsd-nonfused
nmag - nonmagnetic
NO-normally open
NOL—normal overload
nom-nominal
norm-normal
ntn-neutron
nyl-nylon
$\mathbf{N}$-north
OC-over current
OCO-open-close-open
OCR-over-current relay
ohm-ohmmeter
opr-operate
ORLY - overload relay
ose-oscillate; oscillator
OSMV - one-shot multivibrator
out-output
ovld-overload
ovrd-override
p-pole; probe
PA - pulse amplifier
PAM-pulse-amplitude modulation
PB SW - pull-button switch
PC-printed circuit

PCM — pulse-code modulation; pulse-count modulation
pet-percent
PDM-pulse-duration modulation
PEC—photoelectric cell
pelec-photoelectric
pent-pentode
permb-permeability
$\mathbf{P F}$ - power factor; pulse frequency
PFM-pulse-frequency modulation
pF-picofarad
ph-phase
phen-phenolic
phm-phase meter
PIM-pulse-interval modulation
pk-peak
PLB-pull button
plnr-planar
pls-pulse
plyph—polyphase
plz-polarize
plzn-polarization
PNP-positive-negative-positive
pos-positive
pot-potentiometer
pr-pair
preamp-preamplifier
pri-primary
PRV - peak reverse voltage
psiv-passive
PU—pickup
PVC-polyvinyl chloride
pwr-power
pwr sply-power supply
qtz-quartz
Q-merit of a capacitor or coil; quantity of electricity
$\mathbf{r}$-radius
rad—radio
redr-recorder
rev-receive
revr-receiver
rechrg-recharge
rect-rectifier
ref—reference
reg-regenerate
res-resistor
resn-resonant
rev cur-reverse current
$\mathbf{R F}$-radiofrequency
RFC-radiofrequency choke
RFI-radiofrequency interference
rgltr-regulator
RH—right hand
RIFI-radio interference field intensity
rinsul—rubber insulation
RLY - relay
rms-root mean square
rmt-remote
rot-rotate
rpm-revolutions per minute
rps-revolutions per second
rpt-repeat
rtr-rotor
RTTY—radio teletypewriter
$\mathbf{R}$-resistance; resistor
$\mathbf{R C}$-resistance-capacitance
RC cpld-resistance-capacitance coupled
$\mathbf{R L}$-resistance-inductance
RLC-resistance-inductance-capacitance
RTL—resistor-transistor logic
SB—sideband
SC—single contact
SCC—single-conductor cable; single cotton-
covered
SCE-single cotton enamel
schem-schematic
SCR-short-circuit ratio
scrterm-screw terminal
sec-second; secondary
sel-selector
semicond-semiconductor
sens-sensitive; sensitivity
seq-sequence
servo-servomechanism
sft - shaft
sh-shunt
SHF - superhigh frequency
shld—shield; shielding
short-short circuit
SHTC—short time constant
sig-signal
sig gen - signal generator
slp-slope
siv-sleeve
SLWL—straight-line wavelength
SNR-signal-to-noise ratio
snsr-sensor
sol-solenoid
SP—single pole
spdr-spider
SPDT-single-pole, double-throw
SPDT SW-single-pole, double-throw switch
spk-spike
spkr-speaker
SPST - single-pole, single-throw
SPST SW-single-pole, single-throw switch
SP SW - single-pole switch
sq-square
sqcq-squirrel cage
sqw-square wave
SR—slip ring; split ring
SRLY - series relay
SS—subsystem
SSB-single-sideband
SSBO-single swing blocking oscillator
SSC-single silk-covered
SSW-synchro switch
ST-sawtooth; Schmitt trigger; single throw
STALO-stabilized local oscillator
STAMO-stabilized master oscillator
st \& sp-start and stop
stbscp-stroboscope
stby-standby
stdf—standoff
subassy - subassembly
submin-subminiature
substr-substrate
sup cur-superimposed current
suppr-suppressor
svmtr-servomotor
svo-servo
sw-shortwave; switch
swbd—switchboard
swgr-switchgear
swp-sweep
swp exp-sweep expand
swp gen-sweep generator
swp integ - sweep integrator
SWR-standing-wave ratio (voltage)
sym-symbol
syn-synchronous
sync-synchronize
sys-system
syncap-synchroscope
S-signal power; voltage standing-wave ratio
SCR-semiconductor-controlled rectifier
SH - shield (electronic device)
SWG-Stubs Wire Gage
t-temperature; time
tach-tachometer
TB-terminal board
TC-thermocouple; time constant
TCU-tape control unit
tel-telephone
telecom-telecommunications
temp-temperature
templ-template
term-terminal
tet-tetrode
TF—thin film
TFT-thin-film transistor
thermo-thermostat
thms-thermistor
thrm-thermal
thymo-thyratron motor
thyr-thyristor
tlg-telegraph
tlm-telemeter
tlmy -telemetry
TM-temperature meter
TMX - telemeter transmitter
tpho-telephotograph
tpr-teleprinter
TRF - tuned radiofrequency
tsteq-test equipment

T SW - temperature switch; test switch
TT—teletype
TTY-teletypewriter
TV-television
TVM-tachometer voltmeter
TS—telegraph system
UF - ultrasonic frequency
UHF - ultrahigh frequency
undc-undercurrent
undf-underfrequency
unf-unfused
unrgltd-unregulated
USB - upper sideband
util-utility
UJT-unijunction transistor
USG—United States Gage
$\mathbf{v}$-vertical, voltage
vac-vacuum
vam-voltammeter
var-variable; varistor
varhm-var-hour meter
varistor-variable resistor
VC—voice coil
VCO-voltage-controlled oscillator
VD-voltage drop
vdet - voltage detector
vern-vernier
VF-variable frequency; voice frequency
VFO-variable-frequency oscillator
vfreq clk - variable-frequency clock
VHF - very high frequency
vib-vibrate; vibration
vid—video; visual
vidamp-video amplifier
VF-video frequency
VLF - very low frequency
vm-voltmeter
vo-voice
vol-volume
VOM-volt-ohm-milliammeter
VR-voltage regulator
VRLY - voltage relay
VSM-vestigial-sideband modulation
VSWR-voltage standing-wave ratio

VT-vacuum tube
VTVM-vacuum-tube voltmeter
VOX - voice-operated transmitter keyer
VU-volume unit
w-wide
wb-wide band
wd-watt demand meter
wdg-winding
wfr-wafer
WG-waveguide; wire gage
WHIDM - watt-hour demand meter
WHM - watt-hour meter
WL-wavelength
WM - wattmeter
wnd-wound
wpg-wiping
WR-wall receptacle
wrg-wiring
wtrprf - waterproof
WV-working voltage
ww-wire-wound
$\mathbf{X}$-reactance
$\mathbf{X}_{\mathrm{c}}$-capacitive reactance
$\mathbf{X}_{\mathbf{1}}$-inductive reactance
$\mathbf{y}$-admittance
yr-year
ZA-zero adjusted
Z-impedance; zone
1/e-single conductor
$1 \mathbf{P H}$-single-phase
3/C-three-conductor
3P-three-pole
3PDT - three-pole, double-throw
3PDT SW - three-pole, double-pole switch
3PH-three-phase
3PST-three-pole, single-throw
3PST SW-three-pole, single-throw switch
3W -three-wire
3way-three-way
$4 / \mathrm{C}$-four conductor
4P-four-pole
4PIDT - four-pole, double-throw
4PDT SW-four-pole, double-throw switch
4PST - four-pole, single-throw

4PST SW - four-pole, single-throw switch
4W-four-wire
4way - four-way

## SEMICONDUCTOR ABBREVIATIONS

The following abbreviations have been adopted for use with semiconductor devices.
$\alpha$-alpha, common-base short-circuit current gain
$B, b$-base electrode for units employing a single base
$b_{1}, b_{2}$, etc.-base electrodes for more than one base
B-beta, common-emitter short-circuit current gain
$B V_{R}$-breakdown voltage, reverse
C, $c$-collector electrode
$\boldsymbol{C}_{\mathrm{cb}}$-interterminal capacitance, collector-tobase
$\boldsymbol{C}_{\mathrm{cr}}$-interterminal capacitance, collector-toemitter
$\boldsymbol{C}_{\mathrm{ds}}$-drain-source capacitance, with gate connected to the guard terminal of a threeterminal bridge
$\boldsymbol{C}_{\text {d } 50}$-open-circuit drain-source capacitance
$C_{\mathrm{du}}$-drain-substrate capacitance, with gate and source connected to the guard terminal of a three-terminal bridge
$C_{\mathrm{ch}}$-interterminal capacitance, emitter-to-base
$C_{\mathrm{kto}}$-open-circuit gate-drain capacitance
$C_{\text {gin }}$-open-circuit gate-source capacitance
$C_{\text {ibo }}$-open-circuit input capacitance (common base)
$C_{b s}$-short-circuit input capacitance (common base)
$\boldsymbol{C}_{\text {ito }}$-open-circuit input capacitance (common emitter)
$C_{\text {iss }}$-short-circuit input capacitance (common emitter)
$C_{\text {iss }}$ - gate-source capacitance, with drain shortcircuited to source
$C_{\text {ato }}$-open-circuit output capacitance (common base)
$C_{\text {bbs }}$-short-circuit output capacitance (common base)
$C_{\text {od }}$-short-circuit output capacitance (gatedrain short-circuited to AC)
$C_{\text {sev }}$-open-circuit output capacitance (common emitter)
$C_{\text {uss }}$-short-circuit output capacitance (common emitter)
$C_{\mathrm{uss}}$-drain-source capacitance, with gate short-circuited to source
$C_{\text {ros }}$-short-circuit reverse transfer capacitance (common base)
$C_{\text {ran }}$-short-circuit reverse transfer capacitance (common collector)
$\boldsymbol{C}_{\text {ras }}$-short-circuit reverse transfer capacitance (common emitter)
$C_{\mathrm{rw}}$-drain-gate capacitance, with the source connected to the guard terminal of a threeterminal bridge
$D$-duty cycle
$d$-damping coefficient
$E, \boldsymbol{e}$-emitter electrode
$f_{\mathrm{nb}}$-small-signal, short-circuit, forwardcurrent, transfer-ratio cutoff frequency (common base)
$f_{\text {hic }}$-small-signal, short-circuit, forwardcurrent, transfer-ratio cutoff frequency (common collector)
$f_{\text {hif }}$-small-signal, short-circuit, forwardcurrent, transfer-ratio cutoff frequency (common emitter)
$f_{\text {max }}$-maximum frequency of oscillation
$f_{1}$-transition frequency
$g_{\text {MB }}$-static transconductance (common base)
$g_{\mathrm{mb}}$-small-signal transconductance (common base)
$g_{\mathrm{mc}}$-static transconductance (common collector)
$g_{\mathrm{mc}}$-small-signal transconductance (common collector)
$\boldsymbol{g}_{\mathrm{m}}$ - static transconductance (common emitter)
$\boldsymbol{g}_{\mathrm{me}}$-small-signal transconductance (common emitter)
$G e$-germanium
$G_{\mathrm{Pu}}$-large-signal average power gain (common base)
$G_{\mathrm{pb}}$-small-signal average power gain (common base)
$G_{\mathrm{PC}}$-large-signal average power gain (common collector)
$G_{\mathrm{pc}}$-small-signal average power gain (common collector)
$\boldsymbol{G}_{\mathrm{PE}}$-large-signal average power gain (common emitter)
$\boldsymbol{G}_{\mathrm{pr}}$-small-signal average power gain (common emitter)
$G_{\mathrm{pr}}$-small-signal insertion power gain, common gate
$G_{\mathrm{ps}}$-small-signal insertion power gain, common source
$G_{\mathrm{IB}}$-large-signal transducer power gain (common base)
$\boldsymbol{G}_{1 \mathrm{~b}}$-small-signal transducer power gain (common base)
$\boldsymbol{G}_{\mathrm{rr}}$-large-signal transducer power gain (common collector)
$\boldsymbol{G}_{\mathrm{tc}}$-small-signal transducer power gain (common collector)
$G_{17}$-large-signal transducer power gain (common emitter)
$G_{\text {te }}$-small-signal transducer power gain (common emitter)
$G_{t z}$-small-signal transducer power gain, common gate
$\boldsymbol{G}_{1}$-small-signal transducer power gain, common source
$h_{\mathrm{rb}}$-static value of the forward-current transfer ratio (common base)
$\boldsymbol{h}_{\mathrm{th}}$-small-signal, short-circuit, forwardcurrent transfer ratio (common base)
$H_{\mathrm{r}}$-static value of the forward-current transfer ratio (common collector)
$\boldsymbol{h}_{\text {fc }}$-small-signal, short-circuit, forwardcurrent transfer ratio (common collector)
$h_{\text {te }}$-static value of the forward-current transfer ratio (common emitter)
$\boldsymbol{h}_{\mathrm{fe}}$-small-signal, short-circuit, forwardcurrent transfer ratio (common emitter)
$h_{\text {FeI }}$-inherent large-signal, forward-current, transfer ratio
$\boldsymbol{h}_{18}$-static value of the input resistance (common base)
$\boldsymbol{h}_{\mathrm{in}}$-small-signal value of short-circuit input impedance (common base)
$h_{\mathrm{IC}}$-static value of the input resistance (common collector)
$h_{\mathrm{ic}}$-small-signal value of short-circuit input impedance (common collector)
$h_{11}$ - static value of the input resistance (common emitter)
$h_{\mathrm{ic}}$-small-signal value of short-circuit input impedance (common emitter)
$h_{\text {ic }}$ (real) -real part of small-signal value of short-circuit input impedance (common emitter)
$h_{\mathrm{ob}}$-static value of open-circuit output conductance (common base)
$\boldsymbol{h}_{\mathrm{ub}}$-small-signal value of open-circuit output admittance (common base)
$\boldsymbol{h}_{\mathrm{oc}}$-static value of open-circuit output conductance (common collector)
$\boldsymbol{h}_{\text {os }}$-small-signal value of open-circuit output admittance (common collector)
$\boldsymbol{h}_{\text {OE }}$-static value of open-circuit output conductance (common emitter)
$h_{\text {or }}$-small-signal value of open-circuit output admittance (common emitter)
$h_{\mathrm{rb}}$-small-signal value of open-circuit, reversevoltage transfer ratio (common base)
$\boldsymbol{h}_{\mathrm{rc}}$-small-signal value of open-circuit, reversevoltage transfer ratio (common collector)
$\boldsymbol{h}_{\mathrm{rc}}$-small-signal value of open-circuit, reversevoltage transfer ratio (common emitter)
$I, i$-intrinsic region of a device (where neither holes nor electrons predominate)
$I_{\mathrm{B}}$-base current (DC)
$I_{\mathrm{n}}$-base current (rms)
$i_{\mathrm{B}}$-base current (instantaneous)
$\boldsymbol{I}_{\mathrm{Ho}}$-breakover current, direct
$\boldsymbol{I}_{\mathbf{I}}$-collector current (DC)
$I_{\mathrm{c}}$-collector current (rms)
$i_{\text {c }}$-collector current (instantaneous)
$I_{\text {(80 }}$-current cutoff current (DC), emitter open
$I_{\text {ce }}$-collector cutoff current (DC), base open
$\boldsymbol{I}_{\text {ceR }}$-collector cutoff current (DC), with specified resistance between base and emitter
$I_{\text {ces }}$-collector cutoff current (DC), with base short-circuited to emitter
$I_{\text {cz }}$-collector cutoff current with specified voltage between base and emitter
$\boldsymbol{I}_{\mathrm{cx}}$-collector current (DC), with specified circuit between base and emitter
$I_{\mathrm{Co}}-$ collector leakage current (cutoff current)
$I_{\mathrm{n}}$ - drain current (DC)
$\boldsymbol{I}_{\text {Dotrt }}$-drain cutoff current
$I_{\mathrm{Dsk}}$-drain current, (external) gate-source resistance specified
$I_{\mathrm{p} \text { ss }}$-drain current, zero gate voltage
$I_{\mathrm{Dsx}}$-drain current, gate-source condition specified
$\boldsymbol{I}_{\mathrm{k}}$-emitter current (DC)
$I_{\mathrm{e}}$ - emitter current (rms)
$i_{\mathrm{i}}$-emitter current (instantaneous)
$\boldsymbol{I}_{\text {EBO }}$-emitter cutoff current (DC), collector open
$\boldsymbol{I}_{\mathrm{EC}\left(\mathrm{coss}_{\mathrm{s}}\right)}$-emitter-collector offset current
$\boldsymbol{I}_{\mathrm{Ecs}}$-emitter cutoff current (DC), base shortcircuited to collector
$\boldsymbol{I}_{\text {ELE }}$-emitter cutoff current (double-emitter transistors)
$I_{r}$-forward current (DC)
$I_{\mathrm{t}}$-forward current, alternating component
$i_{\mathrm{r}}$-forward current (instantaneous)
$\boldsymbol{I}_{\text {Fan) }}$-forward current, DC value with alternating component
$I_{\mathrm{rG}}$-forward gate current (DC)
$I_{\mathrm{rcm}}$-peak forward gate current
$I_{\mathrm{FM}}$-forward current, peak total value
$I_{\text {riov }}$-forward current, overload
$I_{\mathrm{rsM}}$-forward current, peak repetitive
$I_{\mathrm{rsm}}$-forward current, peak surge
$I_{6}$ - gate current (DC)
$I_{\mathrm{CF}}$-forward gate current
$I_{\mathrm{GR}}$-reverse gate current
$I_{\mathrm{H}}$-holding current (DC)
$\boldsymbol{I}_{\mathrm{i}}$-infection-point current
$I_{0}$-average output rectified current
$\boldsymbol{I}_{\mathrm{ov}}$-overload on-state current
$I_{\mathrm{P}}$-peak-point current (double-base transistor)
$I_{\mathrm{R}}$-reverse current (DC)
$I_{\mathrm{r}}$-alternating component of reverse current (rms value)
$i_{\mathrm{R}}$-reverse current (instantaneous)
$i_{\text {RIEGG }}$-reverse recovery current
$I_{\mathrm{RRM}}$-peak reverse current, repetitive
$I_{\mathrm{kr}(\mathrm{ms})}$-reverse current, total rms value
$I_{5}$-source current
$\boldsymbol{I}_{\text {sins }}$-source current, zero gate voltage
$\boldsymbol{I}_{\mathrm{SDx}}$-source current, gate-drain condition specified
$I_{\text {TRM }}$-peak on-state current, repetitive
$I_{\mathrm{T} \times \mathrm{m}}$-on-state current surge (nonrepetitive)
$I_{u}$-substate current
$I_{1}$-valley-point current (double-base transistor)
$I_{z}$-regulator current, reference current (DC)
$I_{z \mathrm{~K}}$-regulator current, reference current (DC nar breakdown knee)
$\boldsymbol{I}_{\mathrm{zm}}$-regulator current, reference current (DC maximum rated current)
$\boldsymbol{K}_{\mathrm{o}}$-thermal derating factor
$L_{\mathrm{c}}$-conversion loss
$M$-figure of merit
$N, n$-region of a device where electrons are the majority carriers
$N F$-noise figure
$N F_{0}$-overall noise figure
$N R_{0}$-output noise ratio
$P, p$-region of a device where holes are the majority carriers
$\boldsymbol{P}_{B E}$-total power input (DC or average) to the base electrode with respect to the emitter electrode
$\boldsymbol{P}_{\mathrm{RK}}-$ total power input (instantaneous) to the base electrode with respect to the emitter electrode
$P_{C \mathrm{~B}}$-total power input (DC or average) to the collector electrode with respect to the base electrode
$\boldsymbol{P}_{\mathrm{CB}}$ - total power input (instantaneous) to the collector electrode with respect to the base electrode
$\boldsymbol{P}_{\mathrm{ct}}$-total power input (DC or average) to the collector electrode with respect to the emitter electrode
$P_{\mathrm{cr}}=$ total power input (instantaneous) to the collector electrode with respect to the emitter electrode
$\boldsymbol{P}_{\mathrm{Ds}}$-drain-source power dissipation
$\boldsymbol{P}_{\mathrm{kB}}$-total power input (DC or average) to the emitter electrode with respect to the base electrode
$P_{\mathrm{E}:}$-total power input (instantaneous) to the emitter electrode with respect to the base electrode
$\boldsymbol{P}_{\mathrm{F}}$-forward power loss (DC)
$p_{\mathrm{r}}$-forward power loss (instantaneous)
$P_{\mathrm{tm}}$-forward power loss, total peak value
$P_{1 B}$-large-signal input power (common base)
$\boldsymbol{P}_{\text {it }}$-small-signal input power (common base)
$\boldsymbol{P}_{\mathrm{ti}}$-large-signal input power (common collector)
$\boldsymbol{P}_{\text {ic }}$-small-signal input power (common collector)
$\boldsymbol{P}_{\text {It }}$-large-signal input power (common emitter)
$\boldsymbol{P}_{\mathrm{i} \text { - }}$-small-signal input power (common emitter)
$\boldsymbol{P}_{\mathrm{OB}}$-large-signal output power (common base)
$\boldsymbol{P}_{\mathrm{ab}}$-small-signal output power (common base)
$\boldsymbol{P}_{\mathrm{oc}}$-large-signal output power (common collector)
$\boldsymbol{P}_{\mathrm{oc}}$-small-signal output power (common collector)
$\boldsymbol{P}_{o s}$-large-signal output power (common emitter)
$\boldsymbol{P}_{\text {ore }}$-small-signal output power (common emitter)
$\boldsymbol{P}_{\mathrm{R}}$-reverse power loss
$p_{\mathrm{R}}$-reverse power loss (instantaneous)
$P_{\mathrm{sm}}$-surge nonrepetitive power
$P_{1}$-total power input (DC or average) to all electrodes
$p_{\mathrm{T}}$-total power input (instantaneous) to all electrodes
$Q_{s}$-recovered charge (stored charge)
$R_{\mathrm{B}}$-external base resistance
$r_{\text {RB }}$-resistance between two bases, emitter zero (double-base transistor)
$r_{\mathrm{b}}{ }^{\prime} \mathbf{C}_{\mathrm{c}}$-collector-base time constant
$R_{\mathrm{C}}$-external collector resistance
$\boldsymbol{r}_{\text {ck:sur) }}$-collector-to-emitter saturation resistance
$r_{\mathrm{d}}$-damping resistance
$\boldsymbol{R}_{\mathrm{F}}$-external emitter resistance
$\boldsymbol{R}_{\mathrm{FB}}$-emitter-base junction resistance (assume $4 \Omega$ average)
$r_{\text {rlc } 2}$-small-signal emitter-emitter on-state resistance (double emitter transistors)
$r_{i}$-dynamic resistance at inflection point
$R_{\mathrm{t}}$-load resistance
$\boldsymbol{R}_{f}-$ thermal resistance
$\boldsymbol{R}_{8 \mathrm{CA}}$-thermal resistance, case-to-ambient
$\boldsymbol{R}_{\theta, \mathrm{A}}$-thermal resistance, junction-to-ambient
$\boldsymbol{R}_{\text {共 }}$-thermal resistance, junction-to-case
$r_{T}$-slope resistance
Si-silicon
$\boldsymbol{T}$-temperature
$T_{A}$-ambient temperature
$\boldsymbol{T}_{\mathrm{c}}$-case temperature
$t_{\mathrm{d}}$-delay time
$t_{\mathrm{t}}$-fall time
$t_{\mathrm{t}}$-forward recovery time
$\boldsymbol{T}_{\mathrm{j}}$-junction temperature
$t_{\text {off }}$-turn-off time
$t_{\text {on }}$-turn-on time
$\boldsymbol{T}_{\text {opr }}$-operating temperature
$t_{\mathrm{p}}$-pulse time
$t_{r}$-rise time
$t_{n}$-reverse recovery time
$t$,-storage time
TSS - tangential signal sensitivity
$T_{\text {stip }}$-storage temperature
$t_{u}$ - pulse average time
$V_{\mathrm{B}}$-base voltage (DC)
$V_{\mathrm{BB}}$-base supply voltage ( DC )
$V_{B C}$-base-to-collector voltage (DC)
$V_{\mathrm{bc}}$-base-to-collector voltage (rms)
$v_{\mathrm{bc}}$-base-to-collector voltage (instantaneous)
$V_{\mathrm{RF}}$-base-to-emitter voltage (DC)
$V_{\text {Be(sat) }}$-saturation voltage, base to emitter
$V_{\mathrm{bc}}$-base-to-emitter voltage (rms)
$v_{\mathrm{bc}}$-base-to-emitter voltage (instantaneous)
$V_{\mathrm{Bo}}$-breakover voltage (instantaneous)
$V_{(\operatorname{RR}) \text { CBo }}$-breakdown voltage, collector-to-base, emitter open
$V_{\text {aktaro }}$-breakdown voltage, collector-toemitter, base open
$V_{\text {(bricer }}$-breakdown voltage, collector-toemitter, with specified resistance between base and emitter
$V_{\text {(BR)CEs }}$-breakdown voltage, collector-toemitter, with base short-circuited to emitter
$V_{(\mathrm{Br}) \boldsymbol{c} \boldsymbol{x}}$ - breakdown voltage, collector-toemitter, voltage between base and emitter
$\boldsymbol{V}_{\text {(Br)crx }}$ - breakdown voltage, collector-toemitter, circuit between base and emitter
$V_{\text {(нкено }}-$ breakdown voltage, emitter-to-base, collector open
$V_{\text {(вR) })}-$ breakdown voltage, emitter-tocollector, base open (formerly $B V_{\text {zco }}$ )
$V_{\text {(BR)F:1:2 }}$-breakdown voltage, emitter-to-emitter (double-emitter transistor)
$\boldsymbol{V}_{(\mathrm{brec}) \mathrm{ss}}$-breakdown voltage, gate-to-source, drain short-circuited to source
$V_{\text {(BRIGSsi }}$-breakdown voltage, forward voltage applied to gate-source, drain shortcircuited to source
$V_{(\mathrm{RR}) \mathrm{ciss}_{\mathrm{s}}}$-breakdown voltage, reverse voltage to gate-source, drain short-circuited to source
$V_{\text {(BR)R }}$-reverse breakdown voltage
$V_{\text {R2B1 }}$-bias DC voltage between base 2 and base 1 (double-base transistor)
$V_{c}$-collector voltage (DC)
$V_{C B}$-collector-to-base voltage (DC)
$V_{\text {Cr(f) })}$-DC open-circuit voltage, floating potential, collector-to-base
$V_{\mathrm{cb}}$-collector-to-base voltage (rms)
$\boldsymbol{v}_{\text {cb }}$-collector-to-base voltage (instantaneous)
$\boldsymbol{V}_{\text {cио }}$ - collector-to-base voltage (DC), with emitter open
$V_{\text {c: }}$ - collector supply voltage (DC)
$V_{\mathrm{cf}}$-collector-to-emitter voltage (DC)
$V_{\mathrm{cc}}$-collector-to-emitter voltage (rms)
$V_{\text {c:(fi) }}-\mathrm{DC}$ open-circuit voltage, floating potential, collector-to-emitter
$V_{\text {ceo }}$-collector-to-emitter voltage (DC), with base open
$\boldsymbol{V}_{\text {CER }}$-collector-to-emitter voltage (DC), with specified resistance between base and emitter
$V_{\text {crs }}$-collector-to-emitter voltage (DC), with base short-circuited to emitter
$V_{C E(s a)}$-saturation voltage, collector to emitter
$V_{\text {ch }}$ - collector-to-emitter voltage (DC), with voltage between base and emitter
$V_{\mathrm{crx}}$-collector-to-emitter voltage (DC), with circuit between base and emitter
$V_{\mathrm{D}}$-off-state voltage (direct)
$V_{\mathrm{os}}$ - drain supply voltage (DC)
$V_{\mathrm{DG}}$-drain-to-gate voltage (DC)
$V_{\mathrm{Dm}}$-peak off-state voltage
$V_{\text {DRM }}$ - peak off-state voltage repetitive
$F_{\mathrm{Ds}}$ - drain-to-source voltage (DC)
$V_{\mathrm{nsm}}$ - peak off-state voltage, nonrepetitive
$V_{\text {mu }}$-drain-to-substrate voltage (DC)
$V_{\text {owm }}$ - peak off-state voltage, working
$V_{\mathbf{E}}$-emitter voltage (DC)
$V_{\mathrm{r}:}$-emitter-to-base voltage (DC)
$V_{\text {f:Bfll }}-\mathrm{DC}$ open-circuit voltage, floating potential, emitter-to-base
$V_{\text {tuo }}$-emitter-to-base voltage (DC), with collector open
$V_{\text {ec }}$-emitter-to-collector voltage (DC)
$V_{\text {EC(n) }}-\mathrm{DC}$ open-circuit voltage, floating potential, emitter-to-collector
$V_{\mathrm{kf}}$-emitter supply voltage (DC)
$V_{F}$-forward voltage (DC)
$V_{1}$-alternating component of forward voltage (rms value)
$v_{1}$-forward voltage (instantancous)
$V_{t i}$-forward gate voltage (direct)
$V_{\text {rim }}$-peak forward gate voltage
$V_{\text {tw }}$-forward voltage, peak total value
$V_{\text {trmv }}$-forward voltage, total rms value
$V_{\text {t, }}$ - gate nontrigger (direct) voltage
$V_{\mathrm{t}, \mathrm{t}}$ - gate supply voltage (DC)
$V_{\text {(i) }}$ - gate turn-off voltage (direct)
$V_{\text {(, }}$-gate-to-source voltage (DC)
$V_{\text {amorf }}$ - gate-to-source cutoff voltage
$V_{(, \text {mut })}$-gate-to-source theshold voltage
$V_{\text {ist }}$-forward gate-to-source voltage (DC), of such polarity that an increase in its magnitude causes the channel resistance to decrease
$V_{\text {cish }}$-reverse gate-to-source voltage (DC), of such polarity that an increase in its magnitude causes the channel resistance to increase
$V_{1,1}$ - gate trigger voltage (direct)
$V_{\text {(, Itumin) }}-$ minimum gate trigger voltage
$V_{t, 1}$ - gate-to-substrate voltage (DC)
$V_{1}$-inflection-point voltage
$V_{p}$-peak-point voltage (double-base transistor)
$\boldsymbol{V}_{\mathrm{Pp}}$ —projected peak-point voltage
$V_{\mathrm{PI}}$-punch-through voltage
$V_{\mathrm{R}}$-reverse voltage (DC)
$V_{r}$-alternating component of reverse voltage (rms value)
$v_{R}$-reverse voltagc (instantaneous)
$V_{\mathrm{R}(\mathrm{rm})}$-reverse voltage, total rms value
$V_{\text {RRM }}-$ reverse voltage, maximum recurrent
$V_{\text {Rsm }}$-reverse voltage, peak transient
$V_{\mathrm{Rr}}$-reverse collector-to-base voltage, reachthrough voltage
$V_{\text {кмм }}$-reverse voltage, (peak) working
$V_{\mathrm{si}}$-source-substrate voltage
$V_{s}$-source supply voltage (DC)
$V_{\mathrm{si}}$-source-to-substrate voltage (DC)
$V_{1}$-on-state voltage, direct
$V_{1 \text { (min) }}$-minimum on-state voltage
$V_{\mathrm{ro}}$-threshold voltage
$V_{v}$-valley-point voltage (double-base transistor)
V,-regulator voltage, reference voltage (DC working voltage)
$V_{\text {m }}$-regulator voltage, reference voltage (DC at maximum rated current)
$\boldsymbol{Y}_{\mathrm{t}}$-small-signal, short-circuit forward transfer admittance, common base
$\boldsymbol{Y}_{\mathrm{te}}$-small-signal, short-circuit forward transfer admittance, common emitter
$\boldsymbol{Y}_{\mathrm{f}}$ - small-signal, short-circuit forward transfer admittance, common source
$\boldsymbol{Y}_{\mathrm{ib}}$-small-signal, short-circuit input admittance, common base
$Y_{\mathrm{ic}}$-small-signal, short-circuit input admittance, common collector
$Y_{\text {ic }}$-small-signal, short-circuit input admittance, common emitter
$\boldsymbol{Y}_{\text {uh }}$-small-signal, short-circuit output admittance, common base
$Y_{\text {uc }}$-small-signal, short-circuit output admittance, common collector
$Y_{\text {uc }}$-small-signal, short-circuit output admittance, common emitter
$Y_{\mathrm{r}}$-small-signal, short-circuit reverse transfer admittance, common base
$Y_{\text {rc }}$-small-signal, short-circuit reverse transfer admittance, common collector
$\boldsymbol{Y}_{\mathrm{re}}$-small-signal, short-circuit reverse transfer admittance, common emitter
$Z_{\mathrm{n}}$-impedance, modulator frequency load
$z_{\mathrm{kt}}$-impedance, radio frequency
$Z_{\text {tat }}$-transient thermal impedance
$Z_{\text {glatil }}$-transient thermal impedance, junction-to-ambient
$Z_{\text {в, } \mathbb{\prime}=1}$-transient thermal impedance, junction-to-case
$z$.-video impedance
$z$,-regulator impedance, reference impedance (small-signal at $I_{L}$ )
$z_{\gamma \mathrm{K}}$-regulator impedance, reference impedance (small-signal at $I_{r_{k}}$ )

## RESISTOR COLOR CODES

Both composition resistors and the smaller types of wirewound resistors are


Color-band system (two significant figures)


Body-dot system


Body-end-dot system


Dash-band system
color-coded for values. The various methods of marking the resistors are shown in Fig. 3-1. Table 3-10 gives the significance of each color.


Color-band system (three significant figures)


Dot-band system


Body-end band system


Miniature resistor code

Fig. 3-1

TABLE 3-10
Resistor Color Code

|  | Significant <br> figures | Multiplier | Tolerance (\%) | Failure rate* |
| :--- | :---: | :---: | :---: | :---: |
| Black | 0 | 1 | $\pm 20$ | - |
| Brown | 1 | 10 | $\pm 1$ | 1.0 |
| Red | 2 | 1,000 | $\pm 2$ | 0.1 |
| Orange | 3 | 10,000 | $\pm 3$ | 0.01 |
| Yellow | 4 | 100,000 | $\pm 4$ | 0.001 |
| Green | 5 | $10,000,000$ | - | - |
| Blue | 6 | $100,000,000$ | - | - |
| Violet | 7 |  | - | - |
| Gray | 8 | 0.1 | - | Solderable* |
| White | - | 0.01 | $\pm 5$ | - |
| Gold | - |  | $\pm 20$ | - |
| Silver | - |  |  |  |
| No Color |  |  |  |  |

*On composition resistor indicates failures per 1000 hours. On film resistor indicates solderable terminal.

## CAPACITOR COLOR CODES

There are several methods of color coding capacitors, depending on the type of capacitor, the age of the unit, and the manufacturer's preference. Some of the ones listed in the following are no longer in use. However, they are included for reference.

## Molded Paper Tubular Capacitors

Molded paper tubular capacitors are color coded as shown in Fig. 3-2 and Table 3-11.

## Molded Flat Paper and Mica Capacitors

Molded flat paper and mica capacitors are color coded as shown in Fig. 3-3 and Table 3-12.

## Ceramic and Molded Insulated Capacitors

Ceramic and molded insulated capacitors are color coded as shown in Fig. 3-4 and Table 3-13.


Add two zeros to signficant voitage figures One band :ndicates voltage ralugs under 1000 V

Fig. 3-2

TABLE 3-11
Molded Paper Tubular Capacitor Color Code*

| Color | First \& second <br> significant figures | Multiplier | Tolerance (\%) |
| :--- | :---: | :---: | :---: |
| Black | 0 | 1 | $\pm 20$ |
| Brown | 1 | 10 | - |
| Red | 2 | 100 | - |
| Orange | 3 | 1,000 | - |
| Yellow | 4 | 10,000 | - |
| Green | 5 | 100,000 | $\pm 5$ |
| Blue | 6 | - | - |
| Violet | 7 | - | - |
| Gray | 9 | - | $\pm 10$. |
| White | - | - | $\pm 5$ |
| Gold | - | - | $\pm 10$ |
| Silver | - |  | $\pm 20$ |
| No Color |  |  |  |

*All values in picofarads.


Molded flat paper (commercial grade)


Molded flat paper (military grade)


TABLE 3-12
Molded Flat Paper and Mica Capacitor Color Code*

| Color | Characteristic ${ }^{\dagger}$ | Capacitance |  | Tolerance (\%) | DC working voltage | Operating temperature range | Vibration grade (MIL) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1st \& 2nd sig. figs. | Multiplier |  |  |  |  |
| Black | A (EIA) | 0 | 1 | $\pm 20$ | - | -55 to $+70^{\circ} \mathrm{C}$ (MIL) | $10-55 \mathrm{~Hz}$ |
| Brown | B | 1 | 10 | $\pm 1$ | 100 (EIA) | - | - |
| Red | C | 2 | 100 | $\pm 2$ | - | -55 to $+85^{\circ} \mathrm{C}$ | - |
| Orange | D | 3 | 1,000 | - | 300 | - | - |
| Yellow | E | 4 | 10,000 (EIA) | - | - | $-5510+125^{\circ} \mathrm{C}$ | $10-2000 \mathrm{~Hz}$ |
| Green | F | 5 | - | $\pm 5$ | 500 | - | - |
| Blue | - | 6 | - | - | - | $-5510+150^{\circ} \mathrm{C}$ (MIL) | - |
| Violet | - | 7 | - | - | - | - | - |
| Gray | - | 8 | - | - | - | - | - |
| White | - | 9 | - | - | - | - | - |
| Gold | - | - | 0.1 | $\pm 0.5$ (EIA) ${ }^{\text {a }}$ | 1000 (EIA) | - | - |
| Silver | - | - | 0.01 (EIA) | $\pm 10$ | - | - | - |

*All values in picofarads.
:Denotes specifications of design involving $Q$ factors, temperature coefficients, and production test requirements.
$\ddagger$ Or +5.0 pl ; whichever is greater. All others are specified tolerance or +1.0 pl , whichever is greater.

## TABLE 3-13

## Ceramic Capacitor Color Codes*

| Color | Capacitance |  | Tolerance ${ }^{\text {t }}$ |  |  | Temperature coefficient |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $1 s t$ \& $2 n d$ sig. figs. | Multiplier | Class 1 |  | Class 2 | $p p m{ }^{\circ} \mathrm{C}$ | Significant figure | Multiplier |
|  |  |  | 10 pF or less | Over 10 pF |  |  |  |  |
| Black | 0 | 1 | $\pm 2.0 \mathrm{pF}$ | $\pm 20 \%$ | $\pm 20 \%$ | 0 | 0.0 | -1 |
| Brown | 1 | 10 | $\pm 0.1 \mathrm{pF}$ | $\pm 1 \%$ | - | -33 | - | -10 |
| Red | 2 | 100 | - | $\pm 2 \%$ | - | -75 | 1.0 | -100 |
| Orange | 3 | 1,000 | - | $\pm 3 \%$ | - | -150 | 1.5 | -1,000 |
| Yellow | 4 | 10,000 | - | - | + $100 \%,-0 \%$ | -220 | 2.0 | -10,000 |
| Green | 5 | - | $\pm 0.5 \mathrm{pl}$ | $\pm 5 \%$ | $\pm 5 \%$ | -330 | 3.3 | +1 |
| Blue | 6 | - |  | - | - | -470 | 4.7 | $+10$ |
| Violet | 7 | - | - | - | - | -750 | 7.5 | $+100$ |
| Gray | 8 | 0.01 | $\pm 0.25 \mathrm{pF}$ | - | + $80 \%,-20 \%$ | +150 to-1500 | - | $+1,000$ |
| White | 9 | 0.1 | $\pm 1.0 \mathrm{pF}$ | $\pm 10 \%$ | $\pm 10 \%$ | +100 to -750 | - | +10,000 |
| Silver | - | - | - | - | - | - | - | - |
| Gold | - | - | - | - | - | - | - | - |

[^4]

|  |  |  |
| :---: | :---: | :---: |

Tubular high capacitance

Tubular extended range temperuture compensating

Fig. 3-4

## Tantalum Capacitors

Tantalum capacitors are color coded as shown in Fig. 3-5 and Table 3-14.

1st Significant Figure 2nd Signilicant Figure


Fig. 3-5

TABLE 3-14
Tantalum Capacitor Color Codes

| Color | Ist <br> sig. fig. | 2nd <br> sig. fig. | Multiplier | Rated DC <br> voltage |
| :--- | :---: | :---: | :---: | :---: |
| Black | - | 0 | 1 | 10 |
| Brown | 1 | 1 | 10 | - |
| Red | 2 | 2 | 100 | - |
| Orange | 3 | 3 | - | - |
| Yellow | 4 | 4 | - | 6.3 |
| Green | 5 | 5 | - | 16 |
| Blue | 6 | 6 | - | 20 |
| Violet | 7 | 7 | - | - |
| Gray | 8 | 8 | 0.01 | 25 |
| White | 9 | 9 | 0.1 | 3 |
| Pink | - | - | - | 35 |

*All values in microfarads.

## Typographically Marked Capacitors

A system of typographical marking to indicate the various parameters of capacitors is becoming popular. The actual method of marking will vary with manufacturers but one group of markings will usually indicate the type, voltage, and dielectric, and another group the capacitance value and tolerance. The first two (or three) digits in the value indicate the significant digits of the value and the last digit, the multiplier or number of zeros to add to obtain the value in picofarads. An R included in the digits indicates a decimal point. A letter following the value indicates the tolerance. The significance of these letters is as follows:

$$
\begin{aligned}
& \mathrm{M}- \pm 20 \% \\
& \mathrm{~K}- \pm 10 \% \\
& \mathrm{~J}- \pm 5 \% \\
& \mathrm{Z}-+80,-20 \% \\
& \mathrm{P}-\mathrm{GMV}
\end{aligned}
$$

X - Special
$\mathrm{H}- \pm 3 \%$
G- $\pm 2 \%$
F- $\pm 1 \%$
B $- \pm 0.1 \mathrm{pF}$
C $- \pm 0.25 \mathrm{pF}$
D $- \pm 0.5 \mathrm{pF}$

## SEMICONDUCTOR COLOR CODE

The sequence numbers of semiconductor type numbers and suffix letters may use the color-coding indicated in Table 3-15. The colors conform to EIA standard for numerical values.

## ELECTRONICS SCHEMATIC SYMBOLS

The most common schematic symbols are illustrated in Fig 3-6.

TABLE 3-15
Semiconductor Color Code

| Vumber | Color | Suffix letter |
| :---: | :--- | :---: |
| 0 | black | not applicable |
| 1 | brown | A |
| 2 | red | B |
| 3 | orange | C |
| 4 | yellow | D |
| 5 | green | E |
| 6 | blue | F |
| 7 | violet | G |
| 8 | gray | H |
| 9 | white | J |



Tubes


## Tube elements



Cathode-ray tube

Fig. 3-6A. Electronics schematic symbols.


## Semiconductor devices

Fig. 3-6B. Electronics schematic symbols.


Semiconductor devices (cont)

*Decimal point (D P.) available for right hand, left hand. or universal -- must specify.

## 7-Segment led indicator



Logic symbols
Fig. 3-6C. Electronics schematic symbols.

Handbook of Electronics Tables and Formulas


Piezoelectric crystal


Batteries


## Resistors



Wiring
Inductors


Transformers


Fig. 3-6D. Electronics schematic symbols.


Capacitors


Shields


Jacks

Circuit breakers


Microphones


## Antennas



AC receptacles

| - | $0{ }^{\circ}$ | $\begin{gathered} \text { óo } \\ 0 \% 0 \end{gathered}$ | - or | $\underset{0}{1}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $5$ | $79$ | $\frac{q}{i}$ | $\frac{99}{\frac{9}{4}}$ | 010 $0$ |  |  |  |
| SPST | SPDT | DPSI | dpot | Push Button |  |  |  |
| 3-6E | lec | schem | Switches |  |  |  | $A C$ voltage sources |

Fig. 3-6E. Electronics schematic symbols.

## Chapter 4

## SERVICE AND InSTALLATION Data

## COAXIAL CABLE CHARACTERISTICS

Table 4-1 lists the most frequently used coaxial cables. The electrical specifications include the impedance in ohms, capacitance in picofarads per foot, attenuation in decibels per 100 ft and 100 m , and the outside diameter in inches or millimeters. (See page 30 for formulas.)

## TEST-PATTERN INTERPRETATION

Many television stations transmit a test pattern, a color bar pattern, or a combination of color bars and test pattern. Generally, the test pattern is transmitted before the station starts its broadcasting day. The test pattern is broadcast as a "station check of performance," indicating proper operation of the transmitter equipment. It is also a check of performance for the receiver. A person trained in electronics can see at a glance if a receiver is operating properly, and appropriate adjustments can be made on the receiver.

In the following explanation, the significance of various test patterns is given. The test pattern broadcast from the television station follows the characteristics of the Indian Head test pattern (Fig. 4-1), which has been in use since the start of television broadcasting.

The roundness of the circles ( $A$ and $G$ ) in the test pattern provide a quick check on the width, height, and linearity. Horizontal and vertical lines (B) may be used to check linearity, and diagonal lines ( $C$ ) can be used to check interlace. The vertical wedges (E) or any other pattern details in the vertical plane are used to determine horizontal resolution. Hence, they serve to check the overall video-amplifying circuits and receiver alignment. There should not be any black or white trailing edges from the vertical wedge or circle. That would indicate a problem associated with the receiver. Also, if the test pattern has a vertical wedge, the wedge has separate lines that seem to come together at a certain point and become one wide vertical line. The point where the vertical lines are no longer clear indicates the extent of horizontal resolution.

## TABLE 4-1

Coaxial Cable Characteristics

|  | Nominal |  |  | Nominal attenuation |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RG. | impedance | capactance | OD | 100 MHz | 200 MHz | 400 MHz | 900 MHz |



| 6 | 75 | 17.3 | 56.8 | 0.290 | 7.37 | 2.1 | 6.9 | 3.1 | 10.2 | - | - | 6.9 | 22.6 | CATV-MATV IF \& video |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 A | 75 | 20.5 | 67.3 | 0.336 | 7.53 | 2.9 | 9.5 | 4.3 | 14.1 | 6.5 | 21.3 | 10.1 | 33.1 | small, IF/video |
| 8 | 52 | 29.5 | 95.7 | 0.405 | 10.29 | 2.0 | 6.6 | 3.0 | 9.8 | 4.7 | 15.4 | 7.8 | 25.6 | gen. purpose |
| 8A | 52 | 29.5 | 95.7 | 0.405 | 10.29 | 2.0 | 6.6 | 3.0 | 9.8 | 4.7 | 15.4 | 7.8 | 25.6 | gen. purpose, mil. |
| 9 | 51 | 30.0 | 97.3 | 0.420 | 10.67 | 1.9 | 6.2 | 2.8 | 9.2 | 4.1 | 13.5 | 6.5 | 21.3 | gen. purpose |
| 9 B | 50 | 30.0 | 97.3 | 0.430 | 10.92 | 1.9 | 6.2 | 2.8 | 9.2 | 4.1 | 13.5 | 6.5 | 21.3 | gen. purpose, mil |
| 11 | 75 | 20.5 | 66.5 | 0.405 | 10.29 | 2.0 | 6.6 | 2.9 | 9.5 | 4.2 | 13.8 | 6.5 | 21.3 | commun. tv |
| 11 A | 75 | 20.5 | 66.5 | 0.405 | 10.29 | 2.0 | 6.6 | 2.9 | 9.5 | 4.2 | 13.8 | 6.5 | 21.3 | mil. spec. |
| 12A | 75 | 20.5 | 66.5 | 0.475 | 12.07 | 2.1 | 6.9 | 3.2 | 10.5 | 4.7 | 15.4 | 7.8 | 25.6 | with armor |
| 14A | 52 | 29.5 | 95.7 | 0.558 | 14.17 | 1.5 | 4.8 | 2.3 | 7.8 | 3.5 | 11.6 | - | - | RF power |
| 17A | 52 | 29.5 | 95.7 | 0.885 | 22.48 | 0.95 | 3.1 | 1.5 | 4.8 | 2.4 | 7.9 | - | - | gen. purpose |
| 19A | 52 | 29.5 | 95.7 | 1.135 | 28.83 | 0.69 | 2.3 | 1.1 | 3.2 | 1.8 | 5.8 | - | - | gen. purpose |
| 22B | 95 | 16.0 | 52.5 | 0.420 | 10.67 | 3.0 | 9.8 | 4.5 | 14.8 | 6.8 | 22.3 | 11.0 | 36.1 | double shield |
| 55 | 53.5 | 28.5 | 92.5 | 0.206 | 5.23 | 4.8 | 15.8 | 7.0 | 23.1 | 10.5 | 34.4 | 16.0 | 52.9 | flexible, small |
| 55B | 53.5 | 28.5 | 92.5 | 0.206 | 5.23 | 4.8 | 15.8 | 7.0 | 23.1 | 10.5 | 34.4 | 16.0 | 52.9 | double braid |
| 58 | 53.5 | 28.5 | 92.5 | 0.195 | 4.95 | 4.1 | 13.5 | 6.2 | 20.3 | 9.5 | 31.2 | 14.5 | 47.6 | U/L listed |
| 58 | 53.5 | 28.5 | 92.5 | 0.206 | 5.23 | 4.9 | 16.1 | 6.6 | 21.7 | 9.2 | 30.2 | 13.4 | 44.2 | double shield |
| 58A | 50 | 30.8 | 101.1 | 0.195 | 4.95 | 5.3 | 17.4 | 8.2 | 26.9 | 12.6 | 41.3 | 20.0 | 65.6 | test leads |
| 58A | 50 | 30.8 | 101.1 | 0.195 | 4.95 | 4.8 | 15.8 | 6.9 | 22.6 | 10.1 | 33.1 | 15.5 | 50.9 | double shield |
| 58 C | 50 | 30.8 | 101.1 | 0.195 | 4.95 | 5.3 | 17.4 | 8.2 | 26.9 | 12.6 | 41.3 | 20.0 | 65.6 | mil. spec. |
| 59 | 73 | 21.0 | 68.9 | 0.242 | 6.15 | 3.4 | 11.2 | 4.9 | 16.1 | 7.1 | 23.3 | - | - | gen. purpose, TV |
| 59B | 75 | 20.5 | 67.3 | 0.242 | 6.15 | 3.4 | 11.2 | 4.9 | 16.1 | 7.1 | 23.3 | 11.1 | 36.4 | mil. spec. |
| 62 | 93 | 13.5 | 44.3 | 0.242 | 6.15 | 3.1 | 10.2 | 4.4 | 14.4 | 6.3 | 20.7 | 11.0 | 36.1 | low capacity, small |
| 62A | 93 | 13.5 | 44.3 | 0.242 | 6.15 | 3.1 | 10.2 | 4.4 | 14.4 | 6.3 | 20.7 | 11.0 | 36.1 | mil. spec. |
| 62A | 93 | 14.5 | 47.6 | 0.260 | 6.60 | 3.1 | 10.2 | 4.4 | 14.4 | 6.3 | 20.7 | 11.0 | 36.1 | U/L listed |
| 62B | 93 | 13.5 | 44.3 | 0.242 | 6.15 | 3.1 | 10.2 | 4.4 | 14.4 | 6.3 | 20.7 | 11.0 | 36.1 | transmission |
| 63 B | 125 | 10.0 | 33.1 | 0.415 | 10.54 | 2.0 | 6.6 | 2.9 | 9.5 | 4.1 | 13.5 | - | - | low capacitance |
| 71 B | 93 | 13.5 | 44.3 | 0.250 | 6.28 | 2.7 | 8.9 | 3.9 | 12.7 | 5.8 | 18.9 | - | - | transmission |
| 122 | 50 | 30.8 | 101.1 | 0.160 | 4.06 | 7.0 | 23.0 | 11.0 | 36.1 | $\begin{aligned} & 16.5 \\ & \max \end{aligned}$ | 54.1 | 28.0 | 91.9 | - |
| 141A | 50 | 29.0 | 95.1 | 0.190 | 4.83 | - | - | - | - | $\begin{array}{r} 9.0 \\ \max \end{array}$ | 29.5 | - | - | Teflon, Fiberglas |
| 142B | 50 | 29.0 | 95.1 | 0.195 | 4.95 | - | - | - | - | 9.0 | 29.5 | - | - | Teflon, 2 shield |
| 174 | 50 | 30.8 | 101.1 | 0.100 | 2.54 | 8.8 | 28.9 | 13.0 | 42.7 | $\begin{aligned} & 20.0 \\ & \max \end{aligned}$ | 65.6 | - | - | miniature |
| 178B | 50 | 29.0 | 95.1 | 0.070 | 1.78 | - | - | - | - | $\begin{aligned} & 29.0 \\ & \max \end{aligned}$ | 95.1 | - | - | Teflon, trans. |
| 179B | 75 | 19.5 | 64.0 | 0.100 | 2.54 | - | - | - | - | $\begin{aligned} & 21.0 \\ & \max \end{aligned}$ | 68.9 | - | - | Teflon, trans. |
| 180B | 95 | 15.0 | 49.21 | 0.140 | 3.56 | - | - | - | - | 17.0 | 55.8 | - | - | Teflon, trans. |
| 187A | 75 | 19.5 | 64.0 | 0.110 | 2.81 | - | - | - | - | $\begin{aligned} & 21.0 \\ & \max \end{aligned}$ | $68.9$ $\max$ | - | - | Teflon, trans., miniature |
| 188A | 50 | 27.5 | 88.5 | 0.110 | 2.81 | - | - | - | - | $\begin{aligned} & 20.0 \\ & \max \end{aligned}$ | 65.6 max | - | - | Teflon, trans., miniature |
| 195A | 95 | 14.5 | 57.6 | 0.155 | 3.96 | - | - | - | - | 17.0 max | 55.8 max | - | - | pulse, low cap. |
| 196A | 50 | 28.5 | 92.4 | 0.080 | 2.03 | - | - | - | - | 29.0 | 95.1 | - | - | Teflon, miniature |
| 212 | 50 | 29.5 | 95.7 | 0.336 | 7.53 | 2.4 | 7.9 | 3.6 | 11.9 | 5.2 | 17.0 | - | - | double braid |
| 213 | 50 | 30.8 | 101.1 | 0.405 | 10.29 | 2.0 | 6.6 | 3.0 | 9.8 | 4.7 | 15.4 | 7.8 | 25.6 | gen. purpose |
| 214 | 50 | 30.8 | 101.1 | 0.425 | 10.80 | 2.0 | 6.6 | 3.0 | 9.8 | 4.7 | 15.4 | 7.8 | 25.6 | gen. purpose |
| 215 | 50 | 30.5 | 99.4 | 0.412 | 10.46 | 2.1 | 6.9 | 3.1 | 10.2 | 5.0 | 16.5 | - | - | gen. purpose |
| 217 | 50 | 30.0 | 97.3 | 0.555 | 14.14 | 1.5 | 4.8 | 2.3 | 7.8 | 3.5 | 11.5 | - | - | double braid |
| 218 | 50 | 30.0 | 97.3 | 0.880 | 22.45 | 0.95 | 3.1 | 1.5 | 4.8 | 2.4 | 7.9 | - | - | low attenuation |
| 219 | 50 | 30.0 | 97.3 | 0.880 | 22.45 | 0.95 | 3.1 | 1.5 | 4.8 | 2.4 | 7.9 | - | - | low attenuation/ armor |
| 223 | 50 | 30.0 | 97.3 | 0.216 | 5.30 | 4.8 | 15.8 | 7.0 | 23.1 | $\begin{aligned} & 10.5 \\ & \max \end{aligned}$ | $34.4$ $\max$ | - | - | double braid, miniature |
| 316 | 50 | 29.0 | 95.2 | 0.098 | 2.49 | - | - | - | - | $\begin{aligned} & 20.0 \\ & \max \end{aligned}$ | 65.6 max | - | - | Teflon, mil. spec. |



Fig. 4-1

A horizontal wedge (D) in the test pattern is used to indicate the vertical resolution and interlace of the receiver. Generally these wedges have numbers. Various breaks in the lines indicate the number of lines the receiver is capable of producing.

There are one or two diagonal wedges ( F ) that indicate the contrast ratio. Therefore, they can be used to check the adjustments of the contrast, brightness, and automatic gain controls, as well as the video-amplifying and picture-tube circuits. When video-amplifying and picture-tube circuits are operating properly and the con-
trols are properly adjusted, four degrees of shading should be observed, ranging from black at the center to light gray at the outermost point on the wedge.

The horizontal bars (H) are used to check for low-frequency phase shift. Highfrequency ringing can be checked using the single resolution lines (I).

Another test pattern is the color bar pattern shown in Fig. 4-2. The color pattern consists of red to yellow to green, then to blue, and is used for a station check of the color transmitter. It is also used for "receiver color setup."


Fig. 4-2
The test pattern of Fig. 4-3 is a hybrid in which the test pattern is a set of color bars of different widths. The test pattern is also a part of the information for overall setup of the station transmitter or of the color receiver.


Fig. 4-3
MINIATURE LAMP DATA
Table 4-2 lists the most common miniature lamps and their characteristics. The outline drawings for each lamp are shown in Fig. 4-4.

TABLE 4-2
Miniature Lamp Data

| Lamp no. | Volts | Amps | Bead color | Base | Bulb type | Outline fig. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PR2 | 2.4 | 0.50 | blue | flange | B-31/2 | A |
| PR3 | 3.6 | 0.50 | green | flange | 13-31/2 | A |
| PR4 | 2.3 | 0.27 | yellow | flange | B-31/2 | A |
| PR6 | 2.5 | 0.30 | brown | flange | B-31/2 | A |
| PR7 | 3.8 | 0.30 |  | flange | B-31/2 | A |
| PR12 | 5.95 | 0.50 | white | flange | B-31/2 | A |
| PR13 | 4.75 | 0.50 |  | flange | B-31/2 | A |
| PR18 | 7.2 | 0.55 |  | flange | B-31/2 | A |
| PR20 | 8.63 | 0.50 |  | flange | B-31/2 | A |
| 12 | 6.3 | 0.15 |  | 2-pin | G-31/2 | H |
| 13 | 3.8 | 0.30 | green | screw | Ci-31/2 | B |
| 14 | 2.5 | 0.30 | blue | screw | G-31/2 | B |
| 19 | 14.4 | 0.10 |  | 2-pin | G-31/2 | H |
| 27 | 4.9 | 0.30 |  | bayonet | G-4 ${ }^{1 / 2}$ | F |
| 31 | 6.15 | 0.30 |  | bayonet | G-41/2 | F |
| 41 | 2.5 | 0.50 | white | screw | T-31/4 | C |
| 43 | 2.5 | 0.50 | white | bayonet | T-31/4 | D |
| 44 | 6.3 | 0.25 | blue | bayonet | T-31/4 | D |
| 45 | 3.2 | $0.35 \dagger$ | green $\dagger$ | bayonet | T-31/4 | D |
| 46 | 6.3 | 0.25 | blue | screw | T-31/4* | C |
| 47 | 6.3 | 0.15 | brown | bayonet | T-31/4 | D |
| 48 | 2.0 | 0.06 | pink | screw | T-31/4 | C |

# Service and Installation Data 

TABLE 4-2 Cont.
Miniature Lamp Data

| Lamp no. | Volts | Amps | Bead color | Base | Bulb type | Outline fig. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 49 | 2.0 | 0.06 | pink | bayonet | T-31/4 | D |
| 50 | 6.3 | 0.20 | white | screw | G-31/2 | B |
| 51 | 6.3 | 0.20 | white | bayonet | G-31/2 | E |
| 53 | 14.4 | 0.12 |  | bayonet | G-31/2 | E |
| 55 | 6.3 | 0.40 | white | bayonet | G-41/2 | G |
| 57 | 14.0 | 0.24 | white | bayonet | C-41/2 | G |
| 63 | 7.0 | 0.63 |  | bayonet | G-5 | P |
| 67 | 13.5 | 0.59 |  | bayonet | G-6 | P |
| 81 | 6.5 | 1.02 |  | bayonet | G-5 | P |
| 82 | 6.5 | 1.02 |  | bayonet | G-5 | 1 |
| 87 | 6.8 | 1.91 |  | bayonet | S-8 | K |
| 88 | 6.8 | 1.91 |  | bayonet | S-8 | Q |
| 89 | 13.0 | 0.58 |  | bayonet | G-5 | P |
| 93 | 12.8 | 1.04 |  | bayonet | S-8 | K |
| 112 | 1.2 | 0.22 |  | screw | TL-3 | DD |
| 123 | 1.25 | 0.30 |  | screw | G-31/2 | B |
| 136 | 1.25 | 0.60 |  | bayonet | G-41/2 | F |
| 158 | 14.0 | 0.24 |  | wedge | T-31/4 | S |
| 161 | 14.0 | 0.19 |  | wedge | T-31/4 | S |
| 168 | 14.0 | 0.35 |  | wedge | T-31/4 | S |
| 194 | 14.0 | 0.27 |  | wedge | T-31/4 | S |
| 222 | 2.2 | 0.25 | white | screw | TL-3 | DD |
| 301 | 28.0 | 0.17 |  | bayonet | G-5 | R |
| 302 | 28.0 | 0.17 |  | bayonet | G-5 | T |
| 303 | 28.0 | 0.30 |  | bayonet | G-6 | P |
| 305 | 28.0 | 0.51 |  | bayonet | S-8 | K |
| 307 | 28.0 | 0.67 |  | bayonet | S-8 | K |
| 308 | 28.0 | 0.67 |  | bayonet | S-8 | Q |
| 309 | 28.0 | 0.90 |  | bayonet | S-11 | U |
| 313 | 28.0 | 0.17 |  | bayonet | T-31/4 | D |
| 327 | 28.0 | 0.04 |  | flanged | T-13/4 | W |
| 328 | 6.0 | 0.20 |  | flanged | T-13/4 | W |
| 330 | 14.0 | 0.08 |  | flanged | T-13/4 | W |
| 331 | 1.35 | 0.06 |  | flanged | T-13/4 | W |
| 334 | 28.0 | 0.04 |  | grooved | T-13/4 | X |
| 344 | 10.0 | 0.014 |  | flanged | T-13/4 | W |
| 382 | 14.0 | 0.08 |  | flanged | T-13/4 | W |
| 387 | 28.0 | 0.04 |  | flanged | T-13/4 | W |
| 388 | 28.0 | 0.04 |  | grooved | T-13/4 | X |
| 680 | 5.0 | 0.060 |  | wire terminal | T-1 | M |
| 682 | 5.0 | 0.060 |  | wire terminal | T-1 | Y |
| 683 | 5.0 | 0.060 |  | wire terminal | T-1 | M |
| 685 | 5.0 | 0.060 |  | wire terminal | T-1 | Y |
| 713 | 5.0 | 0.075 |  | wire terminal | T-1 | M |
| 714 | 5.0 | 0.075 |  | wire terminal | T-1 | Y |
| 715 | 5.0 | 0.115 |  | wire terminal | T-1 | M |
| 718 | 5.0 | 0.115 |  | wire terminal | T-1 | Y |
| 1003 | 12.8 | 0.94 |  | bayonet | B-6 | AA |
| 1004 | 12.8 | 0.94 |  | bayonet | B-6 | BB |
| 1034 | 12.8 | 1.80 |  | bayonet | S-8 | Q |
| 1076 | 12.8 | 1.80 |  | bayonet | S-8 | Q |
| 1133 | 6.2 | 3.91 |  | bayonet | RP-11 | CC |

TABLE 4-2 Cont.
Miniature Lamp Data

| Lamp no. | Volts | Amps | Bead color | Base | Bulb type | Outine fig. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1156 | 12.8 | 2.10 |  | bayonet | S-8 | K |
| 1157 | 12.8 | 2.10 |  | bayonet | S-8 | Q |
| 1176 | 12.8 | 1.34 |  | bayonet | S-8 | Q |
| 1183 | 5.5 | 6.25 |  | bayonet | RP-11 | CC |
| 1195 | 12.5 | 3.0 |  | bayonct | RP-11 | CC |
| 1445 | 14.4 | 0.135 |  | bayonet | C-31/2 | E |
| 1447 | 18.0 | 0.15 |  | screw | G-31/2 | B |
| 1490 | 3.2 | 0.16 | white | bayonct | T-31/4 | D |
| 1495 | 28.0 | 0.30 |  | bayonet | T-41/2 | Z |
| 1728 | 1.35 | 0.06 |  | wire terminal | T-13/4 | N |
| 1738 | 2.7 | 0.06 |  | wire terminal | T-13/4 | N |
| 1764 | 28.0 | 0.04 |  | wire terminal | T-13/4 | N |
| 1784 | 6.0 | 0.20 |  | wire terminal | T-13/4 | N |
| 1813 | 14.4 | 0.10 |  | bayonet | T-31/4 | D |
| 1815 | 14.0 | 0.20 |  | bayonet | T-31/4 | D |
| 1816 | 13.0 | 0.33 |  | bayonet | T-31/4 | D |
| 1819 | 28.0 | 0.40 | white | bayonet | T-31/4 | D |
| 1820 | 28.0 | 0.10 |  | bayonet | T-31/4 | D |
| 1829 | 28.0 | 0.07 |  | bayonet | T-31/4 | D |
| 1847 | 6.3 | 0.15 | white | bayonct | T-31/4 | D |
| 1850 | 5.0 | 0.09 |  | bayonet | T-31/4 | D |
| 1864 | 28.0 | 0.17 |  | bayonet | T-31/4 | D |
| 1866 | 6.3 | 0.25 |  | bayonet | T-31/4 | D |
| 1869 | 10.0 | 0.014 |  | wire terminal | T-13/4 | N |
| 1888 | 6.3 | 0.46 | white | bayonet | T-31/4 | D |
| 1889 | 14.0 | 0.27 |  | bayonet | T-31/4 | D |
| 1891 | 14.0 | 0.24 | pink | bayonet | T-31/4 | D |
| 1893 | 14.0 | 0.33 |  | bayonet | T-31/4 | D |
| 1895 | 14.0 | 0.27 |  | bayonet | Ci-41/2 | F |
| 2162 | 14.0 | 0.10 |  | wire terminal | T-13/4 | N |
| 2182 | 14.0 | 0.08 |  | wire terminal | T-13/4 | N |
| 2187 | 28.0 | 0.04 |  | wire terminal | T-13/4 | N |
| 6832 | 5.0 | 0.06 |  | wire terminal | T-1 $\ddagger$ | 0 |
| 6833 | 5.0 | 0.06 |  | wire terminal | T-3/4 | O |
| 6838 | 28.0 | 0.24 |  | wire terminal | T-1 | M |
| 6839 | 28.0 | 0.24 |  | wire terminal | T-1 | Y |
| 7152 | 5.0 | 0.115 |  | wire terminal | T-1 $\ddagger$ | I. |
| 7327 | 28.0 | 0.04 |  | wire terminal | T-13/4 | V |
| 7328 | 6.0 | 0.20 |  | wire terminal | T-13/4 | V |
| 7344 | 10.0 | 0.014 |  | wire terminal | T-13/4 | V |
| 7382 | 14.0 | 0.08 |  | wire terminal | T-13/4 | V |
| 7387 | 28.0 | 0.04 |  | wire terminal | T-13/4 | V |
| 7931 | 1.35 | 0.06 |  | wire terminal | T-13/4 | V |

*Frosted.
$\dagger$ Some brands are 0.5 A and whice bead.
$\ddagger$ Short.

Service and Installation Data


Fig. 4-4

## GAS-FILLED LAMP DATA

The characteristics of the more common gas-filled lamps are given in Table 4-3. The
value of external resistance needed for operation with circuit voltages from 110 to 600 V is given in Table 4-4.

TABLE 4-3
Gas-Filled Lamp Data

| Number | Average life (h)* | Type <br> gas | Maximum length (in) | Type of base | Amps | Volts | Watts $\dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AR-1 | 3000 | argon | 3.50 | medium screw | 0.018 | 105-125 | 2 |
| AR-3 | 1000 | argon | 1.625 | candelabra screw | 0.0035 | 105-125 | 0.25 |
| AR-4 | 1000 | argon | 1.50 | double-contact bayonet | 0.0035 | 105-125 | 0.25 |
| NE-2 | over 25,000 | neon | $1.063 \ddagger$ | 1 -in wire terminal | 0.003 | 105-125 | 0.04 |
| - $\mathrm{E}-2 \mathrm{~A}$ | over 25,000 | neon | $0.844 \ddagger$ | 2 -in wire terminal | 0.003 | 105-125 | 0.04 |
| NI:-2D | 25,000 | neon | 0.938 | S. C. mid: flanged | 0.007 | 105-125 | 0.08 |
| NE-2E | 25,000 | neon | 0.750 | 2 -in wire terminal | 0.007 | 105-125 | 0.08 |
| NE-2H | 25,000 | neon | 0.750 | 2 -in wire terminal | 0.0019 | 105-125 | $0.25 \mathrm{H}-\mathrm{B}$ |
| NE-2.J | 25,000 | neon | 0.938 | S. C. mid. flanged | 0.0019 | 105-125 | $0.25 \mathrm{H}-\mathrm{B}$ |
| NE-2V | 25,000 | neon | 1.063 | 2 -in wire terminal | 0.0065 | 105-125 | 0.7 |
| NE-2AS | 25,000 | neon | 1.063 | 2 -in wire terminal | 0.0003 | 60-90 | 0.03 |
| NE-3 | over 5000 | neon | 0.875 | telephone slide | 0.0003 | 55-90 | 0.03 |
| NE:-4 | over 5000 | neon | 0.875 | tclephone slide | 0.0003 | 60-90 | 0.03 |
| NE-16 | 1000 | neon | 1.50 | double-contact bayonet | 0.0015 | 53-65 | 0.1 |
| NE-17 | 5000 | neon | 1.50 | double-contact bayonet | 0.002 | 105-125 | 0.25 |
| NE-23 | 6000 | neon | 1.00 | 1 -in wire terminal | 0.0003 | 60-90 | 0.03 |
| NE-30 | 10,000 | neon | 2.250 | medium screw | 0.012 | 105-125 | 1 |
| NE-32 | 10,000 | neon | 2.125 | double-contact bayonet§ | 0.012 | 105-125 | 1 |
| NE-45 | over 7500 | neon | 1.625 | candelabra screw | 0.002 | 105-125 | 0.25 |
| NE-47 | 5000 | neon | 1.375 | single-contact bayonct | 0.002 | 105-125 | 0.25 |
| NE-48 | over 7500 | neon | 1.50 | double-contact bayonet | 0.002 | 105-125 | 0.25 |
| NE-51 | over 15,000 | neon | 1.188 | miniature bayonet | 0.0003 | 105-125 | 0.04 |
| NE-51H | 25,000 | neon | 1.188 | miniature bayonet | 0.0012 | 105-125 | 1 |
| NE-51S | 25,000 | neon | 1.188 | miniature bayonet | 0.0002 | 55-90 | 0.02 |
| NE-56 | 10,000 | neon | 2.250 | medium screw§ | 0.005 | 210-250 | 0.5 |
| NE-57 | 5000 | neon | 1.625 | candelabra screw§ | 0.002 | 105-125 | 0.25 |
| NE:-58 | over 7500) | neon | 1.625 | candelabra screw | 0.002 | 105-125 | 0.50 |
| NE-67 | 25,000 | neon | 1.188 | miniature bayonet | 0.0002 | 55-90 | 0.02 |
| NE:-68 | 5000 | neon | 1.063 | 2 -in wire terminal | 0.0003 | 52-65 | 0.02 |
| NE-75 | 2000 | neon | 1.063 | 1 -in wire terminal | 0.0004 | 60-90 | 0.04 |
| NE-76 | 2000 | neon | 1.063 | 1-in wire terminal | 0.0004 | 68-76 | 0.03 |
| NE-81 | 5000 | neon | 1.063 | 1-in wire terminal | 0.0003 | 64-80 | 0.0024 |
| NE-83 | 5000 | neon | 1.063 | 1 -in wire terminal | 0.005 | 60-100 | 0.5 |
| NE-86 | 5000 | neon | 1.063 | 1 -in wire terminal | 0.0015 | 55-90 | 0.14 |
| NE-96 | 6000 | neon | 1.063 | 1-in wire terminal | 0.0005 | 60-80 | 0.04 |
| NE-97 | 6000 | neon | 1.00 | 1-in wire terminal | 0.0005 | 60-80 | 0.04 |

*I ife on DC is approximately $60 \%$ of AC values.
†For 105- to $125-\mathrm{V}$ operation.
$\ddagger$ The dimension is for glass only.
§In DC circuits, the base should be negative.

TABILE 4-4
External Resistances Needed for Gas-Filled Lamps

| Type | $\mathbf{1 0 5 - 1 2 5} \mathbf{V}$ | $\mathbf{2 2 0 - 3 0 0} \mathbf{V}$ | $\mathbf{3 0 0 - 3 7 5} \mathbf{V}$ | $\mathbf{3 7 5 - 4 5 0} \mathbf{V}$ | $\mathbf{4 5 0 - 6 0 0} \mathbf{V}$ |
| :---: | :---: | ---: | ---: | ---: | ---: |
| AR-1 | included in base | 10,000 | 18,000 | 24,000 | 30,000 |
| AR-3 | included in base | 68,000 | 90,000 | 150,000 | 160,000 |
| AR-4 | 15,000 | 82,000 | 100,000 | 160,000 | 180,000 |
| NE-2 | 200,000 | 750,000 | $1,000,000$ | $1,200,000$ | $1,600,000$ |
| NE-2A | 200,000 | 750,000 | $1,000,000$ | $1,200,000$ | $1,600,000$ |
| NE-2D | 100,000 | - | - | - | - |
| NE-2E | 100,000 | - | - | - | - |
| NE-2H | 30,000 | - | - | - | - |
| NE-2H | 30,000 | - | - | - | - |
| NE-2V | 100,000 | 30,000 | 110,000 | 150,000 | 180,000 |
| NE-17 | included in base | 10,000 | 20,000 | 24,000 | 240,000 |
| NE-30 | 7,500 | 18,000 | 27,000 | 33,000 | 43,000 |
| NE-32 | included in base | 82,000 | 120,000 | 150,000 | 200,000 |
| NE-45 | 30,000 | - | - | - | - |
| NE-47 | 30,000 | - | - | - | - |
| NE-48 | 200,000 | 750,000 | $1,000,000$ | $1,200,000$ | $1,600,000$ |
| NE-51 | - | - | - | - |  |
| NE-51H | included in base | - | - | - | - |
| NE-56 | included in base | 82,000 | 120,000 | 150,000 | 200,000 |
| NE-57 | - | - | - | - |  |
| NE-58 | included in base |  |  | - | - |

## RECEIVER AUDIOPOWER AND FREQUENCY RESPONSE CHECK

Normally the first receiver check performed is the audiopower check. This determines whether the receiver is dead. If not, it will show whether it can deliver appropriate audiopower. If it is found that audiopower output is as specified, then the frequency re-
sponse can be quickly and easily checked by comparing the audio output power at 400 and 2500 Hz to a $1000-\mathrm{Hz}$ reference. This check shows the overall ability of the receiver to pass all audiosignals in the voice communications range (Fig. 2-11). Figures $4-5$ and $4-6$ provide conversion charts of audiovoltage to audiopower for $0.1-1.0 \mathrm{~W}$ and $1.0-10 \mathrm{~W}$, respectively.


Fig. 4-5


Fig. 4-6

## SPEAKER CONNECTIONS

Figures $4-7$ through $4-10$ show the proper connection methods for single- or multiple-speaker operation.


Fig. 4-7. Single speaker.


Fig. 4-8. Two speakers in series.

## MACHINE SCREW AND DRILL SIZES

The decimal equivalents of No. 80 to 1 in drills are in Table 4-5.



Fig. 4-9. 70.7-V hook-up using matching transformers.

The most common screw sizes and threads, together with the tap and clearance drill sizes, are given in Table 4-6. The number listed under the "Type" column is actually a combination of the screw size and the number of threads per inch. For example, a No. 6-32 screw denotes a size no. 6 screw with 32 threads per inch.


Fig. 4-10. Speakers in parallel.

TABLE 4-5
Drill Sizes and Decimal Equivalents

| Drill size | Decimal | Drill size | Decimal | Drill size | Decimal | Drill size | Decimal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 80 | 0.0135 | 42 | 0.0935 | 7 | 0.2010 | X | 0.3970 |
| 79 | 0.0145 | 3/22 | 0.0938 | 13/64 | 0.2031 | Y | 0.4040 |
| 1/64 | 0.0156 | 41 | 0.0960 | 6 | 0.2040 | 13/32 | 0.4062 |
| 78 | 0.0160 | 40 | 0.0980 | 5 | 0.2055 | Z | 0.4130 |
| 77 | 0.0180 | 39 | 0.0995 | 4 | 0.2090 | 27/64 | 0.4219 |
| 76 | 0.0200 | 38 | 0.1015 | 3 | 0.2130 | 7/16 | 0.4375 |
| 75 | 0.0210 | 37 | 0.1040 | 7/32 | 0.2188 | 29/64 | 0.4531 |
| 74 | 0.0225 | 36 | 0.1065 | 2 | 0.2210 | 15/32 | 0.4688 |
| 73 | 0.0240 | 7/64 | 0.1094 | 1 | 0.2280 | 31/64 | 0.4844 |
| 72 | 0.0250 | 35 | 0.1100 | A | 0.2340 | 1/2 | 0.5000 |
| 71 | 0.0260 | 34 | 0.1110 | 15/64 | 0.2344 | 33/64 | 0.5156 |
| 70 | 0.0280 | 33 | 0.1130 | B | 0.2380 | 17/32 | 0.5313 |
| 69 | 0.0292 | 32 | 0.1160 | C | 0.2420 | 35/64 | 0.5469 |
| 68 | 0.0310 | 31 | 0.1200 | D | 0.2460 | $9 / 16$ | 0.5625 |
| 1/32 | 0.0313 | 1/8 | 0.1250 | 1/4 | 0.2500 | 37/64 | 0.5781 |
| 67 | 0.0320 | 30 | 0.1285 | F | 0.2570 | 19/32 | 0.5938 |
| 66 | 0.0330 | 29 | 0.1360 | G | 0.2610 | 39/64 | 0.6094 |
| 65 | 0.0350 | 28 | 0.1405 | 17/64 | 0.2656 | $5 / 8$ | 0.6250 |
| 64 | 0.0360 | 9/64 | 0.1406 | H | 0.2660 | 41/64 | 0.6406 |
| 63 | 0.0370 | 27 | 0.1440 | I | 0.2720 | 21/32 | 0.6562 |
| 62 | 0.0380 | 26 | 0.1470 | J | 0.2770 | $43 / 64$ | 0.6719 |
| 61 | 0.0390 | 25 | 0.1495 | K | 0.2810 | 11/16 | 0.6875 |
| 60 | 0.0400 | 24 | 0.1520 | 9/32 | 0.2812 | $45 / 64$ | 0.7031 |
| 59 | 0.0410 | 23 | 0.1540 | I. | 0.2900 | $23 / 32$ | 0.7188 |
| 58 | 0.0420 | 5/32 | 0.1562 | M | 0.2950 | $47 / 64$ | 0.7344 |
| 57 | 0.0430 | 22 | 0.1570 | 19/64 | 0.2969 | $3 / 4$ | 0.7500 |
| 56 | 0.0465 | 21 | 0.1590 | N | 0.3020 | 49/64 | 0.7656 |
| 3/64 | 0.0469 | 20 | 0.1610 | $5 / 16$ | 0.3125 | 25/32 | 0.7812 |
| 55 | 0.0520 | 19 | 0.1660 | O | 0.3160 | $51 / 64$ | 0.7969 |
| 54 | 0.0550 | 18 | 0.1695 | P | 0.3230 | 13/16 | 0.8125 |
| 53 | 0.0595 | 11/64 | 0.1709 | 21/64 | 0.3281 | 53/64 | 0.8281 |
| 1/16 | 0.0625 | 17 | 0.1730 | Q | 0.3320 | 27/32 | 0.8438 |
| 52 | 0.0635 | 16 | 0.1770 | R | 0.3390 | $55 / 64$ | 0.8594 |
| 51 | 0.0670 | 15 | 0.1800 | $11 / 32$ | 0.3438 | 7/8 | 0.8750 |
| 50 | 0.0700 | 14 | 0.1820 | S | 0.3480 | $57 / 64$ | 0.8906 |
| 49 | 0.0730 | 13 | 0.1850 | T | 0.3580 | 29/32 | 0.9062 |
| 48 | 0.0760 | 3/16 | 0.1875 | 23/64 | 0.3594 | 59/64 | 0.9219 |
| 5/64 | 0.0781 | 12 | 0.1890 | U | 0.3680 | 15/16 | 0.9375 |
| 47 | 0.0785 | 11 | 0.1910 | $3 / 8$ | 0.3750 | 61/64 | 0.9531 |
| 46 | 0.0810 | 10 | 0.1935 | V | 0.3770 | $31 / 32$ | 0.9688 |
| 45 | 0.0820 | 9 | 0.1960 | W | 0.3860 | 63/64 | 0.9844 |
| 44 | 0.0860 | 8 | 0.1990 | 25/64 | 0.3906 | 1 | 1.000 |
| 43 | 0.0890 |  |  |  |  |  |  |

## TYPES OF SCREW HEADS

The most common types of screw heads are listed and illustrated in Fig. 4-11.

TABLE 4-6
Machine Screw Tap and Clearance Drill Sizes.

| Type | Tap drill | Clearance drill |
| :---: | :---: | :---: |
| 0-80 | 3/6+ | 50 |
| 1-64 | 53 | 47 |
| 1-72 | 53 | 47 |
| 2-56 | 50 | 42 |
| 2-64 | 50 | 42 |
| 3-48 | 47 | 36 |
| 3-56 | 45 | 36 |
| 4-40 | 43 | 31 |
| 4-48 | 42 | 31 |
| 5-40 | 38 | 29 |
| 5-44 | 37 | 29 |
| 6-32 | 36 | 25 |
| 6-40 | 33 | 25 |
| 8-32 | 29 | 16 |
| 8-36 | 29 | 16 |
| 10-24 | 25 | 13/64 |
| 10-32 | 21 | $13 / 64$ |
| 12-24 | 16 | $7 / 32$ |
| 12-28 | 14 | 7/32 |
| $1 / 4-20$ | 7 | 17/64 |
| 1/4-28 | 3 | 17/6+ |
| $5 / 16-18$ | F | 21/64 |
| $5 / 16-24$ | , | 21/64 |
| $3 / 8$-16 | $5 / 16$ | 25/6+ |
| $3 / 8-24$ | Q | 25/64 |
| 7/16-14 | U | 29/64 |
| 7/16-20 | 25/64 | 29/64 |
| 1/2-12 | 27/64 | 33/64 |
| $1 / 2-13$ | 27/64 | $33 / 64$ |
| $1 / 2-20$ | 29/6+ | 33/64 |



Fig. 4-11

Materials are customarily made to certain gage systems. While materials can usually be had specially in any system, some usual practices are shown in Tables 4-7 and 4-8.

TABLE 4-7
Common Gage Practices

| Material | Sheet | Wire |
| :--- | :---: | :---: |
| aluminum <br> brass, bronze, shect <br> copper <br> iron, steel, band, and <br> hoop <br> iron, steel, telephone, and <br> telegraph wire | B\&S | AWG (B\&S) |
| steel wire, except <br> telephone and telegraph | B\&S | AWG (B\&S) |
| steel sheet <br> tank steel <br> zinc sheet | - | - |

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TABLE 4-8
Comparison of Gages

| Gage | AWG <br> (B\&S) | Birmingham or Stubs (BWG) | Wash. \& Moen ( $\mathbf{W} \boldsymbol{\&} \mathbf{M}$ ) | British Standard (NBS SWC) | London or Old English | United <br> States Standard (US) | American Standard preferred thickness* |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0000000 | - | - | 0.490 | 0.500 | - | 0.50000 | - |
| 000000 | 0.5800 | - | 0.460 | 0.464 | - | 0.46875 | - |
| 00000 | 0.5165 | - | 0.430 | 0.432 | - | 0.43750 | - |
| 0000 | 0.4600 | 0.454 | 0.3938 | 0.400 | 0.454 | 0.40625 | - |
| 000 | 0.4096 | 0.425 | 0.3625 | 0.372 | 0.425 | 0.37500 | - |
| 00 | 0.3648 | 0.380 | 0.3310 | 0.348 | 0.380 | 0.34375 | - |
| 0 | 0.3249 | 0.340 | 0.3065 | 0.324 | 0.340 | 0.31250 | - |
| 1 | 0.2893 | 0.300 | 0.2830 | 0.300 | 0.300 | 0.2815 | - |
| 2 | 0.2576 | 0.284 | 0.2625 | 0.276 | 0.284 | 0.265625 | - |
| 3 | 0.2294 | 0.259 | 0.2437 | 0.252 | 0.259 | 0.250000 | 0.224 |
| 4 | 0.2043 | 0.238 | 0.2253 | 0.232 | 0.238 | 0.234375 | 0.200 |
| 5 | 0.1819 | 0.220 | 0.2070 | 0.212 | 0.220 | 0.218750 | 0.180 |
| 6 | 0.1620 | 0.203 | 0.1920 | 0.192 | 0.203 | 0.203125 | 0.160 |
| 7 | 0.1443 | 0.180 | 0.1770 | 0.176 | 0.180 | 0.187500 | 0.140 |
| 8 | 0.1285 | 0.165 | 0.1620 | 0.160 | 0.165 | 0.171875 | 0.125 |
| 9 | 0.1144 | 0.148 | 0.1483 | 0.144 | 0.148 | 0.156250 | 0.112 |
| 10 | 0.1019 | 0.134 | 0.1350 | 0.128 | 0.134 | 0.140625 | 0.100 |
| 11 | 0.09074 | 0.120 | 0.1205 | 0.116 | 0.120 | 0.125000 | 0.090 |
| 12 | 0.08081 | 0.109 | 0.1055 | 0.104 | 0.109 | 0. 109375 | 0.080 |
| 13 | 0.07196 | 0.095 | 0.0915 | 0.092 | 0.095 | 0.093750 | 0.071 |
| 14 | 0.06408 | 0.083 | 0.0800 | 0.080 | 0.083 | 0.078125 | 0.063 |
| 15 | 0.05707 | 0.072 | 0.0720 | 0.072 | 0.072 | 0.0703125 | 0.056 |
| 16 | 0.05082 | 0.065 | 0.0625 | 0.064 | 0.065 | 0.0625000 | 0.050 |
| 17 | 0.04526 | 0.058 | 0.0540 | 0.056 | 0.058 | 0.0562500 | 0.045 |
| 18 | 0.04030 | 0.049 | 0.0475 | 0.048 | 0.049 | 0.0500000 | 0.040 |
| 19 | 0.03589 | 0.042 | 0.0410 | 0.040 | 0.040 | 0.0437500 | 0.036 |
| 20 | 0.03196 | 0.035 | 0.0348 | 0.036 | 0.035 | 0.0375000 | 0.032 |
| 21 | 0.02846 | 0.032 | 0.03175 | 0.032 | 0.0315 | 0.0343750 | 0.028 |
| 22 | 0.02535 | 0.028 | 0.02860 | 0.028 | 0.0295 | 0.0312500 | 0.025 |
| 23 | 0.02257 | 0.025 | 0.02580 | 0.024 | 0.0270 | 0.0281250 | 0.022 |
| 24 | 0.02010 | 0.022 | 0.02300 | 0.022 | 0.0250 | 0.0250000 | 0.020 |
| 25 | 0.01790 | 0.020 | 0.02040 | 0.020 | 0.0230 | 0.0218750 | 0.018 |
| 26 | 0.01594 | 0.018 | 0.01810 | 0.018 | 0.0205 | 0.0187500 | 0.016 |
| 27 | 0.01420 | 0.016 | 0.01730 | 0.0164 | 0.0187 | 0.0171875 | 0.014 |
| 28 | 0.01264 | 0.014 | 0.01620 | 0.0148 | 0.0165 | 0.0156250 | 0.012 |
| 29 | 0.01126 | 0.013 | 0.01500 | 0.0136 | 0.0155 | 0.0140625 | 0.011 |
| 30 | 0.01003 | 0.012 | 0.01400 | 0.0124 | 0.01372 | 0.0125000 | 0.010 |
| 31 | 0.008928 | 0.010 | 0.01320 | 0.0116 | 0.01220 | 0.01093750 | 0.009 |
| 32 | 0.007950 | 0.009 | 0.01280 | 0.0108 | 0.01120 | 0.01015625 | 0.008 |
| 33 | 0.007080 | 0.008 | 0.01180 | 0.0100 | 0.01020 | 0.00937500 | 0.007 |
| 34 | 0.006305 | 0.007 | 0.01040 | 0.0092 | 0.00950 | 0.00859375 | 0.006 |
| 35 | 0.005615 | 0.005 | 0.00950 | 0.0084 | 0.00900 | 0.00781250 | - |
| 36 | 0.005000 | 0.004 | 0.00900 | 0.0076 | 0.00750 | 0.007031250 | - |
| 37 | 0.004453 | - | 0.00850 | 0.0068 | 0.00650 | 0.006640625 | - |
| 38 | 0.003965 | - | 0.00800 | 0.0060 | 0.00570 | 0.006250000 | - |
| 39 | 0.003531 | - | 0.00750 | 0.0052 | 0.00500 | - | - |
| 40 | 0.003145 | - | 0.00700 | 0.0048 | 0.00450 | - | - |

[^5]
## RESISTANCE OF METALS AND ALLOYS

The resistance for a given length of wire is determined by:

$$
R=\frac{K L}{d^{2}}
$$

where
$R$ is the resistance of the length of wire, in ohms,
$K$ is the resistance of the material, in ohms per circular mil foot,
$L$ is the length of the wire, in feet, $d$ is the diameter of the wire, in mils.

The resistance, in ohms per circular mil foot, of many of the materials used for conductors or heating elements is given in Table $4-9$. The resistance shown is for $20^{\circ} \mathrm{C}$ ( $68^{\circ} \mathrm{F}$ ), unless otherwise stated.

## COPPER-WIRE CHARACTERISTICS

Copper-wire sizes ranging from American wire gage (B\&S) 0000 to 60 are listed in Table 4-10. The turns per linear inch, diameter, area in circular mils, current-carrying capacity, feet per pound, and resistance per 1000 ft are included in the table.

TABLE 4-9
Resistance of Metals and Alloys

| Material | Symbol | Resistance <br> ( $\Omega /$ cir mil fout) |
| :--- | :--- | :---: |
| nichrome | $\mathrm{Ni}-\mathrm{Fe}-\mathrm{Cr}$ | 675 |
| tophet A | $\mathrm{Ni}-\mathrm{Cr}$ | 659 |
| nichrome V | $\mathrm{Ni}-\mathrm{Cr}$ | 650 |
| chromax | $\mathrm{Cr}-\mathrm{Ni}-\mathrm{Fe}$ | 610 |
| steel, stainless | $\mathrm{C}-\mathrm{Cr}-\mathrm{Ni}-\mathrm{Fe}$ | 549 |
| chromel | $\mathrm{Ni}-\mathrm{Cr}$ | 427 |
| steel, manganese | $\mathrm{Mn}-\mathrm{C}-\mathrm{Fe}$ | 427 |
| kovar A | $\mathrm{Ni}-\mathrm{Co}-\mathrm{Mn}-\mathrm{Fe}$ | 1732 |
| titanium | Ti | 292 |
| constantan | $\mathrm{Cu}-\mathrm{Ni}$ | 270 |
| manganin | $\mathrm{Cu}-\mathrm{Mn}-\mathrm{Ni}$ | 268 |
| monel | $\mathrm{Ni}-\mathrm{Cu}-\mathrm{Fe}-\mathrm{Mn}$ | 256 |
| arsenic | As | 214 |
| alumel | $\mathrm{Ni}-\mathrm{Al}-\mathrm{Mn}-\mathrm{Si}$ | 203 |
| nickel-silver | $\mathrm{Cu}-\mathrm{Zn}-\mathrm{Ni}$ | 171 |
| lead | Pb | 134 |
| stcel | $\mathrm{C}-\mathrm{Fe}$ | 103 |
| manganese-nickel | $\mathrm{Ni}-\mathrm{Mn}$ | 85 |
| tantalum | Ta | 79.9 |
| tin | Sn | 69.5 |
| palladium | Pd | 65.9 |
| platinum | Pt | 63.8 |
| iron | Fe | 60.14 |
| nickel, pure | Ni | 60 |
| phosphor-bronze | $\mathrm{Sn}-\mathrm{P}-\mathrm{Cu}$ | 57.38 |
| high-brass | $\mathrm{Cu}-\mathrm{Zn}$ | 50 |
| potassium | K | 42.7 |
| molybdenum | Mo | 34.27 |
| tungsten | W | 33.22 |
| rhodium | Rh | 31 |
| aluminum | Al | 16.06 |
| chromium | Cr | 15.87 |
| gold | Au | 14.55 |
| copper | Cu | 10.37 |
| silver | Ag | 9.706 |
| selenium | Se | 7.3 |
|  |  |  |

TABLE 4-10
Copper-Wire Characteristics

| AWG | Nominal bare diameter (in) | Nominal circular mils | Nominal feet per pound (bare) | Nominal ohms per 1000 ft @ $20^{\circ} \mathrm{C}$ | Current- <br> carrying <br> capacity <br> (a) $700 \mathrm{CM} / \mathrm{A}$ | Turns per linear inch |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Single <br> film coated | Heavy film coated |
| 0000 | 0.4600 | 211,600 | 1.561 | 0.04901 | 302.3 |  |  |
| 000 | 0.4096 | 167,800 | 1.969 | 0.06182 | 239.7 |  |  |
| 00 | 0.3648 | 133,100 | 2.482 | 0.07793 | 190.1 |  |  |
| 0 | 0.3249 | 105,600 | 3.130 | 0.09825 | 150.9 |  |  |
| 1 | 0.2893 | 83,690 | 3.947 | 0.1239 | 119.6 |  |  |
| 2 | 0.2576 | 66,360 | 4.978 | 0.1563 | 94.8 |  |  |
| 3 | 0.2294 | 52,620 | 6.278 | 0.1971 | 75.2 |  |  |
| 4 | 0.2043 | 41,740 | 7.915 | 0.2485 | 59.6 |  | 4.80 |
| 5 | 0.1819 | 33,090 | 9.984 | 0.3134 | 47.3 |  | 5.38 |
| 6 | 0.1620 | 26,240 | 12.59 | 0.3952 | 37.5 |  | 6.03 |
| 7 | 0.1443 | 20,820 | 15.87 | 0.4981 | 29.7 |  | 6.75 |
| 8 | 0.1285 | 16,510 | 20.01 | 0.6281 | 23.6 |  | 7.57 |
| 9 | 0.1144 | 13,090 | 25.24 | 0.7925 | 18.7 |  | 8.48 |
| 10 | 0.1019 | 10,380 | 31.82 | 0.9988 | 14.8 |  | 9.50 |
| 11 | 0.0907 | 8230 | 40.2 | 1.26 | 11.8 |  | 10.6 |
| 12 | 0.0808 | 6530 | 50.6 | 1.59 | 9.33 |  | 11.9 |
| 13 | 0.0720 | 5180 | 63.7 | 2.00 | 7.40 |  | 13.3 |
| 14 | 0.0641 | 4110 | 80.4 | 2.52 | 5.87 | 15.2 | 14.8 |
| 15 | 0.0571 | 3260 | 101 | 3.18 | 4.66 | 17.0 | 16.6 |
| 16 | 0.0508 | 2580 | 128 | 4.02 | 3.69 | 19.0 | 18.5 |
| 17 | 0.0453 | 2050 | 161 | 5.05 | 2.93 | 21.3 | 20.7 |
| 18 | 0.0403 | 1620 | 203 | 6.39 | 2.31 | 23.9 | 23.1 |
| 19 | 0.0359 | 1290 | 256 | 8.05 | 1.84 | 26.7 | 25.9 |
| 20 | 0.0320 | 1020 | 323 | 10.1 | 1.46 | 29.9 | 28.9 |
| 21 | 0.0285 | 812 | 407 | 12.8 | 1.16 | 33.4 | 32.3 |
| 22 | 0.0253 | 640 | 516 | 16.2 | 0.914 | 37.5 | 36.1 |
| 23 | 0.0226 | 511 | 647 | 20.3 | 0.730 | 41.8 | 40.2 |
| 24 | 0.0201 | 404 | 818 | 25.7 | 0.577 | 46.8 | 44.8 |
| 25 | 0.0179 | 320 | 1030 | 32.4 | 0.457 | 52.5 | 50.1 |
| 26 | 0.0159 | 253 | 1310 | 41.0 | 0.361 | 58.8 | 56.0 |
| 27 | 0.0142 | 202 | 1640 | 51.4 | 0.289 | 65.6 | 62.3 |
| 28 | 0.0126 | 159 | 2080 | 65.3 | 0.227 | 73.3 | 69.4 |
| 29 | 0.0113 | 123 | 2590 | 81.2 | 0.183 | 81.6 | 76.9 |
| 30 | 0.0100 | 100 | 3300 | 104.0 | 0.143 | 91.7 | 86.2 |
| 31 | 0.0089 | 79.2 | 4170 | 131 | 0.113 | 103 | 96 |
| 32 | 0.0080 | 64.0 | 5160 | 162 | 0.091 | 114 | 106 |
| 33 | 0.0071 | 50.4 | 6550 | 206 | 0.072 | 128 | 118 |
| 34 | 0.0063 | 39.7 | 8320 | 261 | 0.057 | 145 | 133 |
| 35 | 0.0056 | 31.4 | 10,500 | 331 | 0.045 | 163 | 149 |
| 36 | 0.0050 | 25.0 | 13,200 | 415 | 0.036 | 182 | 167 |

TABLE 4-10 Cont.
Copper-Wire Characteristics

| AWG | Nominal bare diameter (in) | Nominal circular mils | $\begin{aligned} & \text { Nominal } \\ & \text { feet } \\ & \text { per pound } \\ & \text { (bare) } \end{aligned}$ | Nominal ohms per 1000 ft (31) $20^{\circ} \mathrm{C}$ | Current- <br> carrying <br> capacity <br> @ 700 CM/A | Turns per linear inch |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | Single film coated | Heavy film coated |
| 37 | 0.0045 | 20.2 | 16,300 | 512 | 0.029 | 202 | 183 |
| 38 | 0.0040 | 16.0 | 20,600 | 648 | 0.023 | 225 | 206 |
| 39 | 0.0035 | 12.2 | 27,000 | 847 | 0.017 | 260 | 235 |
| 40 | 0.0031 | 9.61 | 34,400 | 1080 | 0.014 | 290 | 263 |
| 41 | 0.0028 | 7.84 | 42,100 | 1320 | 0.011 | 323 | 294 |
| 42 | 0.0025 | 6.25 | 52,900 | 1660 | 0.0089 | 357 | 328 |
| 43 | 0.0022 | 4.84 | 68,300 | 2140 | 0.0069 | 408 | 370 |
| 44 | 0.0020 | 4.00 | 82,600 | 2590 | 0.0057 | 444 | 400 |
| 45 | 0.00176 | 3.10 | 107,000 | 3350 | 0.0044 | 520 | 465 |
| 46 | 0.00157 | 2.46 | 134,000 | 4210 | 0.0035 | 580 | 510 |
| 47 | 0.00140 | 1.96 | 169,000 | 5290 | 0.0028 | 630 | 560 |
| 48 | 0.00124 | 1.54 | 215,000 | 6750 | 0.0022 | 710 | 645 |
| 49 | 0.00111 | 1.23 | 268,000 | 8420 | 0.0018 | 800 | 720 |
| 50 | 0.00099 | 0.980 | 337,000 | 10,600 | 0.0014 | 880 | 780 |
| 51 | 0.00088 | 0.774 | 427,000 | 13,400 | 0.0011 | 970 | 855 |
| 52 | 0.00078 | 0.608 | 543,000 | 17,000 | 0.00087 | 1080 | 935 |
| 53 | 0.00070 | 0.490 | 674,000 | 21,200 | 0.00070 | 1270 | 1110 |
| 54 | 0.00062 | 0.384 | 859,000 | 27,000 | 0.00055 | 1430 | 1220 |
| 55 | 0.00055 | 0.302 | 1,090,000 | 34,300 | 0.00043 | 1560 | 1330 |
| 56 | 0.00049 | 0.240 | 1,380,000 | 43,200 | 0.00034 | 1690 | 1450 |
| 57 | 0.000438 | 0.192 | 1,722,000 | 54,100 | 0.00027 | 1960 |  |
| 58 | 0.000390 | 0.152 | 2,166,000 | 68,000 | 0.00022 | 2160 |  |
| 59 | 0.000347 | 0.121 | 2,737,000 | 85,900 | 0.00017 | 2450 |  |
| 60 | 0.000309 | 0.090 | 3,453,000 | 108,400 | 0.00014 | 2740 |  |

## Chapter 5

## Design Data

## VACUUM-TUBE FORMULAS

The following formulas can be used to calculate the vacuum-tube properties listed.

Amplification Factor:

$$
\left.\mu=\frac{\Delta E_{\mathrm{b}}}{\Delta E_{\mathrm{z}}} \text { (with } I_{\mathrm{b}} \text { constant }\right)
$$

AC (Dynamic) Plate Resistance:

$$
\left.r_{\mathrm{r}}=\frac{\Delta E_{\mathrm{b}}}{\Delta I_{\mathrm{b}}} \text { (with } E_{\mathrm{c}} \text { constant }\right)
$$

Mutual Conductance (Transconductance):

$$
g_{\mathrm{m}}=\frac{\Delta I_{\mathrm{b}}}{\Delta E_{\mathrm{b}}} \text { (with } E_{\mathrm{b}} \text { constant) }
$$

Gain of an Amplifier Stage:

$$
\text { Gain }=\mu \frac{R_{\mathrm{t}}}{R_{\mathrm{t}}+r_{\mathrm{r}}}
$$

where
$\mu$ is the amplification factor,
$\Delta$ is the variation or change in value, $E_{b}$ is the plate voltage, in volts, $E_{\mathrm{c}}$ is the grid voltage, in volts, $I_{b}$ is the plate current, in amperes, $R_{1}$ is the plate-load resistance, in ohms, $r_{\mathrm{p}}$ is the AC plate resistance, in ohms, $g_{n}$ is the mutual conductance, in siemens.

## TRANSISTOR FORMULAS

The following formulas can be used to calculate the transistor properties listed.

Input Resistance:

$$
R_{\mathrm{i}}=\frac{\Delta V_{\mathrm{i}}}{\Delta I_{\mathrm{i}}}
$$

Current Gain (Fig. 5-1):

$$
\left.A_{\mathrm{i}}=\frac{\Delta I_{\mathrm{e}}}{\Delta I_{\mathrm{b}}} \text { (with } V_{\mathrm{c}} \text { constant }\right)
$$

The current gain of the common-base configuration is alpha ( $\alpha$ ):

$$
\alpha=\frac{\Delta I_{c}}{\Delta I_{c}}\left(\text { with } V_{c} \text { constant }\right)
$$



Fig. 5-1A. Common emitter.


Fig. 5-1B. Common base.


Fig. 5-1C. Common collector.


Fig. 5-11). Basic current paths.

The current gain of the common emitter is beta $(\beta)$ :

$$
\beta=\frac{\Delta I_{\mathrm{c}}}{\Delta I_{\mathrm{b}}} \text { (with } V_{\mathrm{c}} \text { constant) }
$$

A direct relationship exists between the alpha and beta of a transistor:

$$
\begin{aligned}
& \alpha=\frac{\beta}{1+\beta} \\
& \beta=\frac{\alpha}{1-\alpha}
\end{aligned}
$$

Voltage Gain:

$$
A_{\mathrm{v}}=\frac{\Delta V_{\mathrm{c}}}{\Delta V_{\mathrm{b}}}\left(\text { with } I_{\mathrm{c}} \text { constant }\right)
$$

Output Resistance:

$$
R_{\mathrm{o}}=\frac{\Delta V_{\mathrm{o}}}{\Delta I_{\mathrm{o}}}
$$

Power Gain:

$$
A_{\mathrm{p}}=\frac{\Delta P_{\mathrm{o}}}{\Delta P_{\mathrm{i}}}
$$

Base Current:

$$
I_{\mathrm{b}}=I_{\mathrm{c}}-I_{\mathrm{c}}=\frac{I_{\mathrm{c}}}{h_{\mathrm{fe}}}
$$

or

$$
=\frac{I_{\mathrm{c}}}{h_{\mathrm{ic}}}-I_{\mathrm{co}}
$$

Collector Current:

$$
I_{\mathrm{c}}=I_{\mathrm{c}}-I_{\mathrm{b}}=\alpha I_{\mathrm{e}}=h_{\mathrm{fc}} I_{\mathrm{h}}
$$

Collector Power:

$$
P_{\mathrm{c}}=V_{\mathrm{ce}} I_{\mathrm{c}}
$$

Emitter Current:

$$
I_{\mathrm{c}}=I_{\mathrm{b}}+I_{\mathrm{c}}(\text { Total Current })
$$

Small-Signal Emitter Resistance:

$$
r_{\mathrm{c}}=\frac{26}{I_{\mathrm{c}}}
$$

where
$I_{\mathrm{e}}$ is emitter current, in milliamperes.
Transconductance:

$$
g_{\mathrm{n}}=\frac{I_{\mathrm{c}}}{26}
$$

where
$I_{\mathrm{c}}$ is emitter current, in milliamperes.
Input Capacitance:

$$
C_{\mathrm{in}}=\frac{g_{\mathrm{m}}}{6.28 f_{\mathrm{mb}}}
$$

Upper Frequency Limit:

$$
f_{u}=\frac{g_{\mathrm{w}}}{6.28 C_{t}}
$$

Bandwidth:

$$
f_{\mathrm{hle}}=\frac{F_{\mathrm{htb}}}{h_{i \mathrm{ic}}}
$$

or

$$
f_{\mathrm{brb}}=h_{\mathrm{fc}} f_{\mathrm{hlic}}
$$

where
$\alpha$ is the current gain of a common-base configuration, in amperes, $A_{\mathrm{v}}$ is the voltage gain, in volts, $A_{i}$ is the current gain, in amperes, $A_{\mathrm{r}}$ is the power gain, in watts, $\beta$ is the current gain in a commonemitter configuration, in amperes,
$C_{1}$ is total capacitance, in picofarads, $C_{\text {in }}$ is input capacitance, in farads, $f_{\mathrm{u}}$ is upper frequency limit (unity gain), in megahertz,
$f_{\text {hic }}$ is the beta cutoff frequency ( $3-\mathrm{dB}$ point),
$f_{\text {lub }}$ is the alpha cutoff frequency ( $3-\mathrm{dB}$ point),
$g_{m}$ is transconductance, in microsiemens,
$h_{\mathrm{fe}}$ is $\beta=\alpha /(1-\alpha)$,
$I_{\mathrm{b}}$ is the base current, in amperes,
$I_{c}$ is the collector current, in amperes,
$I_{\mathrm{c}}$ is the emitter current, in amperes,
$I_{i}$ is the input current, in amperes,
$I_{0}$ is the output current, in amperes,
$P_{\mathrm{c}}$ is collector power, in watts,
$P_{P}$ is the input power, in watts,
$P_{0}$ is the output power, in watts,
$R_{\mathrm{i}}$ is the input resistance, in ohms,
$R_{\mathrm{o}}$ is the output resistance, in ohms,
$r_{\mathrm{c}}$ is small-signal emitter resistance, in ohms,
$V_{\mathrm{b}}$ is the base voltage, in volts,
$V_{c}$ is the collector voltage, in volts,
$V_{\mathrm{ce}}$ is the collector-emitter voltage, in volts,
$V_{i}$ is the input voltage, in volts, $V_{0}$ is the output voltage, in volts.
Terminology:
$h_{\mathrm{ie}}$ or $h_{\mathrm{ile}}=$ input impedance with output short-circuited (CE mode)
$h_{0 e}$ or $h_{22 c}=$ output admittance with open-circuit input
$h_{\mathrm{tc}}$ or $h_{12 c}=$ reverse open-circuit voltage amplification factor
$h_{\mathrm{ic}}$ or $h_{\text {2|c }}=$ forward short-circuit current amplification factor

Conventionally, capital letters denote DC relations, and lowercase letters denote AC small-signal relations.

## OPERATIONAL AMPLIFIERS (OP AMPS)

An op amp is a DC-coupled high-gain differential amplifier in integrated-circuit (IC) form. Typical op amps have very high input impedance and very low output impedance. Open-loop gain refers to the voltage gain of the op amp (without feedback) and working into its rated load value. An op amp has very high open-loop gain at zero frequency (DC), with progressively falling frequency response. The op amp is almost always operated with a large amount of negative feedback so that it has an essentially flat frequency response. A typical generalpurpose op amp provides full power output to 10 kHz and decreases to unity gain at 1 MHz .

A general-purpose op amp typically develops an open-loop gain of 100,000 times, with an input impedance of $5 \mathrm{M} \Omega$ and a low output impedance rated for working into a $1000-\Omega$ load. This type of op amp can provide an output-voltage swing of $\pm 10 \mathrm{~V}$. A basic rating is its slew rate, or its maximum possible rate of change in output voltage (transient response). A general-purpose op amp may have a rated slew rate of $0.5 \mathrm{~V} / \mu \mathrm{s}$ at unity gain. Although originally designed for analog computers, op amps are now used in radio and TV receivers, magnetic recording pickup head amplifiers, and a wide range of instrumentation applications.

Op amps are used as electronic integrators and differentiators to obtain characteristics that approximate mathematical integration and differentiation. Although many op amps require a positive as well as a
negative power-supply source, various op amps can operate from a single power-supply source, and some operate from the same power supply as the digital ICs in a computer. As shown in Figs. 5-2 through 5-6, op amps are also used as basic amplifiers, mixers, limiters, comparators, and filters with optimized characteristics.

Since a typical op amp has very low input impedance due to substantial negative feedback, the input terminal is regarded as a virtual ground that is almost at ground potential. In turn, the voltage gain of the am-


Fig. 5-2. Audio amplifier.


Fig. 5-3. Audio amplifier.


Fig. 5-4. Audio mixer.


Fig. 5-5. Limiting amplifier.
plifier is equal to the sum of the series input resistance and feedback resistance, divided by the input resistance. For example, if the series input resistance is $1000 \Omega$ and the feedback resistance is $100,000 \Omega$, the voltage gain of the op amp is essentially $101,000 /$ 1000 , or 101 times. Note that the inverting input of an op amp is indicated by a minus sign; the noninverting input is indicated by a plus sign.


Fig. 5-6. Active filter ( $\mathbf{1 2 0 0} \mathbf{H z}$ ).

## HEAT

When working with power transistors, integrated circuits, and heat sinks, the following equations will be useful:

Joule: The unit of energy required to move one coulomb between two points having a potentialenergy difference of 1 V .

## Electrical Equivalent of Heat

Calorie: 1 cal is equal to 4.18605 J . 1 cal will heat 1 g of water by $1^{\circ} \mathrm{C}$.
252 cal will heat 1 lb of water $1^{\circ} \mathrm{F}$.
1 kWh equals $860,000 \mathrm{cal}$. 1 cal equals $1 / 860 \mathrm{~Wh}$.
0.293 Wh will heat 1 lb of water $1^{\circ} \mathrm{F}$.

## Thermal Conductivity

Thermal conductivity is analogous to electrical conductivity. The unit of thermal conductivity is one calorie of heat flow per second per square centimeter per centimeter of thickness per degree Celsius temperature difference from one surface to the next.

## Thermal Resistance

The value of thermal resistance specified in a transistor data sheet is used to calculate the maximum permissible power dissipation at a given ambient temperature.

$$
\begin{aligned}
T_{\mathrm{i}}= & \text { junction temperature } \\
T_{\mathrm{a}} & =\text { ambient temperature } \\
\theta_{\mathrm{ia}}= & \text { ambient temperature } \\
& \text { junction thermal } \\
& \text { resistance } \\
P_{\mathrm{d}}= & \text { power dissipated } \\
\theta_{\mathrm{i}:}-P_{\mathrm{a}}= & \text { temperature rise }
\end{aligned}
$$

Example. A small transistor has a maximum rated junction temperature of $85^{\circ} \mathrm{C}$ and a thermal resistance of $0.5^{\circ} \mathrm{C} / \mathrm{mW}$. If the ambient temperature is $25^{\circ} \mathrm{C}$, the transistor may dissipate an amount of power to raise the junction temperature to $85^{\circ} \mathrm{C}$. This increase in temperature of $610^{\circ} \mathrm{C}$ will result, in this case, from a power of 120 mW in the transistor:

$$
\begin{aligned}
T_{1} & =T_{\Delta}+\theta_{\ldots, \ldots}\left(P_{\mathrm{a}}\right) \\
& =60^{\circ} \mathrm{C} /\left(0.5^{\circ} \mathrm{C} / \mathrm{mW}\right) \\
& =120 \mathrm{~mW}
\end{aligned}
$$

If a heat sink is correctly installed with thermally conducting washers, silicone grease, and proper bolting pressure, then the thermal resistance from transistor case to heat sink can be neglected. The junction-to-case thermal resistance is added to the sink-to-ambient thermal resistance to obtain the total thermal resistance.
$\theta_{\mathrm{a}}=$ junction to ambient temperature
$\theta_{\mathrm{jc}}=$ junction to case temperature
$\theta_{\mathrm{a}}=$ sink to ambient temperature
$\theta_{\mathrm{ja}}=\theta_{\mathrm{ic}}+\theta_{\mathrm{wa}}$

## FIBER OPTICS

Glass fibers (thin strands) are used to transmit light in curved paths. Bundles of fibers are analogous to coaxial cables and waveguides, where electromagnetic radiation is transmitted along an arbitrary path. Circular fibers, as shown in Fig. 5-7, are generally used, and fiber optics is based on principles of reflection, refraction, absorption, and transmission.

A simple round fiber (single mode fiber) is less efficient than a multimode fiber. A multimode fiber is formed like a coaxial cable; the glass fiber is surrounded by a tubular cladding. This cladding may be plastic, or it may be a different type of glass with a widely different index of refraction. A graded index fiber is formed with a gradual change in refractive index from the core to the surface, so that the light is continually refracted back toward the center of the core. Coherent light sources require either graded-index fibers or single-mode fibers. A light source feeds into an optical coupler and, in turn, into the optic fiber. At the receiving end, the optic fiber drives an optical coupler, which in turn feeds into a photodetector. Although fiber-optics transmission is very costly at present, it has the advantages of unusually high information capacity, miniature construction, and immunity to various types of electromagnetic interference. An optic-fiber cable is composed of hundreds of fibers, each of which may have a diameter of 50 or 100 mm . Half of the fibers transmit data in one direction, while the other half transmit data in the opposite direction.


Fig. 5-7A. Single-mode fiber.


Fig. 5-7B. Multimode fiber.


Fig. 5-7C. Graded-index fiber.

## THREE-PHASE POWER FORMULAS

In a three-phase system, there are three voltages, each separated by a phase difference of $120^{\circ}$. The power-supply input transformers may be connected in either a delta or a Y (star). Figure 5-8 shows how the terminals are placed in relationship to the coils. In the delta connection, there is one coil between each pair of terminals; in the Y connection, there are two. The voltage between two terminals of the Y -connected coil is equal to $\sqrt{3}$ times the voltage across one winding.

The formulas for determining the voltage across the secondary winding for each of the four possible connections are as follows:
$\Delta$ to $Y$ :

$$
E_{\uparrow}=E_{\mathrm{r}} \times N \times \sqrt{3}
$$

$Y$ to $\Delta:$

$$
E_{\bigcirc}=\frac{E_{\mathrm{r}} \times N}{\sqrt{3}}
$$



Fig. 5-8A. Delta connection.


Fig. 5-8B. Y connection.
$\Delta$ to $\Delta$ :

$$
E_{\checkmark}=E_{\mathrm{n}} \times N
$$

$Y$ to $Y$ :

$$
E_{\mathrm{s}}=E_{\mathrm{r}} \times N
$$

where
$E_{\text {, }}$ is the secondary voltage, in volts, $E_{\mathrm{p}}$ is the primary voltage, in volts, $N$ is the turns ratio.

## COIL WINDINGS

## Single-Layer Coils (Fig. 5-9)

The inductance of single-layer coils can be calculated to an accuracy of approximately $1 \%$ with the formula:

$$
L=\frac{(N \times A)^{2}}{9 A+10 B}
$$



## Fig. 5-9

To find the number of turns required for a single-layer coil with a given inductance, the foregoing formula is rearranged as follows:

$$
N=\frac{\sqrt{L(9 A+10 B)}}{A}
$$

where
$L$ is the inductance, in microhenrys,
$N$ is the number of turns,
$A$ is the mean radius, in inches, $B$ is the length of the coil, in inches.

## Multilayer Coils (Fig. 5-10)

The inductance of a multilayer coil of rectangular cross section can be computed from the formula:

$$
L=\frac{0.8(N \times A)^{2}}{6 A+9 B+10 C}
$$

where
$L$ is the inductance, in microhenrys, $N$ is the number of turns,
$A$ is the mean radius, in inches,
$B$ is the length of the coil, in inches,
$C$ is the depth of the coil, in inches.

## Single-Layer Air-Core Coil Chart

The chart in Fig. 5-11 provides an easy


Fig. 5-10
method for determining either the inductance or the number of turns for single-layer coils. When the length of the winding, the diameter, and the number of turns of the coil are known, the inductance can be found by placing a straightedge from the "Turns" scale to the "Ratio" (diameter $\div$ length) scale and noting the point where the straightedge intersects the "Axis" scale. Then lay the straightedge from the point of intersection of the "Axis" scale to the "Diameter" scale. The point at which this line intersects the "Inductance" scale indicates the inductance, in microhenrys, of the coil. The number of turns can be determined by reversing the procedure.

After finding the number of turns, consult Table 4-8 to determine the size of wire to be used.

Example. What is the inductance of a single-layer air-core coil having 80 turns wound to 4 in in length on a coil form 2 in in diameter?
Answer. $\quad 130 \mu \mathrm{H}$. (First lay the straightedge as indicated by the line labeled "Example 1A." Then lay the straightedge as indicated by the line labeled "Example 1B.")

## Design Data



Fig. 5-11. Single-layer coil chart.

## CURRENT RATINGS FOR EQUIPMENT AND CHASSIS WIRING

Table 5-1 lists the recommended current rating (for continuous duty) for various wire sizes used on electronic equipment and chassis wiring.

FILTER FORMULAS

## Constant-k Filters

A constant-k filter presents an impedance match to the line at only one fre-
quency and a mismatch at all others. The three basic configurations are the T, L (halfsection), and pi.

A constant-k low-pass filter will pass frequencies below and attenuate those above a set frequency. Figure 5-12 gives the circuit configurations, attenuation characteristics, and impedance characteristics of the three types of constant-k low-pass filters.

The attenuation of the $L$ section is equal to half that of the T or pi sections. The impedance of the filter is equal to the characteristic impedance of the line $\left(Z_{0}\right)$ at the zero

TABLE 5-1
Recommended Current Ratings (Continuous Duty)

| Wire size |  | Copper conductor $\left(100^{\circ} \mathrm{C}\right)$ nominal resistance $(\Omega / 1000 \mathrm{ft}$ ) | Maximum current (A) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Copper wire | Aluminum wire |  |
| AWG | Circular mils |  | Wiring in free air | Wiring confined* | Wiring in free air | Wiring confined* |
| 32 | 63.2 |  | 188.0 | 0.53 | 0.32 |  |  |
| 30 | 100.5 | 116.0 | 0.86 | 0.52 |  |  |
| 28 | 159.8 | 72.0 | 1.4 | 0.83 |  |  |
| 26 | 254.1 | 45.2 | 2.2 | 1.3 |  |  |
| 24 | 404.0 | 28.4 | 3.5 | 2.1 |  |  |
| 22 | 642.4 | 22.0 | 7.0 | 5.0 |  |  |
| 20 | 1022 | 13.7 | 11.0 | 7.5 |  |  |
| 18 | 1624 | 6.50 | 16 | 10 |  |  |
| 16 | 2583 | 5.15 | 22 | 13 |  |  |
| 14 | 4107 | 3.20 | 32 | 17 |  |  |
| 12 | 6530 | 2.02 | 41 | 23 |  |  |
| 10 | 10,380 | 1.31 | 55 | 33 |  |  |
| 8 | 16,510 | 0.734 | 73 | 46 | 60 | 36 |
| 6 | 26,250 | 0.459 | 101 | 60 | 83 | 50 |
| 4 | 41,740 | 0.290 | 135 | 80 | 108 | 66 |
| 2 | 66,370 | 0.185 | 181 | 100 | 152 | 82 |
| 1 | 83,690 | 0.151 | 211 | 125 | 174 | 105 |
| 0 | 105,500 | 0.117 | 245 | 150 | 202 | 123 |
| 00 | 133,100 | 0.092 | 283 | 175 | 235 | 145 |
| 000 | 167,800 | 0.074 | 328 | 200 | 266 | 162 |
| 0000 | 211,600 | 0.059 | 380 | 225 | 303 | 190 |

[^6]frequency only. For all other frequencies, the input and output impedance of the filter are equal to $Z_{1}$ or $Z_{1}{ }^{\prime}$, as shown in Fig. 5-12.

The values for $L_{1}, C_{2}, Z_{0}$, and $f_{\mathrm{c}}$ can be computed from the following formulas:

$$
\begin{aligned}
& L_{1}=\frac{Z_{t}}{\pi f_{c}} \\
& C_{2}=\frac{1}{\pi f_{i} Z_{0}} \\
& Z_{0}=\sqrt{\frac{L_{1}}{C_{2}}} \\
& f_{c}=\frac{1}{\pi \sqrt{L_{1} C_{2}}}
\end{aligned}
$$

The values computed for $L_{1}$ and $C_{2}$ must be divided in half, where specified in Fig. 512. That is, the coils in the T and L sections, and the capacitors in the $L$ and pi sections,
are equal to one-half the computed value.
A high-pass filter will pass all frequencies above and attenuate all those below a set frequency.

The circuit configurations, attenuation characteristics, and impedance characteristics of constant-k high-pass filters are given in Fig. 5-13. The formulas for computing $L_{2}, C_{1}, Z_{0}$, and $f_{\mathrm{c}}$ are as follows:

$$
\begin{aligned}
L_{2} & =\frac{Z_{0}}{4 \pi f_{\mathrm{c}}} \\
C_{1} & =\frac{1}{4 \pi f_{\mathrm{c}} Z_{0}} \\
Z_{0} & =\sqrt{\frac{L_{2}}{C_{1}}} \\
f_{\mathrm{c}} & =\frac{1}{4 \pi \sqrt{L_{2} C_{1}}}
\end{aligned}
$$

Fig. 5-12A. T section.


Fig. 5-12B. L section.


Fig. 5-12C. Pi section.



Fig. 5-13A. T section.

Fig. 5-13B. L section.

Notice that the values computed for $C$ in the foregoing formulas must be doubled in the T and L sections. Likewise, the value computed for $L$ must be doubled in the $L$ and pi sections.

Bandpass filters will pass frequencies of a certain band and reject all others. The configuration and the transmission characteristics for a constant-k bandpass filter are given in Fig. 5-14. The formulas for computing the various values are:

$$
\begin{aligned}
& L_{1}=\frac{Z_{0}}{\pi\left(f_{2}-f_{1}\right)} \\
& L_{2}=\frac{\left(f_{2}-f_{1}\right)}{4 \pi f_{1} f_{2}} \\
& C_{1}=\frac{\left(f_{2}-f_{1}\right)}{4 \pi f_{1} f_{2} Z_{0}} \\
& C_{2}=\frac{1}{\pi\left(f_{2}-f_{1}\right) Z_{0}}
\end{aligned}
$$



Fig. 5-14A. Configuration.


Fig. 5-14B. Transmission characteristics.

## Design Data

As before, some values must be doubled or halved, as shown in Fig. 5-14.

A band-rejection filter will reject a certain band of frequencies and pass all others. The configuration and the transmission characteristics of a constant-k band-rejection filter are given in Fig. 5-15. The formulas for computing the component values, frequencies, and line impedance are:

$$
\begin{aligned}
& L_{1}=\frac{\left(f_{2}-f_{1}\right) Z_{0}}{\pi f_{1} f_{2}} \\
& L_{2}=\frac{Z_{0}}{4 \pi\left(f_{2}-f_{1}\right)} \\
& C_{1}=\frac{1}{4 \pi\left(f_{2}-f_{1}\right) Z_{0}} \\
& C_{2}=\frac{\left(f_{2}-f_{1}\right)}{\pi f_{1} f_{2} Z_{0}} \\
& f_{\mathrm{m}}=\sqrt{f_{1} f_{2}}=\frac{1}{2 \pi \sqrt{L_{1} C_{1}}}=\frac{1}{2 \pi \sqrt{L_{2} C_{2}}} \\
& Z_{0}=\sqrt{\frac{L_{1}}{C_{2}}}=\sqrt{\frac{L_{2}}{C_{1}}}
\end{aligned}
$$

where
$L_{1}$ and $L_{2}$ are the inductances of the coils, in henrys,
$C_{1}$ and $C_{2}$ are the capacitances of the capacitors, in farads,
$f_{1}$ and $f_{2}$ are the frequencies at the edge of the passband, in hertz,
$f_{\mathrm{m}}$ is the frequency at the center of the passband, in hertz,
$f_{1 \infty}$ and $f_{2 \infty}$ are the frequencies of infinite attenuation, in hertz,
$Z_{0}$ is the line impedance, in ohms.


Fig. 5-15A. Configuration.


Fig. 5-15B. Transmission characteristics.

## m-Derived Filters

In an $m$-derived filter, the designer can control either the impedance or the attenuation characteristics. The values are first computed as for a constant-k filter and then modified by an algebraic expression containing the constant $m$. The term $m$ is a positive number between zero and one. Its value governs the characteristics of the filter.

Two frequencies - the cutoff and the frequency of infinite attenuation - are involved in the design of $m$-derived filters. By selecting the proper value for $m$, it is possible to control the spacing between the two frequencies. Figure 5-16 shows the effect different values of $m$ have on the impedance characteristics. The best impedance match is obtained when $m$ is equal to 0.6 ; hence, this value is usually employed.

The attenuation characteristics for the various values of $m$ are given in Fig. 5-17.

Handbook of Electronics Tables and Formulas


Fig. 5-16


Fig. 5-17

The attenuation rises to maximum and then drops on all curves. This graph applies to both low- and high-pass filters.

The value of $m$ is determined from the formulas:

$$
m=\sqrt{1-\left(\frac{f_{\mathrm{c}}}{f_{\infty}}\right)^{2}}
$$

or

$$
m=\sqrt{1-\left(\frac{f_{\infty}}{f_{c}}\right)^{2}}
$$

Select the formula that will give a positive number.

The configurations for $m$-derived filters are classified as either series or shunt. Those for the series $m$-derived low-pass filters are given in Fig. 5-18. The formulas are as follows:

$$
\begin{aligned}
& L_{1}=m\left(\frac{Z_{0}}{2 \pi f_{\mathrm{c}}}\right) \\
& L_{2}=\left(\frac{1-m^{2}}{4 m}\right)\left(\frac{Z_{0}}{2 \pi f_{\mathrm{c}}}\right) \\
& C_{2}=\left(\frac{1}{\pi f_{\mathrm{c}} Z_{0}}\right)
\end{aligned}
$$

For a series $m$-derived high-pass filter (Fig. 5-19), the formulas are:

$$
\begin{aligned}
L_{2} & =\frac{\left(\frac{Z_{0}}{4 \pi f_{\mathrm{c}}}\right)}{m} \\
C_{1} & =\frac{\left(\frac{1}{4 \pi f_{\mathrm{c}} Z_{0}}\right)}{m} \\
C_{2} & =\left(\frac{4 m}{1-m^{2}}\right)\left(\frac{1}{4 \pi f_{\mathrm{c}} Z_{0}}\right)
\end{aligned}
$$

The configurations for shunt $m$-derived low-pass filters are given in Fig. 5-20. The formulas for computing the component values are:

$$
\begin{aligned}
& L_{1}=m\left(\frac{Z_{0}}{\pi f_{6}}\right) \\
& C_{1}=\left(\frac{1-m^{2}}{4 m}\right)\left(\frac{1}{\pi f_{\mathrm{c}} Z_{0}}\right) \\
& C_{2}=m\left(\frac{1}{\pi f_{\mathrm{c}} Z_{0}}\right)
\end{aligned}
$$



Fig. 5-18A. T section.


Fig. 5-18B. L section.


Fig. 5-18C. Pi section.


Fig. 5-19A. T section.


Fig. 5-20A. T section.


Fig. 5-21A. T section.


Fig. 5-19B. L section.


Fig. 5-20B. L section.


Fig. 5-21B. L section.


Fig. 5-19C . Pi section.


Fig. 5-20C. Pi section.


Fig. 5-21C. Pi section.

For shunt $m$-derived high-pass filters (Fig. 5-21), the formulas are:

$$
\begin{aligned}
& L_{1}=\left(\frac{4 m}{1-m^{2}}\right)\left(\frac{Z_{0}}{4 \pi f_{\mathrm{c}}}\right) \\
& L_{2}=\frac{\left(\frac{Z_{0}}{4 \pi f_{\mathrm{c}}}\right)}{m} \\
& C_{1}=\frac{\left(\frac{1}{4 \pi f_{\mathrm{c}} Z_{0}}\right)}{m}
\end{aligned}
$$

where
$L_{1}$ and $L_{2}$ are the inductances of the coils, in henrys,
$C_{1}$ and $C_{2}$ are the capacitances of the capacitors, in farads,
$m$ is a constant between 0 and 1 , $Z_{0}$ is the line impedance, in ohms, $f_{c}$ is the cutoff frequency, in hertz.

## ATTENUATOR FORMULAS

## General

An attenuator is an arrangement of noninductive resistors used in an electrical
circuit to reduce the audio- or radiosignal strength without introducing distortion. The resistors may be fixed or variable. Attenuators can be designed to work between equal or unequal impedances; hence, they are often used as impedance-matching networks.

Any attenuator working between unequal impedances must introduce a certain minimum loss. These values are given in the graph of Fig. 5-22. The impedance ratio is the input impedance divided by the output impedance, or vice versa-whichever gives a value of more than one.

A factor is used in the calculation of resistor values in attenuator networks. Called $K$, it is the ratio of current, voltage, or power corresponding to a given value of at-
tenuation in decibels. Table 5-2 gives the value of $K$ for the more common loss values.

The four steps in the design of a pad are:
(1) Determine the type of network required.
(2) If impedances are unequal, calculate the ratio of input to output impedance (or output to input impedance) and refer to Fig. 522 for the minimum loss value. (3) From Table 5-2, find the value of $K$ for the desired loss. (4) Calculate the resistor values using the following formulas.

## Combining or Dividing Network

(Fig. 5-23)

$$
R_{\mathrm{B}}=\left(\frac{N-1}{N+1}\right) Z
$$



Fig. 5-22

TABLE 5-2
K Factors for Calculating Attenuator Loss

| $\mathbf{d B}$ | $\boldsymbol{K}$ | $\mathbf{d B}$ | $\boldsymbol{K}$ | $\mathbf{d B}$ | $\boldsymbol{K}$ | $\mathbf{d B}$ | $\boldsymbol{K}$ |
| :---: | :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 0.05 | 1.0058 | 9.5 | 2.9854 | 29.0 | 28.184 | 49.0 | 281.84 |
| 0.1 | 1.0116 | 10.0 | 3.1623 | 30.0 | 31.623 | 50.0 | 316.23 |
| 0.5 | 1.0593 | 11.0 | 3.5481 | 31.0 | 35.481 | 51.0 | 354.81 |
| 1.0 | 1.1220 | 12.0 | 3.9811 | 32.0 | 39.811 | 52.0 | 398.11 |
| 1.5 | 1.1885 | 13.0 | 4.4668 | 33.0 | 44.668 | 54.0 | 501.19 |
| 2.0 | 1.2589 | 14.0 | 5.0119 | 34.0 | 50.119 | 55.0 | 562.34 |
| 2.5 | 1.3335 | 15.0 | 5.6234 | 35.0 | 56.234 | 56.0 | 630.96 |
| 3.0 | 1.4125 | 16.0 | 6.3096 | 36.0 | 63.096 | 57.0 | 707.95 |
| 3.5 | 1.4962 | 17.0 | 7.0795 | 37.0 | 70.795 | 58.0 | 794.33 |
| 4.0 | 1.5849 | 18.0 | 7.9433 | 38.0 | 79.433 | 60.0 | 1000.0 |
| 4.5 | 1.6788 | 19.0 | 8.9125 | 39.0 | 89.125 | 65.0 | 1778.3 |
| 5.0 | 1.7783 | 20.0 | 10.0000 | 40.0 | 100.000 | 70.0 | 3162.3 |
| 5.5 | 1.8837 | 21.0 | 11.2202 | 41.0 | 112.202 | 75.0 | 5623.4 |
| 6.0 | 1.9953 | 22.0 | 12.589 | 42.0 | 125.89 | 80.0 | 10,000 |
| 6.5 | 2.1135 | 23.0 | 14.125 | 43.0 | 141.25 | 85.0 | 17,783 |
| 7.0 | 2.2387 | 24.0 | 15.849 | 44.0 | 158.49 | 90.0 | 31,623 |
| 7.5 | 2.3714 | 25.0 | 17.783 | 45.0 | 177.83 | 95.0 | 56,234 |
| 8.0 | 2.5119 | 26.0 | 19.953 | 46.0 | 199.53 | 100.0 | 105 |
| 8.5 | 2.6607 | 27.0 | 22.387 | 47.0 | 223.87 | 28.0 | 251.19 |

where
$R_{\mathrm{B}}$ is the resistance of the building-out resistors, in ohms,
$N$ is the number of circuits fed by the source impedance,
$Z$ is the source impedance, in ohms.


Fig. 5-23

T-Type Attenuator (Between Equal Impedances) (Fig. 5-24)

$$
\begin{aligned}
R_{1} \text { and } R_{2} & =\left(\frac{K-1}{K+1}\right) Z \\
R_{2} & =\left(\frac{K}{K^{2}-1}\right) 2 Z
\end{aligned}
$$

where
$K$ is the impedance factor,
$R_{1}, R_{2}$, and $R_{3}$ are the measured resistances, in ohms.


Fig. 5-24

## H-Type Attenuator (Balanced-T Attenuator)

Calculate the values for $R_{1}, R_{2}$, and $R_{3}$ as for an unbalanced T-attenuator (Fig. 5-24). Then halve the values of $R_{1}$ and $R_{2}$, as shown in Fig. 5-25. The tap on $R_{3}$ is exactly in the center.


Fig. 5-25
Taper Pad (T-Type Attenuator Between Unequal Impedances) (Fig. 5-26)

$$
\begin{aligned}
& R_{1}=Z_{1}\left(\frac{K^{2}+1}{K^{2}-1}\right)-2 \sqrt{Z_{1} Z_{2}}\left(\frac{K}{K^{2}-1}\right) \\
& R_{2}=Z_{2}\left(\frac{K^{2}+1}{K^{2}-1}\right)-2 \sqrt{Z_{1} Z_{2}}\left(\frac{K}{K^{2}-1}\right) \\
& R_{3}=2 \sqrt{Z_{1} Z_{2}}\left(\frac{K}{K^{2}-1}\right)
\end{aligned}
$$

where
$K$ is the impedance factor, $R_{\mathrm{t}}, R_{2}$, and $R_{\mathrm{i}}$ are the measured resistances, in ohms, $Z_{1}$ is the larger impedance, in ohms, $Z_{2}$ is the smaller impedance, in ohms.


Fig. 5-26

## Bridged-T Attenuator (Unbalanced)

(Fig. 5-27)

$$
\begin{aligned}
& R_{\mathrm{t}}=Z \\
& R_{\mathrm{s}}=(K-1) Z \\
& R_{6}=\left(\frac{1}{K-1}\right) Z
\end{aligned}
$$

$R_{5}$ and $R_{6}$ are connected to a common shaft, and each varies inversely in value with respect to the other.


Fig. 5-27

## Balanced Bridged-T Attenuator

Calculate the values for $R_{1}, R_{5}$, and $R_{6}$ as for an unbalanced bridged-T attenuator (Fig. 5-27). Then halve the values as shown in Fig. 5-28.


Fig. 5-28

## L-Type Attenuators

An L-type attenuator can supply an impedance match in only one direction. If the impedances it works out of and into are unequal, it can be made to match either-but not both-impedances. The arrows in Figs. 5-29 through 5-32 indicate the direction of impedance match.

Between equal impedances and with the impedance match in the direction of the series arm:

$$
\begin{aligned}
& R_{1}=Z\left(\frac{K-1}{K}\right) \\
& R_{2}=Z\left(\frac{1}{K-1}\right)
\end{aligned}
$$



Fig. 5-29
Between equal impedances and with the impedance match in the direction of the shunt arm:

$$
\begin{aligned}
& R_{1}=Z(K-1) \\
& R_{2}=Z\left(\frac{K}{K-1}\right)
\end{aligned}
$$



Fig. 5-30

Between unequal impedances and with the impedance match toward the larger value:

$$
\begin{aligned}
& R_{1}=\left(\frac{Z_{1}}{S}\right)\left(\frac{K S-1}{K}\right) \\
& R_{2}=\left(\frac{Z_{1}}{S}\right)\left(\frac{1}{K-S}\right)
\end{aligned}
$$

where
$S$ equals $\sqrt{Z_{1} / Z_{2}}$.


Fig. 5-31
Between unequal impedances and with the impedance match toward the smaller value:

$$
\begin{aligned}
& R_{1}=\left(\frac{Z_{1}}{S}\right)(K-S) \\
& R_{2}=\frac{Z_{1}}{S}\left(\frac{K}{K S-1}\right)
\end{aligned}
$$

where
$S$ equals $\sqrt{Z_{1} / Z_{2}}$.


Fig. 5-32

## Design Data

## Pi-Type Attenuator (Between Equal

 Impedances) (Fig. 5-33)$$
\begin{aligned}
& R_{1}=Z\left(\frac{K+1}{K-1}\right) \\
& R_{2}=\left(\frac{Z}{2}\right)\left(\frac{K^{2}-1}{K}\right)
\end{aligned}
$$



Fig. 5-33

## Pi-Type Attenuator (Between Unequal Impedances) (Fig. 5-34)

$$
\begin{aligned}
& R_{1}=Z_{1}\left(\frac{K^{2}-1}{K^{2}-2 K S+1}\right) \\
& R_{2}=\left(\frac{\sqrt{Z_{1} Z_{2}}}{2}\right)\left(\frac{K^{2}-1}{K}\right) \\
& R_{3}=Z_{2}\left(\frac{K^{2}-1}{K_{2}-2 \frac{K}{S}+1}\right)
\end{aligned}
$$

where
$S$ equals $\sqrt{Z_{1} / Z_{2}}$.


Fig. 5-34

## O-Type Attenuators

Calculate the values for a pi-type attenuator (Figs. 5-33 and 5-34), then halve the values for the series resistors as shown in Figs. 5-35 (balanced) and 5-36 (unbalanced).


Fig. 5-35


Fig. 5-36

## U-Type Attenuator (Figs. 5-37 and 5-38)

For impedance match in the direction of the series arms:

$$
\begin{aligned}
& R_{1}=\left(\frac{Z_{1}}{2 S}\right)\left(\frac{K S-1}{K}\right) \\
& R_{2}=\left(\frac{Z_{1}}{S}\right)\left(\frac{1}{K-S}\right)
\end{aligned}
$$



Fig. 5-37

For impedance match in the direction of the shunt arm:

$$
\begin{aligned}
& R_{\mathrm{t}}=\left(\frac{Z_{1}}{2 S}\right)(K-S) \\
& R_{2}=\left(\frac{Z_{1}}{S}\right)\left(\frac{K}{K S-1}\right)
\end{aligned}
$$

where
The arrows indicate the direction of the impedance match,
$S$ equals $\sqrt{Z_{1} / Z_{2}}$.


Fig. 5-38

## Lattice-Type Attenuator (Fig. 5-39)

$$
\begin{aligned}
& R_{1}=\left(\frac{K-1}{K+1}\right) Z \\
& R_{2}=\left(\frac{K+1}{K-1}\right) Z
\end{aligned}
$$



Fig. 5-39

## Ladder-Type Attenuator (Fig. 5-40)

$$
\begin{aligned}
& R_{1}=\left(\frac{K^{2}-1}{2 K}\right) Z \\
& R_{2}=\left(\frac{K+1}{K-1}\right) Z \\
& R_{3}=\frac{R_{2} \times Z}{R_{2}+Z} \\
& R_{4}=\frac{Z}{2} \\
& Z_{\mathrm{t} 1}=Z_{\mathrm{out}}
\end{aligned}
$$

where
$K$ depends on the loss per step-not on the total loss.


Fig. 5-40

Note. An instructive special case of an L-section resistive network with equal input and terminating resistances, regardless of the number of sections, is shown in Fig. 5-41. Observe that if $10-\Omega$ series resistors and $100-\Omega$ shunt resistors are used with a $27-\Omega$ terminating resistance, the input resistance will always be $37 \Omega$, regardless of the number of sections. (The characteristic resistance of the network is $37 \Omega$.)

## Design Data



- More precisely 37015621 !
* More prectsely 27015621 ?

Fig. 5-41

## STANDARD <br> POTENTIOMETER TAPERS

(Fig. 5-42)
Taper S straight or uniform resistance change with rotation

Taper T right-hand $30 \%$ resistance at $50 \%$ of counterclockwise rotation

Taper V right-hand $20 \%$ resistance at $50 \%$ of counterclockwise rotation


Fig. 5-42

Taper W left-hand $20 \%$ resistance at $50 \%$ of clock wise rotation

Taper $Z$ left-hand (log. audio) $10 \%$ resistance at $50 \%$ clockwise rotation

Taper Y left-hand $5 \%$ resistance at $50 \%$ of clockwise rotation

## Chapter 6

## Mathematical Tables and Formulas

MATHEMATICAL CONSTANTS

$$
\begin{array}{ll}
\pi & =3.1416 \\
\pi^{2} & =9.8696 \\
\pi^{3} & =31.0063 \\
\frac{1}{\pi} & =0.3183 \\
\frac{1}{\pi^{2}} & =0.1013 \\
\frac{1}{\pi^{3}} & =0.0323 \\
\sqrt{\pi} & =1.7725 \\
\frac{1}{\sqrt{\pi}} & =0.5642 \\
\frac{1}{2 \pi} & =0.1592 \\
\left(\frac{1}{2 \pi}\right)^{2} & =0.0253 \\
2 \pi & =6.2832 \\
(2 \pi)^{2} & =39.4786 \\
4 \pi & =12.5664 \\
\frac{\pi}{2} & =1.5708
\end{array}
$$

$$
\begin{array}{ll}
\sqrt{\frac{\pi}{2}} & =1.2533 \\
\sqrt{2} & =1.4142 \\
\sqrt{3} & =1.7321 \\
\frac{1}{\sqrt{2}} & =0.7071 \\
\frac{1}{\sqrt{3}} & =0.5773 \\
\log \pi & =0.4971 \\
\log \pi^{2} & =0.9943 \\
\log \sqrt{\pi} & =0.2486 \\
\log \frac{\pi}{2} & =0.1961
\end{array}
$$

MATHEMATICAL SYMBOLS

$$
\begin{aligned}
& \times \text { or } \cdot \text { multiplied by } \\
& \quad \div \text { divided by } \\
& \quad=\text { equals } \\
& \quad \neq \text { does not equal } \\
& <\text { is less than } \\
& \quad \pm \text { plus or minus }
\end{aligned}
$$

$\equiv$ identical with

+ positive, add, and plus
- negative, subtract, and minus
$>$ is greater than
$\geq$ equal to or greater than
$\leq$ equal to or less than
$\therefore$ therefore
|| parallel to
$\angle$ angle
$\leftrightarrow$ is much less than
$>$ is much greater than
$\perp$ perpendicular to
$|n|$ absolute value of $n$
$\cong$ is approximately equal to
square root


## FRACTIONAL INCH, DECIMAL, AND MILLIMETER EQUIVALENTS

Table 6-1 gives the decimal inch and millimeter equivalents of fractional parts of an inch by 64ths to four significant figures.

## POWERS OF 10

## Exponent Determination

Large numbers can be simplified by using powers of 10 . For example, some of the multiples of 10 from 1 to $1,000,000$, with their equivalents in powers of 10 , are:

[^7]TABLE 6-1
Fractional Inch, Decimal, and Millimeter Equivalents

| Fractional <br> inch | Decimal <br> inch | Millimeter <br> equivalent | Practional <br> inch | Decimal <br> inch | Millimeter <br> equivalent |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $1 / 64$ | 0.0156 | 0.397 | $33 / 64$ | 0.5156 | 13.097 |
| $1 / 32$ | 0.0313 | 0.794 | $17 / 32$ | 0.5313 | 13.494 |
| $3 / 64$ | 0.0469 | 1.191 | $9 / 16$ | 0.5469 | 13.891 |
| $1 / 16$ | 0.0625 | 1.588 | $35 / 64$ | 0.5625 | 14.288 |
| $5 / 64$ | 0.0781 | 1.934 | $37 / 64$ | 0.5781 | 14.684 |
| $3 / 32$ | 0.0938 | 2.381 | $19 / 32$ | 0.5938 | 15.081 |
| $7 / 64$ | 0.1094 | 2.778 | $39 / 64$ | 0.6094 | 15.478 |
| $1 / 8$ | 0.1250 | 3.175 | $5 / 4$ | 0.6250 | 15.875 |
| $9 / 64$ | 0.1406 | 3.572 | $41 / 64$ | 0.6406 | 16.272 |
| $5 / 32$ | 0.1563 | 3.969 | $21 / 32$ | 0.6563 | 16.669 |
| $11 / 64$ | 0.1719 | 4.366 | $43 / 64$ | 0.6719 | 17.066 |
| $3 / 16$ | 0.1875 | 4.763 | $11 / 16$ | 0.6875 | 17.463 |
| $13 / 64$ | 0.2031 | 5.159 | $45 / 64$ | 0.7031 | 17.859 |
| $7 / 32$ | 0.2188 | 5.556 | $23 / 32$ | 0.7188 | 18.256 |
| $15 / 64$ | 0.2344 | 5.953 | $47 / 64$ | 0.7344 | 18.653 |
| $1 / 4$ | 0.2500 | 6.350 | $3 / 4$ | 0.7500 | 19.050 |
| $17 / 64$ | 0.2656 | 6.747 | $49 / 64$ | 0.7656 | 19.447 |
| $1 / 32$ | 0.2813 | 7.144 | $25 / 32$ | 0.7813 | 19.844 |
| $19 / 64$ | 0.2969 | 7.541 | $51 / 64$ | 0.7969 | 20.241 |
| $5 / 16$ | 0.3125 | 7.938 | $13 / 16$ | 0.8125 | 20.638 |
| $21 / 64$ | 0.3281 | 8.334 | $53 / 64$ | 0.8281 | 21.034 |
| 1132 | 0.3438 | 8.731 | $27 / 32$ | 0.8438 | 21.431 |
| $23 / 64$ | 0.3594 | 9.128 | $55 / 64$ | 0.8594 | 21.828 |
| $3 / 8$ | 0.3750 | 9.525 | $7 / 8$ | 0.8750 | 22.225 |
| $25 / 64$ | 0.3906 | 9.922 | $57 / 64$ | 0.8906 | 22.622 |
| $13 / 32$ | 0.4063 | 10.319 | $29 / 32$ | 0.9063 | 23.019 |
| $27 / 64$ | 0.4219 | 10.716 | $5 / 64$ | 0.9219 | 23.416 |
| $7 / 16$ | 0.4375 | 11.113 | $15 / 16$ | 0.9375 | 23.813 |
| $29 / 64$ | 0.4531 | 11.509 | $61 / 64$ | 0.9531 | 24.209 |
| $15 / 32$ | 0.4688 | 11.906 | $31 / 32$ | 0.9688 | 24.606 |
| $31 / 64$ | 0.4844 | 12.303 | $63 / 64$ | 0.9844 | 25.003 |
| $1 / 2$ | 0.5000 | 12.700 | 1 | 1.000 | 25.400 |
|  |  |  |  |  |  |

$$
\begin{aligned}
1 & =10^{0 *} \\
10 & =10^{1} \\
100 & =10^{2} \\
1000 & =10^{3} \\
10,000 & =10^{+} \\
100,000 & =10^{3} \\
1,000,000 & =10^{6}
\end{aligned}
$$

Likewise, powers of 10 can be used to simplify decimal expressions. Some of the submultiples of 10 from 0.1 to 0.000001 , with their equivalents in powers of 10 , are:

$$
\begin{aligned}
0.1 & =10^{-1} \\
0.01 & =10^{-2} \\
0.001 & =10^{-3} \\
0.0001 & =10^{-} \\
0.00001 & =10^{2} \\
0.000001 & =10^{-2}
\end{aligned}
$$

Any whole number can be expressed as a smaller whole number, and any decimal can be expressed as a whole number, by moving the decimal point to the left or right and expressing the number as a power of 10 . If the decimal point is moved to the left, the power is positive and is equal to the number of places the decimal point was moved. If the decimal point is moved to the right, the power is negative and is equal to the number of places the decimal point was moved.

## Example.

$$
\begin{aligned}
1.23 & =0.0123 \times 10^{2} \\
456.7 & =4.567 \times 10^{:} \\
78,900 & =78.9 \times 10^{5} \\
0.00012 & =1.2 \times 10^{-1} \\
0.0345 & =34.5 \times 10^{-7} \\
0.678 & =67.8 \times 10^{2}
\end{aligned}
$$

## Addition and Subtraction

To add or subtract using powers of 10 , first convert all numbers to the same power of 10 . The numbers can then be added or subtracted, and the answer will be in the same power of 10 .

## Example.

$$
\begin{aligned}
& 9.32 \times 10^{2}+17.63 \times 10^{2}+297=? \\
& 9.32 \times 10^{2}=0.932 \times 10^{2} \\
& 17.63 \times 10^{2}=17.630 \times 10^{3} \\
& 297=\frac{0.297 \times 10^{2}}{18.859 \times 10^{2}}=18,859
\end{aligned}
$$

## Example.

$$
18.47 \times 10^{2}-1.59 \times 10^{2}=?
$$

$$
\begin{aligned}
18.47 \times 10^{2} & =1.847 \times 10^{2} \\
1.59 \times 10^{\prime} & =\frac{1.590 \times 10^{3}}{0.257 \times 10^{3}}=257
\end{aligned}
$$

## Multiplication

To multiply using powers of 10 , add the exponents.

## Example.

$$
\begin{aligned}
1000 \times 3721 & =10^{2} \times 37.21 \times 10^{2} \\
& =37.21 \times 10^{1+2} \\
& =37.21 \times 10^{2} \\
& =3,721,000
\end{aligned}
$$

## Example.

$$
\begin{aligned}
225 \times 0.00723 & =2.25 \times 10^{2} \times 7.23 \times 10^{-3} \\
& =2.25 \times 7.23 \times 10^{2-(-i-1)} \\
& =2.25 \times 7.23 \times 10^{-1} \\
& =16.2675 \times 10^{-1} \\
& =1.62675
\end{aligned}
$$

## Division

To divide using powers of 10 , subtract the exponent of the denominator from the exponent of the numerator.

## Example.

$$
\begin{aligned}
\frac{10^{4}}{10^{2}} & =10^{6-3} \\
& =10^{2} \\
& =100
\end{aligned}
$$

Example.

$$
\begin{aligned}
\frac{72,600}{0.002} & =\frac{72.6 \times 10^{3}}{2 \times 10^{-3}} \\
& =\frac{72.6 \times 10^{112}}{2} \\
& =36.3 \times 10^{4} \\
& =36,300,000
\end{aligned}
$$

## Combination Multiplication and Division

Problems involving a combination of multiplication and division can be solved using powers of 10 by multiplying and dividing, as called for, until the problem is completed.

## Example.

$$
\begin{aligned}
\frac{3900 \times 0.007 \times 420}{142.000 \times 0.00005} & =\frac{3.9 \times 10^{7} \times 7 \times 10^{-3} \times 4.2 \times 10^{2}}{1.42 \times 10^{5} \times 5 \times 10^{-5}} \\
& =\frac{3.9 \times 7 \times 4.2 \times 10^{:}}{1.42 \times 5} \\
& =\frac{114.66 \times 10^{2}}{7.1} \\
& =16.1493 \times 10: \\
& =1614.93
\end{aligned}
$$

## Reciprocal

To take the reciprocal of a number using powers of 10, first (if necessary) state the number so the decimal point precedes the first significant figure of the number. Then divide this number into 1 . The power of 10 in the answer will be the same value as in the original number, but it will have the opposite sign.

## Example.

$$
\begin{aligned}
\text { Reciprocal of } 400 & =\frac{1}{400} \\
\frac{1}{400} & =\frac{1}{0.4 \times 10^{3}} \\
& =2.5 \times 10^{3} \\
& =0.0025
\end{aligned}
$$

## Example.

$$
\text { Reciprocal of } \begin{aligned}
0.0025 & =\frac{1}{0.0025} \\
\frac{1}{0.0025} & =\frac{1}{0.25 \times 10^{2}} \\
& =4 \times 10^{2} \\
& =400
\end{aligned}
$$

## Square and Square Root

To square a number using powers of 10 , multiply the number by itself, and double the exponent.

## Example.

$$
\begin{aligned}
\left(7 \times 10^{3}\right)^{2} & =49 \times 10^{6} \\
& =49,000,000
\end{aligned}
$$

## Example.

$$
\begin{aligned}
\left(9.2 \times 10^{-4}\right)^{:} & =84.64 \times 10^{-4} \\
& =0.0000008464
\end{aligned}
$$

To extract the square root of a number using powers of 10 , do the opposite. (If the number is an odd power of 10 , first convert it to an even power of 10 .) Extract the square root of the number, and divide the power of 10 by 2 .

## Example.

$$
\begin{aligned}
\sqrt{36 \times 10^{10}} & =6 \times 10^{0} \\
& =600,000
\end{aligned}
$$

Example.

$$
\begin{aligned}
\overline{5.72 \times 10^{2}} & =\sqrt{57.2 \times 10^{2}} \\
& =7.56 \times 10 \\
& =75.6
\end{aligned}
$$

## ALGEBRAIC OPERATIONS

## Transposition of Terms

The following rules apply to the transposition of terms in algebraic equations:

If $A=B / C$, then:

$$
\begin{aligned}
B & =A C \\
C & =\frac{B}{A}
\end{aligned}
$$

If $A / B=C / D$, then:

$$
\begin{aligned}
& A=\frac{B C}{D} \\
& B=\frac{A D}{C} \\
& C=\frac{A D}{B} \\
& D=\frac{B C}{A}
\end{aligned}
$$

If $A+B=C$, then:

$$
\begin{aligned}
A & =C-B \\
A+B-C & =0
\end{aligned}
$$

If $A^{2}=1 /(D \sqrt{B C})$, then:

$$
\begin{aligned}
& A^{2}=\frac{1}{D^{2} B C} \\
& B=\frac{1}{D^{2} A^{2} C} \\
& C=\frac{1}{D^{2} A^{2} B} \\
& D=\frac{1}{A \sqrt{B C}}
\end{aligned}
$$

If $A=\sqrt{B^{2}+C^{2}}$, then:

$$
\begin{aligned}
A^{2} & =B^{2}+C^{2} \\
B & =\sqrt{A^{2}-C^{2}} \\
C & =\sqrt{A^{2}-B^{2}}
\end{aligned}
$$

## Laws of Exponents

A power of a fraction is equal to that power of the numerator divided by the same power of the denominator:

$$
\left(\frac{a}{b}\right)^{\prime}=\frac{a^{\wedge}}{b^{\prime}}
$$

The product of two powers of the same base is also a power of that base; the exponent of the product is equal to the sum of the exponents of the two factors:

$$
a^{x} \cdot a^{y}=a^{x-y}
$$

The quotient of two powers of the same base is also a power of that base; the exponent of the quotient is equal to the numerator exponent minus the denominator exponent:

$$
\frac{a^{\star}}{a^{\prime}}=a^{x-1}
$$

The power of a power of a base is also a power of that base; the exponent of the product is equal to the product of the exponents:

$$
\left(a^{x}\right)^{y}=a^{y}
$$

A negative exponent of a base is equal to the reciprocal of that base, with a positive exponent numerically equal to the original exponent:

$$
a^{-x}=\frac{1}{a^{x}}
$$

A fractional exponent indicates that the base should be raised to the power indicated by the numerator of the fraction; the root indicated by the denominator should then be extracted:

$$
a^{\vdots}=\sqrt[y]{a^{\prime}}
$$

A root of a fraction is equal to the identical root of the numerator divided by the identical root of the denominator:

$$
\sqrt{\frac{a}{b}}=\frac{\sqrt[{\sqrt{a}}]{\sqrt{b}}}{\sqrt{b}}
$$

A root of a product is equal to the product of the roots of the individual factors:

$$
\sqrt[{\sqrt{a b}}]{a b}=\sqrt[x]{a} \times \sqrt[x]{b}
$$

## Quadratic Equation

The general quadratic equation:

$$
a x^{2}+b x+c=0
$$

may be solved by:

$$
x=\frac{-b \pm \sqrt{b^{2}-4 a c}}{2 a}
$$

## GEOMETRIC FORMULAS

Triangle (Fig. 6-1):

$$
\operatorname{area}(A)=\frac{b h}{2}
$$



Fig. 6-1
Square (Fig. 6-2):

$$
\operatorname{area}(A)=b^{2}
$$



Fig. 6-2
Rectangle (Fig. 6-3):

$$
\operatorname{area}(A)=a b
$$



Fig. 6-3

Parallelogram (Fig. 6-4):


Fig. 6-4
Trapezoid (Fig. 6-5):

$$
\operatorname{area}(A)=\frac{h}{2}(a+b)
$$



Fig. 6-5
Trapezium (Fig. 6-6):
$\operatorname{area}(A)=\frac{1}{2}[b(H+h)+a h+c H]$


Fig. 6-6

Regular pentagon (Fig. 6-7):

$$
\operatorname{area}(A)=1.720 a^{2}
$$



Fig. 6-7
Regular hexagon (Fig. 6-8):


Fig. 6-8
Octagon (Fig. 6-9):

$$
\operatorname{area}(A)=4.828 a^{2}
$$



Fig. 6-9

Circle (Figs. 6-10 through 6-12):

$$
\text { circumference } \begin{aligned}
(C) & =2 \pi R \\
& =\pi D
\end{aligned}
$$

$$
\operatorname{area}(A)=\pi R^{2}
$$



Fig. 6-10

$$
\begin{aligned}
\operatorname{chord}(c) & =\sqrt{4\left(2 h R-h^{2}\right)} \\
\operatorname{area}(A) & =\pi R^{2}\left(\frac{\theta}{360}\right)-\left(\frac{c(R-h)}{2}\right)
\end{aligned}
$$



Fig. 6-11

$$
\begin{aligned}
\operatorname{area}(A) & =\frac{b R}{2} \\
& =\pi R^{2}\left(\frac{\theta}{360}\right)
\end{aligned}
$$



Fig. 6-12

Circular ring (Fig. 6-13):

$$
\text { area }(A)=\pi\left(R^{2}-r^{2}\right)=0.7854\left(D^{2}-d^{2}\right)
$$



Fig. 6-13

Ellipse (Fig. 6-14): circumference $(C)=$

$$
\pi(a+b)\left[\frac{64-3\left(\frac{b-a^{4}}{b+a}\right)}{64-16\left(\frac{b-a^{2}}{b+a}\right)}\right]
$$

$$
\operatorname{area}(A)=\pi a b
$$



Fig. 6-14

Sphere (Fig. 6-15):

$$
\text { area } \begin{aligned}
(A) & =4 R^{2} \\
& =\pi D^{2}
\end{aligned}
$$

volume $(V)=\frac{4}{3} \pi R^{3}$

$$
=\frac{1}{6} \pi D^{3}
$$



Fig. 6-15
Cube (Fig. 6-16):

$$
\operatorname{area}(A)=6 b^{2}
$$

volume $(V)=b^{3}$


Fig. 6-16

Rectangular solid (Fig. 6-17):

$$
\begin{aligned}
\text { area }(A) & =2(a b+b c+a c) \\
\text { volume }(V) & =a b c
\end{aligned}
$$



Fig. 6-17
Cone (Fig. 6-18):

$$
\begin{aligned}
\text { area }(A) & =\pi R S \\
& =\pi R \sqrt{R^{2}+h^{2}} \\
\text { volume }(V) & =\frac{\pi R^{2} h}{3} \\
& =1.047 R^{2} h \\
& =0.2618 D^{2} h
\end{aligned}
$$

Fig. 6-18

Cylinder (Fig. 6-19):
cylindrical surface $=\pi D h$

$$
\text { total surface }=2 \pi R(R+h)
$$

volume $(V)=\pi R^{2} h$
$=\frac{c^{2} h}{4 \pi}$


Fig. 6-19

Ring of rectangular cross section (Fig. 6-20):

$$
\text { volume } \begin{aligned}
(V) & =\frac{\pi c}{4}\left(D^{2}-d^{2}\right) \\
& =\left(\frac{D+d}{2}\right) \pi b c
\end{aligned}
$$



Fig. 6-20

Torus-ring of circular cross section (Fig. 6-21):

$$
\begin{aligned}
\text { total surface } & =4 \pi^{2} R r \\
& =\pi^{2} D d \\
\text { volume }(V) & =2 \pi R \times r^{2} \\
& =2.463 D \times d^{2}
\end{aligned}
$$



Fig. 6-21

## TRIGONOMETRIC FUNCTIONS

## Plane Trigonometry (Fig. 6-22)

In any right triangle, the values in Table 6-2 are valid if:
$a$ equals the acute angle formed by the hypotenuse and the altitude leg,
$b$ equals the acute angle formed by the hypotenuse and the base leg,
$A$ equals the side adjacent to $\angle b$ and opposite $\angle a$,
$B$ equals the side opposite $\angle b$ and adjacent to $\angle a$,
$C$ equals the hypotenuse.

TABLE 6-2
Trigonometric Formulas

| Known values | Formulas for unknown values of |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | A | B | $C$ | $\angle b$ | $\angle a$ |
| $A \& B$ | - | - | $\sqrt{A^{2}+B}$ | $\arctan \frac{B}{A}$ | $\arctan \frac{A}{B}$ |
| $A \& C$ | - | $\sqrt{C^{2}-A^{2}}$ | - | $\arccos \frac{A}{C}$ | $\arcsin \frac{A}{C}$ |
| $A \& \angle b$ | - | $A \tan <b$ | $\frac{A}{\cos \angle b}$ | - | $90^{\circ}-<b$ |
| $A \&<a$ | - | $\frac{A}{\tan \angle a}$ | $\frac{A}{\sin \angle a}$ | $90^{\circ}-\angle 4$ | - |
| $B \& C$ | $\sqrt{C^{2}-B^{2}}$ | - | - | $\arcsin \frac{B}{C}$ | $\arccos \frac{B}{C}$ |
| $B \& \angle b$ | $\frac{B}{\tan \angle b}$ | - | $-\frac{B}{\sin \angle b}$ | - | $90^{\circ}-\angle b$ |
| $B \&<a$ | $B \tan \angle a$ | - | $\frac{B}{\cos \angle a}$ | $90^{\circ}-\angle a$ | - |
| $C \&<b$ | $C \cos \angle b$ | $C \sin \angle b$ | - | - | $90^{\circ}-\angle b$ |
| $C \& \angle a$ | $C \sin \angle a$ | $C \cos \angle a$ | - | $90^{\circ}-\angle a$ | - |

[^8]

Fig. 6-22

## Table of Trigonometric Functions

Table 6-3 gives the natural sines, cosines, tangents, and cotangents of angles. To find these values for angles from $0^{\circ}$ to $45^{\circ}$, use
the headings at the top of the table and the degree listings in the left-hand column. For angles from $45^{\circ}$ to $90^{\circ}$, use the headings at the bottom of the table and the degree listings in the right-hand column.

Note. Read the degree listings in the right-hand column from bottom to top; thus, the $10^{\prime}$ listing directly above $89^{\circ}$ signifies $89^{\circ} 10^{\prime}$.

## BINARY NUMBERS

## Binary Digits

In the binary system of numbers, there are only two digits- 0 and 1 . All numbers

Handbook of Electronics Tables and Formulas

TABLE 6-3
Natural Trigonometric Functions

| Degrees | sin | cos | tan | cot |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ} 00^{\prime}$ | 0.0000 | 1.0000 | 0.0000 | $\infty$ | $90^{\circ}$ | $00^{\prime}$ |
| 10 | 0.0029 | 1.0000 | 0.0029 | 343.77 |  | 50 |
| 20 | 0.0058 | 1.0000 | 0.0058 | 171.89 |  | 40 |
| 30 | 0.0087 | 1.0000 | 0.0087 | 114.59 |  | 30 |
| 40 | 0.0116 | 0.9999 | 0.0116 | 85.940 |  | 20 |
| 50 | 0.0145 | 0.9999 | 0.0145 | 68.750 |  | 10 |
| $1^{\circ} 00{ }^{\prime}$ | 0.0175 | 0.9998 | 0.0175 | 57.290 | $89^{\circ}$ | $00{ }^{\prime}$ |
| 10 | 0.0204 | 0.9998 | 0.0204 | 49.104 |  | 50 |
| 20 | 0.0233 | 0.9997 | 0.0233 | 42.964 |  | 40 |
| 30 | 0.0262 | 0.9997 | 0.0262 | 38.188 |  | 30 |
| 40 | 0.0291 | 0.9996 | 0.0291 | 34.368 |  | 20 |
| 50 | 0.0320 | 0.9995 | 0.0320 | 31.242 |  | 10 |
| $2^{\circ} 00{ }^{\prime}$ | 0.0349 | 0.9994 | 0.0349 | 28.636 | $88^{\circ}$ | $00{ }^{\prime}$ |
| 10 | 0.0378 | 0.9993 | 0.0378 | 26.432 |  | 50 |
| 20 | 0.0407 | 0.9992 | 0.0407 | 24.542 |  | 40 |
| 30 | 0.0436 | 0.9990 | 0.0437 | 22.904 |  | 30 |
| 40 | 0.0465 | 0.9989 | 0.0466 | 21.470 |  | 20 |
| 50 | 0.0494 | 0.9988 | 0.0495 | 20.206 |  | 10 |
| $3^{\circ} 00^{\prime}$ | 0.0523 | 0.9986 | 0.0524 | 19.081 | $87^{\circ}$ | 00 ' |
| 10 | 0.0552 | 0.9985 | 0.0553 | 18.075 |  | 50 |
| 20 | 0.0581 | 0.9983 | 0.0582 | 17.169 |  | 40 |
| 30 | 0.0610 | 0.9981 | 0.0612 | 16.350 |  | 30 |
| 40 | 0.0640 | 0.9980 | 0.0641 | 15.605 |  | 20 |
| 50 | 0.0669 | 0.9978 | 0.0670 | 14.924 |  | 10 |
| $4^{\circ} 00{ }^{\prime}$ | 0.0698 | 0.9976 | 0.0699 | 14.301 | $86^{\circ}$ | $00^{\prime}$ |
| 10 | 0.0727 | 0.9974 | 0.0729 | 13.727 |  | 50 |
| 20 | 0.0756 | 0.9971 | 0.0758 | 13.197 |  | 40 |
| 30 | 0.0785 | 0.9969 | 0.0787 | 12.706 |  | 30 |
| 40 | 0.0814 | 0.9967 | 0.0816 | 12.251 |  | 20 |
| 50 | 0.0843 | 0.9964 | 0.0846 | 11.826 |  | 10 |
| $5^{\circ} 00^{\prime}$ | 0.0872 | 0.9962 | 0.0875 | 11.430 | $85^{\circ}$ | $00^{\prime}$ |
| 10 | 0.0901 | 0.9959 | 0.0904 | 11.059 |  | 50 |
| 20 | 0.0929 | 0.9957 | 0.0934 | 10.712 |  | 40 |
| 30 | 0.0958 | 0.9954 | 0.0963 | 10.385 |  | 30 |
| 40 | 0.0987 | 0.9951 | 0.0992 | 10.078 |  | 20 |
| 50 | 0.1016 | 0.9948 | 0.1022 | 9.7882 |  | 10 |
| $6^{\circ} 00{ }^{\prime}$ | 0.1045 | 0.9945 | 0.1051 | 9.5144 | $84^{\circ}$ | 00 ' |
| 10 | 0.1074 | 0.9942 | 0.1080 | 9.2553 |  | 50 |
| 20 | 0.1103 | 0.9939 | 0.1110 | 9.0098 |  | 40 |
| 30 | 0.1132 | 0.9936 | 0.1139 | 8.7769 |  | 30 |
| 40 | 0.1161 | 0.9932 | 0.1169 | 8.5555 |  | 20 |
| 50 | 0.1190 | 0.9929 | 0.1198 | 8.3450 |  | 10 |
| $7^{\circ} 00^{\prime}$ | 0.1219 | 0.9925 | 0.1228 | 8.1443 | $83^{\circ}$ | $00^{\prime}$ |
| 10 | 0.1248 | 0.9922 | 0.1257 | 7.9530 |  | 50 |
| 20 | 0.1276 | 0.9918 | 0.1287 | 7.7704 |  | 40 |
| 30 | 0.1305 | 0.9914 | 0.1317 | 7.5958 |  | 30 |
| 40 | 0.1334 | 0.9911 | 0.1346 | 7.4287 |  | 20 |
| 50 | 0.1363 | 0.9907 | 0.1376 | 7.2687 |  | 10 |

cot
$\tan$
Degrees

TABLE 6-3 Cont.
Natural Trigonometric Functions

| Degrees |  | $\sin$ | $\cos$ | tan | cot |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $8^{\circ}$ | $00^{\prime}$ | 0.1392 | 0.9903 | 0.1405 | 7.1154 | $82^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.1421 | 0.9899 | 0.1435 | 6.9682 |  | 50 |
|  | 20 | 0.1449 | 0.9894 | 0.1465 | 6.8269 |  | 40 |
|  | 30 | 0.1478 | 0.9890 | 0.1495 | 6.6912 |  | 30 |
|  | 40 | 0.1507 | 0.9886 | 0.1524 | 6.5606 |  | 20 |
|  | 50 | 0.1536 | 0.9881 | 0.1554 | 6.4348 |  | 10 |
| $9^{\circ}$ | $00^{\prime}$ | 0.1564 | 0.9877 | 0.1584 | 6.3138 | $81^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.1593 | 0.9872 | 0.1614 | 6.1970 |  | 50 |
|  | 20 | 0.1622 | 0.9868 | 0.1644 | 6.0844 |  | 40 |
|  | 30 | 0.1650 | 0.9863 | 0.1673 | 5.9758 |  | 30 |
|  | 40 | 0.1679 | 0.9858 | 0.1703 | 5.8708 |  | 20 |
|  | 50 | 0.1708 | 0.9853 | 0.1733 | 5.7694 |  | 10 |
| $10^{\circ}$ | $00^{\prime}$ | 0.1736 | 0.9848 | 0.1763 | 5.6713 | $80^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.1765 | 0.9843 | 0.1793 | 5.5764 |  | 50 |
|  | 20 | 0.1794 | 0.9838 | 0.1823 | 5.4845 |  | 40 |
|  | 30 | 0.1822 | 0.9833 | 0.1853 | 5.3955 |  | 30 |
|  | 40 | 0.1851 | 0.9827 | 0.1883 | 5.3093 |  | 20 |
|  | 50 | 0.1880 | 0.9822 | 0.1914 | 5.2257 |  | 10 |
| $11^{\circ}$ | $00^{\prime}$ | 0.1908 | 0.9816 | 0.1944 | 5.1446 | $79^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.1937 | 0.9811 | 0.1974 | 5.0658 |  | 50 |
|  | 20 | 0.1965 | 0.9805 | 0.2004 | 4.9894 |  | 40 |
|  | 30 | 0.1994 | 0.9799 | 0.2035 | 4.9152 |  | 30 |
|  | 40 | 0.2022 | 0.9793 | 0.2065 | 4.8430 |  | 20 |
|  | 50 | 0.2051 | 0.9787 | 0.2095 | 4.7729 |  | 10 |
| $12^{\circ}$ | $00^{\prime}$ | 0.2079 | 0.9781 | 0.2126 | 4.7046 | $78^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.2108 | 0.9775 | 0.2156 | 4.6382 |  | 50 |
|  | 20 | 0.2136 | 0.9769 | 0.2186 | 4.5736 |  | 40 |
|  | 30 | 0.2164 | 0.9763 | 0.2217 | 4.5107 |  | 30 |
|  | 40 | 0.2193 | 0.9757 | 0.2247 | 4.4494 |  | 20 |
|  | 50 | 0.2221 | 0.9750 | 0.2278 | 4.3897 |  | 10 |
| $13^{\circ}$ | $00^{\prime}$ | 0.2250 | 0.9744 | 0.2309 | 4.3315 | $77^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.2278 | 0.9737 | 0.2339 | 4.2747 |  | 50 |
|  | 20 | 0.2306 | 0.9730 | 0.2370 | 4.2193 |  | 40 |
|  | 30 | 0.2334 | 0.9724 | 0.2401 | 4.1653 |  | 30 |
|  | 40 | 0.2363 | 0.9717 | 0.2432 | 4.1126 |  | 20 |
|  | 50 | 0.2391 | 0.9710 | 0.2462 | 4.0611 |  | 10 |
| $14^{\circ}$ | $00^{\prime}$ | 0.2419 | 0.9703 | 0.2493 | 4.0108 | $76^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.2447 | 0.9696 | 0.2524 | 3.9617 |  | 50 |
|  | 20 | 0.2476 | 0.9689 | 0.2555 | 3.9136 |  | 40 |
|  | 30 | 0.2504 | 0.9681 | 0.2586 | 3.8667 |  | 30 |
|  | 40 | 0.2532 | 0.9674 | 0.2617 | 3.8208 |  | 20 |
|  | 50 | 0.2560 | 0.9667 | 0.2648 | 3.7760 |  | 10 |
| $15^{\circ}$ | $00^{\prime}$ | 0.2588 | 0.9659 | 0.2679 | 3.7321 | $75^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.2616 | 0.9652 | 0.2711 | 3.6891 |  | 50 |
|  | 20 | 0.2644 | 0.9644 | 0.2742 | 3.6470 |  | 40 |
|  | 30 | 0.2672 | 0.9636 | 0.2773 | 3.6059 |  | 30 |
|  | 40 | 0.2700 | 0.9628 | 0.2805 | 3.5656 |  | 20 |
|  | 50 | 0.2728 | 0.9621 | 0.2836 | 3.5261 |  | 10 |
|  |  | $\cos$ | $\sin$ | cot | $t a n$ | Deg | rees |

## Handbook of Electronics Tables and Formulas

TABLE 6-3 Cont.
Natural Trigonometric Functions

| Degrees |  | sin | cos | $t a n$ | cot |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $16^{\circ}$ | $00^{\prime}$ | 0.2756 | 0.9613 | 0.2867 | 3.4874 | $74^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.2784 | 0.9605 | 0.2899 | 3.4495 |  | 50 |
|  | 20 | 0.2812 | 0.9596 | 0.2931 | 3.4124 |  | 40 |
|  | 30 | 0.2840 | 0.9588 | 0.2962 | 3.3759 |  | 30 |
|  | 40 | 0.2868 | 0.9580 | 0.2994 | 3.3402 |  | 20 |
|  | 50 | 0.2896 | 0.9572 | 0.3026 | 3.3052 |  | 10 |
|  | $00^{\prime}$ | 0.2924 | 0.9563 | 0.3057 | 3.2709 | $73^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.2952 | 0.9555 | 0.3089 | 3.2371 |  | 50 |
|  | 20 | 0.2979 | 0.9546 | 0.3121 | 3.2041 |  | 40 |
|  | 30 | 0.3007 | 0.9537 | 0.3153 | 3.1716 |  | 30 |
|  | 40 | 0.3035 | 0.9528 | 0.3185 | 3.1397 |  | 20 |
|  | 50 | 0.3062 | 0.9520 | 0.3217 | 3.1084 |  | 10 |
| $18^{\circ}$ | $00^{\prime}$ | 0.3090 | 0.9511 | 0.3249 | 3.0777 | $72^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.3118 | 0.9502 | 0.3281 | 3.0475 |  | 50 |
|  | 20 | 0.3145 | 0.9492 | 0.3314 | 3.0178 |  | 40 |
|  | 30 | 0.3173 | 0.9483 | 0.3346 | 2.9887 |  | 30 |
|  | 40 | 0.3201 | 0.9474 | 0.3378 | 2.9600 |  | 20 |
|  | 50 | 0.3228 | 0.9465 | 0.3411 | 2.9319 |  | 10 |
| $19^{\circ}$ | $00^{\prime}$ | 0.3256 | 0.9455 | 0.3443 | 2.9042 | $71^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.3283 | 0.9446 | 0.3476 | 2.8770 |  | 50 |
|  | 20 | 0.3311 | 0.9436 | 0.3508 | 2.8502 |  | 40 |
|  | 30 | 0.3338 | 0.9426 | 0.3541 | 2.8239 |  | 30 |
|  | 40 | 0.3365 | 0.9417 | 0.3574 | 2.7980 |  | 20 |
|  | 50 | 0.3393 | 0.9407 | 0.3607 | 2.7725 |  | 10 |
| $20^{\circ}$ | $00^{\prime}$ | 0.3420 | 0.9397 | 0.3640 | 2.7475 | $70^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.3448 | 0.9387 | 0.3673 | 2.7228 |  | 50 |
|  | 20 | 0.3475 | 0.9377 | 0.3706 | 2.6985 |  | 40 |
|  | 30 | 0.3502 | 0.9367 | 0.3739 | 2.6746 |  | 30 |
|  | 40 | 0.3529 | 0.9356 | 0.3772 | 2.6511 |  | 20 |
|  | 50 | 0.3557 | 0.9346 | 0.3805 | 2.6279 |  | 10 |
| $21^{\circ}$ | $00{ }^{\prime}$ | 0.3584 | 0.9336 | 0.3839 | 2.6051 | $69^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.3611 | 0.9325 | 0.3872 | 2.5826 |  | 50 |
|  | 20 | 0.3638 | 0.9315 | 0.3906 | 2.5605 |  | 40 |
|  | 30 | 0.3665 | 0.9304 | 0.3939 | 2.5386 |  | 30 |
|  | 40 | 0.3692 | 0.9293 | 0.3973 | 2.5172 |  | 20 |
|  | 50 | 0.3719 | 0.9283 | 0.4006 | 2.4960 |  | 10 |
| $22^{\circ}$ | $00{ }^{\prime}$ | 0.3746 | 0.9272 | 0.4040 | 2.4751 | $68^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.3773 | 0.9261 | 0.4074 | 2.4545 |  | 50 |
|  | 20 | 0.3800 | 0.9250 | 0.4108 | 2.4342 |  | 40 |
|  | 30 | 0.3827 | 0.9239 | 0.4142 | 2.4142 |  | 30 |
|  | 40 | 0.3854 | 0.9228 | 0.4176 | 2.3945 |  | 20 |
|  | 50 | 0.3881 | 0.9216 | 0.4210 | 2.3750 |  | 10 |
| $23^{\circ}$ | $00{ }^{\prime}$ | 0.3907 | 0.9205 | 0.4245 | 2.3559 | $67^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.3934 | 0.9194 | 0.4279 | 2.3369 |  | 50 |
|  | 20 | 0.3961 | 0.9182 | 0.4314 | 2.3183 |  | 40 |
|  | 30 | 0.3987 | 0.9171 | 0.4348 | 2.2998 |  | 30 |
|  | 40 | 0.4014 | 0.9159 | 0.4383 | 2.2817 |  | 20 |
|  | 50 | 0.4041 | 0.9147 | 0.4417 | 2.2637 |  | 10 |
| cos |  |  | sin | cot | tan | Deg |  |

TABLE 6-3 Cont.
Natural Trigonometric Functions

| Degrees |  | $\sin$ | $\cos$ | $1 a n$ | cot |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $24^{\circ}$ | $00^{\prime}$ | 0.4067 | 0.9135 | 0.4452 | 2.2460 | $66^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.4094 | 0.9124 | 0.4487 | 2.2286 |  | 50 |
|  | 20 | 0.4120 | 0.9112 | 0.4522 | 2.2113 |  | 40 |
|  | 30 | 0.4147 | 0.9100 | 0.4557 | 2.1943 |  | 30 |
|  | 40 | 0.4173 | 0.9088 | 0.4592 | 2.1775 |  | 20 |
|  | 50 | 0.4200 | 0.9075 | 0.4628 | 2.1609 |  | 10 |
| $25^{\circ}$ | $00^{\prime}$ | 0.4226 | 0.9063 | 0.4663 | 2.1445 | $65^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.4253 | 0.9051 | 0.4699 | 2.1283 |  | 50 |
|  | 20 | 0.4279 | 0.9038 | 0.4734 | 2.1123 |  | 40 |
|  | 30 | 0.4305 | 0.9026 | 0.4770 | 2.0965 |  | 30 |
|  | 40 | 0.4331 | 0.9013 | 0.4806 | 2.0809 |  | 20 |
|  | 50 | 0.4358 | 0.9001 | 0.4841 | 2.0655 |  | 10 |
| $26^{\circ}$ | $00^{\prime}$ | 0.4384 | 0.8988 | 0.4877 | 2.0503 | $64^{\circ}$ | 00 |
|  | 10 | 0.4410 | 0.8975 | 0.4913 | 2.0353 |  | 50 |
|  | 20 | 0.4436 | 0.8962 | 0.4950 | 2.0204 |  | 40 |
|  | 30 | 0.4462 | 0.8949 | 0.4986 | 2.0057 |  | 30 |
|  | 40 | 0.4488 | 0.8936 | 0.5022 | 1.9912 |  | 20 |
|  | 50 | 0.4514 | 0.8923 | 0.5059 | 1.9768 |  | 10 |
| $27^{\circ}$ | $00^{\prime}$ | 0.4540 | 0.8910 | 0.5095 | 1.9626 | $63^{\circ}$ | $00{ }^{\prime}$ |
|  | 10 | 0.4566 | 0.8897 | 0.5132 | 1.9486 |  | 50 |
|  | 20 | 0.4592 | 0.8884 | 0.5169 | 1.9347 |  | 40 |
|  | 30 | 0.4617 | 0.8870 | 0.5206 | 1.9210 |  | 30 |
|  | 40 | 0.4643 | 0.8857 | 0.5243 | 1.9074 |  | 20 |
|  | 50 | 0.4669 | 0.8843 | 0.5280 | 1.8940 |  | 10 |
| $28^{\circ}$ | $00^{\prime}$ | 0.4695 | 0.8829 | 0.5317 | 1.8807 | $62^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.4720 | 0.8816 | 0.5354 | 1.8676 |  | 50 |
|  | 20 | 0.4746 | 0.8802 | 0.5392 | 1.8546 |  | 40 |
|  | 30 | 0.4772 | 0.8788 | 0.5430 | 1.8418 |  | 30 |
|  | 40 | 0.4797 | 0.8774 | 0.5467 | 1.8291 |  | 20 |
|  | 50 | 0.4823 | 0.8760 | 0.5505 | 1.8165 |  | 10 |
| $29^{\circ}$ | $00^{\prime}$ | 0.4848 | 0.8746 | 0.5543 | 1.8040 | $61^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.4874 | 0.8732 | 0.5581 | 1.7917 |  | 50 |
|  | 20 | 0.4899 | 0.8718 | 0.5619 | 1.7796 |  | 40 |
|  | 30 | 0.4924 | 0.8704 | 0.5658 | 1.7675 |  | 30 |
|  | 40 | 0.4950 | 0.8689 | 0.5696 | 1.7556 |  | 20 |
|  | 50 | 0.4975 | 0.8675 | 0.5735 | 1.7437 |  | 10 |
| $30^{\circ}$ | $00^{\prime}$ | 0.5000 | 0.8660 | 0.5774 | 1.7321 | $60^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.5025 | 0.8646 | 0.5812 | 1.7205 |  | 50 |
|  | 20 | 0.5050 | 0.8631 | 0.5851 | 1.7090 |  | 40 |
|  | 30 | 0.5075 | 0.8616 | 0.5890 | 1.6977 |  | 30 |
|  | 40 | 0.5100 | 0.8601 | 0.5930 | 1.6864 |  | 20 |
|  | 50 | 0.5125 | 0.8587 | 0.5969 | 1.6753 |  | 10 |
| $31^{\circ}$ | $00^{\prime}$ | 0.5150 | 0.8572 | 0.6009 | 1.6643 | $59^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.5175 | 0.8557 | 0.6048 | 1.6534 |  | 50 |
|  | 20 | 0.5200 | 0.8542 | 0.6088 | 1.6426 |  | 40 |
|  | 30 | 0.5225 | 0.8526 | 0.6128 | 1.6319 |  | 30 |
|  | 40 | 0.5250 | 0.8511 | 0.6168 | 1.6212 |  | 20 |
|  | 50 | 0.5275 | 0.8496 | 0.6208 | 1.6107 |  | 10 |


| $\cos$ | $\sin$ | $\cot$ | $\tan$ | Degrees |
| :---: | :---: | :---: | :---: | :---: |

Handbook of Electronics Tables and Formulas

TABLE 6-3 Cont.
Natural Trigonometric Functions

| Degrees |  | sin | $\boldsymbol{c o s}$ | $\tan$ | cot |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $32^{\circ}$ |  | 0.5299 | 0.8480 | 0.6249 | 1.6003 | $58^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.5324 | 0.8465 | 0.6289 | 1.5900 |  | 50 |
|  | 20 | 0.5348 | 0.8450 | 0.6330 | 1.5798 |  | 40 |
|  | 30 | 0.5373 | 0.8434 | 0.6371 | 1.5697 |  | 30 |
|  | 40 | 0.5398 | 0.8418 | 0.6412 | 1.5597 |  | 20 |
|  | 50 | 0.5422 | 0.8403 | 0.6453 | 1.5497 |  | 10 |
| $33^{\circ}$ | $00^{\prime}$ | 0.5446 | 0.8387 | 0.6494 | 1.5399 | $57^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.5471 | 0.8371 | 0.6536 | 1.5301 |  | 50 |
|  | 20 | 0.5495 | 0.8355 | 0.6577 | 1.5204 |  | 40 |
|  | 30 | 0.5519 | 0.8339 | 0.6619 | 1.5108 |  | 30 |
|  | 40 | 0.5544 | 0.8323 | 0.6661 | 1.5013 |  | 20 |
|  | 50 | 0.5568 | 0.8307 | 0.6703 | 1.4919 |  | 10 |
| $34^{\circ}$ | $00^{\prime}$ | 0.5592 | 0.8290 | 0.6745 | 1.4826 | $56^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.5616 | 0.8274 | 0.6787 | 1.4733 |  | 50 |
|  | 20 | 0.5640 | 0.8258 | 0.6830 | 1.4641 |  | 40 |
|  | 30 | 0.5664 | 0.8241 | 0.6873 | 1.4550 |  | 30 |
|  | 40 | 0.5688 | 0.8225 | 0.6916 | 1.4460 |  | 20 |
|  | 50 | 0.5712 | 0.8208 | 0.6959 | 1.4370 |  | 10 |
| $35^{\circ}$ | $00^{\prime}$ | 0.5736 | 0.8192 | 0.7002 | 1.4281 | $55^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.5760 | 0.8175 | 0.7046 | 1.4193 |  | 50 |
|  | 20 | 0.5783 | 0.8158 | 0.7089 | 1.4106 |  | 40 |
|  | 30 | 0.5807 | 0.8141 | 0.7133 | 1.4019 |  | 30 |
|  | 40 | 0.5831 | 0.8124 | 0.7177 | 1.3934 |  | 20 |
|  | 50 | 0.5854 | 0.8107 | 0.7221 | 1.3848 |  | 10 |
| $36^{\circ}$ | 00 ' | 0.5878 | 0.8090 | 0.7265 | 1.3764 | $54^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.5901 | 0.8073 | 0.7310 | 1.3680 |  | 50 |
|  | 20 | 0.5925 | 0.8056 | 0.7355 | 1.3597 |  | 40 |
|  | 30 | 0.5948 | 0.8039 | 0.7400 | 1.3514 |  | 30 |
|  | 40 | 0.5972 | 0.8021 | 0.7445 | 1.3432 |  | 20 |
|  | 50 | 0.5995 | 0.8004 | 0.7490 | 1.3351 |  | 10 |
| $37^{\circ}$ | $00^{\prime}$ | 0.6018 | 0.7986 | 0.7536 | 1.3270 | $53{ }^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.6041 | 0.7969 | 0.7581 | 1.3190 |  | 50 |
|  | 20 | 0.6065 | 0.7951 | 0.7627 | 1.3111 |  | 40 |
|  | 30 | 0.6088 | 0.7934 | 0.7673 | 1.3032 |  | 30 |
|  | 40 | 0.6111 | 0.7916 | 0.7720 | 1.2954 |  | 20 |
|  | 50 | 0.6134 | 0.7898 | 0.7766 | 1.2876 |  | 10 |
| $38^{\circ}$ | 00' | 0.6157 | 0.7880 | 0.7813 | 1.2799 | $52^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.6180 | 0.7862 | 0.7860 | 1.2723 |  | 50 |
|  | 20 | 0.6202 | 0.7844 | 0.7907 | 1.2647 |  | 40 |
|  | 30 | 0.6225 | 0.7826 | 0.7954 | 1.2572 |  | 30 |
|  | 40 | 0.6248 | 0.7808 | 0.8002 | 1.2497 |  | 20 |
|  | 50 | 0.6271 | 0.7790 | 0.8050 | 1.2423 |  | 10 |
| $39^{\circ}$ | $00^{\prime}$ | 0.6293 | 0.7771 | 0.8098 | 1.2349 | $51{ }^{\circ}$ | $00^{\prime}$ |
|  | 10 | 0.6316 | 0.7753 | 0.8146 | 1.2276 |  | 50 |
|  | 20 | 0.6338 | 0.7735 | 0.8195 | 1.2203 |  | 40 |
|  | 30 | 0.6361 | 0.7716 | 0.8243 | 1.2131 |  | 30 |
|  | 40 | 0.6383 | 0.7698 | 0.8292 | 1.2059 |  | 20 |
|  | 50 | 0.6406 | 0.7679 | 0.8342 | 1.1988 |  | 10 |


| $\cos$ | $\sin$ | $\cot$ | $\tan$ | Degrees |
| :--- | :--- | :--- | :--- | :--- |

TABLE 6-3 Cont.
Natural Trigonometric Functions

| Degrees | sin | cos | $t a n$ | cot |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $40^{\circ}$ | 0.6428 | 0.7660 | 0.8391 | 1.1918 | $50^{\circ} 00^{\prime}$ |
|  | 0.6450 | 0.7642 | 0.8441 | 1.1847 | 50 |
|  | 0.6472 | 0.7623 | 0.8491 | 1.1778 | 40 |
|  | 0.6494 | 0.7604 | 0.8541 | 1.1708 | 30 |
|  | 0.6517 | 0.7585 | 0.8591 | 1.1640 | 20 |
|  | 0.6539 | 0.7566 | 0.8642 | 1.1571 | 10 |
| $41^{\circ}$ | 0.6561 | 0.7547 | 0.8693 | 1.1504 | $49^{\circ} 00{ }^{\prime}$ |
|  | 0.6583 | 0.7528 | 0.8744 | 1.1436 | 50 |
|  | 0.6604 | 0.7509 | 0.8796 | 1.1369 | 40 |
|  | 0.6626 | 0.7490 | 0.8847 | 1.1303 | 30 |
|  | 0.6648 | 0.7470 | 0.8899 | 1.1237 | 20 |
|  | 0.6670 | 0.7451 | 0.8952 | 1.1171 | 10 |
| $42^{\circ}$ | 0.6691 | 0.7431 | 0.9004 | 1.1106 | $48^{\circ} 00{ }^{\prime}$ |
|  | 0.6713 | 0.7412 | 0.9057 | 1.1041 | 50 |
|  | 0.6734 | 0.7392 | 0.9110 | 1.0977 | 40 |
|  | 0.6756 | 0.7373 | 0.9163 | 1.0913 | 30 |
|  | 0.6777 | 0.7353 | 0.9217 | 1.0850 | 20 |
|  | 0.6799 | 0.7333 | 0.9271 | 1.0786 | 10 |
| $43^{\circ}$ | 0.6820 | 0.7314 | 0.9325 | 1.0724 | $47^{\circ} 00{ }^{\prime}$ |
|  | 0.6841 | 0.7294 | 0.9380 | 1.0661 | 50 |
|  | 0.6862 | 0.7274 | 0.9435 | 1.0599 | 40 |
|  | 0.6884 | 0.7254 | 0.9490 | 1.0538 | 30 |
|  | 0.6905 | 0.7234 | 0.9545 | 1.0477 | 20 |
|  | 0.6926 | 0.7214 | 0.9601 | 1.0416 | 10 |
| $44^{\circ}$ | 0.6947 | 0.7193 | 0.9657 | 1.0355 | $46^{\circ} 00{ }^{\prime}$ |
|  | 0.6967 | 0.7173 | 0.9713 | 1.0295 | 50 |
|  | 0.6988 | 0.7163 | 0.9770 | 1.0235 | 40 |
|  | 0.7009 | 0.7133 | 0.9827 | 1.0176 | 30 |
|  | 0.7030 | 0.7112 | 0.9884 | 1.0117 | 20 |
|  | 0.7050 | 0.7092 | 0.9942 | 1.0058 | 10 |
| $45^{\circ} 00{ }^{\prime}$ | 0.7071 | 0.7071 | 1.0000 | 1.0000 | $45^{\circ} 00{ }^{\prime}$ |
|  | cos | sin | cot | tan | Degrees |

are written as successive powers of 2 . Actually, in the decimal system, all numbers are written as successive powers of 10 .

Example. Decimal 3487 is actually:

$$
\begin{aligned}
& 3 \times 10^{3}=3000 \\
& 4 \times 10^{2}=400 \\
& 8 \times 10^{2}=80 \\
& 7 \times 10^{4}= \\
& =\frac{7}{3487}
\end{aligned}
$$

With binary numbers, a like system is used except the base (radix) is 2 instead of
10. For example, the binary numbers corresponding to decimal numbers 0 through 10 are $0,1,10,11,100,101,110,111,1000$, 1001, 1010. Each number is written as a succession of powers of 2 .

Example. Binary 1010 actually means:

$$
\begin{array}{r}
1 \times 2^{3}= \\
+1 \times 2^{\prime}=\frac{2}{10}
\end{array}
$$

The powers of 2 , from 0 to 20, are given in Table 6-4. Thus, to write a number above decimal $1,048,056$ using binary numbers requires a minimum of 21 digits!

TABLE 6-4
Powers of 2

| Power | Decimal | Power | Decimal | Power | Decimal |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $2{ }^{\prime \prime}$ | 1 | 2 | 128 | $2^{14}$ | 16,384 |
| 2 | 2 | $2^{\text {s }}$ | 256 | $2^{1 /}$ | 32,768 |
| 2: | 4 | $2^{\prime \prime}$ | 512 | $2^{16}$ | 65,536 |
| $2{ }^{\text {3 }}$ | 8 | $2^{\text {III }}$ | 1024 | $2^{17}$ | 131,072 |
| 24 | 16 | $2^{11}$ | 2048 | $2^{1 \times}$ | 262,144 |
| 2 ' | 32 | $2^{12}$ | 4096 | $2^{11}$ | 524,288 |
| $2^{\text {b }}$ | 64 | $2^{17}$ | 8192 | $2{ }^{\text {² }}$ | 1,048,576 |

Binary numbers are also arranged into widely used codes such as the Excess-3 and Gray Codes shown in Tables 6-5 and 6-6, respectively. (See also the discussion of the ASCII Code in Chapter 7.)

TABLE 6-5
Excess-3 Code

| Decimal | Binary code |
| :---: | :---: |
| 0 | 0011 |
| 1 | 0100 |
| 2 | 0101 |
| 3 | 0110 |
| 4 | 0111 |
| 5 | 1000 |
| 6 | 1001 |
| 7 | 1010 |
| 8 | 1011 |
| 9 | 1100 |

## Conversion

To convert from binary to decimal or from decimal to binary, you could use Table $6-4$ and compute the equivalent in the other numbering system. However, there are simpler methods. To convert from decimal to binary, successively divide the decimal num-

TABLE 6-6
Gray Code

| Decimal | Gray code <br> $a_{1} a_{2} a_{1} a_{11}$ |
| :---: | :---: |
| 0 | 0000 |
| 1 | 0001 |
| 2 | 0011 |
| 3 | 0010 |
| 4 | 0110 |
| 5 | 0111 |
| 6 | 0101 |
| 7 | 0100 |
| 8 | 1100 |
| 9 | 1101 |
| 10 | 1111 |
| 11 | 1110 |
| 12 | 1010 |
| 13 | 1011 |
| 14 | 1001 |
| 15 | 1000 |

ber by 2 . Write down a 1 if there is a remainder and a 0 if not, until the division gives a 0 .

Example. To covert decimal 22 to binary.

$$
\begin{aligned}
\frac{2}{2} \sqrt[22]{11} & R=0 \\
2 \sqrt{5} & R=1 \\
2 \sqrt{2} & R=1 \\
2 \sqrt{1} & R=0 \\
\overline{0} & R=1
\end{aligned}
$$

The least significant figure is at the top; thus, the binary number corresponding to decimal 22 is 10110.

To convert from binary to decimal, take the first binary digit, double it, and add your answer to the second digit. Write this sum under the second digit. Then double this number, add it to the third digit, and write the sum under the third digit. Con-
tinue this process up to and including the last digit, as follows:

| 1 | 0 | 1 | 1 | 0 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 5 | 11 | 22 | 45 |

The number under the last digit (45) is the decimal equivalent of binary 101101.

## Addition

Binary addition has only four rules:

$$
\begin{array}{cccc}
0 & 0 & 1 & 1 \\
0 & \frac{0}{1} & \frac{1}{2} & \frac{1}{10} \\
\hline 0 & 1 & 1 & 1
\end{array}
$$

Following these rules, any binary number can be added.

## Example.

$$
\begin{array}{r}
1011 \\
\hline 110 \\
\hline 10001
\end{array}
$$

To simplify the carry when $1+1=10$, place the carry under the next digit. Then add the partial total and the carries, as follows:

$$
\begin{array}{r}
111101 \\
10110 \\
\hline 101011 \\
\frac{11}{1010011}
\end{array}
$$

## Subtraction

Binary numbers can be subtracted directly, as follows:

However, it is simpler to complement the subtracted number and add. In the binary system, a number is complemented by merely changing all 0 's to 1 's and all 1's to 0 's and adding 1 to the final digit.

## Example.

1111

-0111 complemented | 1111 |
| ---: |
| +1001 |

Answer. The first digit in the answer is disregarded. Hence, the answer is 1000 (decimal 8), the same as before.

## Multiplication

Binary multiplication is similar to decimal multiplication. All products are the same as in decimal multiplication. That is:

$$
\begin{aligned}
& 0 \times 0=0 \\
& 1 \times 0=0 \\
& 1 \times 1=1
\end{aligned}
$$

Example. To multiply 1011 by 101 :

$$
\begin{array}{r}
1011 \\
0101 \\
\hline 1011 \\
0000 \\
\frac{1011}{110111}
\end{array}
$$

## Division

Binary division is similar to decimal division.

Example. To divide 1101001 by 101:

$$
\begin{aligned}
& 1 0 1 \longdiv { 1 0 1 0 1 } \\
& \frac{101}{101001} \\
& \frac{101}{101} \\
& 101
\end{aligned}
$$

## Handling Negative Remainders

In the preceding example of binary division, there was no 0 generated in the quotient. That is, there were no remainders smaller than the divisor. The following example shows what steps must be taken when a 0 is generated.

Example. Dividing 45 by 9 :

$$
\begin{gathered}
\frac{101}{1 0 0 1 \longdiv { 1 0 1 1 0 1 }} \\
\frac{1001}{1001} \\
\underline{1001}
\end{gathered}
$$

Bringing down the next digit resulted in a remainder smaller than the divisor. Therefore a 0 was placed in the quotient. When the next digit was transferred down, the remainder was larger than the quotient.

The successive-subtraction method used by a computer follows:

|  |  | Quotient |
| :--- | :---: | :---: |
| Subtract | $\underline{101101}$ |  |
|  | $\underline{100100}$ |  |
| Shift | $\underline{001001}$ | 1 |
|  | $\underline{100100}$ |  |
| Restore-add | $\underline{101110}$ | 0 |
|  | $\underline{100100}$ |  |
| Shift | $\underline{010010}$ |  |
|  | $\underline{100100}$ | 1 |

After the first subtraction, the number is positive. This positive remainder is shifted left but is still smaller than the divisor. Subtracting now would result in a negative number. A computer has no way of detecting
that the remainder is larger than the divisor until the subtraction operation is performed. One indication is that the highest order will require a borrow, or what is termed an overdraw.

When a subtraction causes a negative number, the computer must restore the remainder to the original value before the next dividend is used. This is done by adding the divisor to the remainder prior to the next shift operation.

## Binary Coded Decimal

Various codes based on the binary 1 and 0 concept have evolved to meet the needs of digital equipment operation. The binary coded decimal (BCD) is widely used. Here, four bits are used to represent each digit of the decimal number. Each digit position has a definite value or weight in the order 8,4, 2,1 and each four digit combination in the $B C D$ represents one digit of a decimal number as follows:

| Decimal | BCD |
| :---: | :---: |
| 0 | 0000 |
| 1 | 0001 |
| 2 | 0010 |
| 3 | 0011 |
| 4 | 0100 |
| 5 | 0101 |
| 6 | 0110 |
| 7 | 0111 |
| 8 | 1000 |
| 9 | 1001 |

For larger decimal numbers, where two or more decimal digits are needed, additional four-bit BCD combinations are used. For example, decimal 25 in BCD is 0010 0101 and decimal 372 in BCD is 00110111 0010.

## OTHER NUMBER SYSTEMS

Octal is a numbering system with a base of 8 . Since 8 is a power of 2 , conversion between the octal and binary systems is an easy operation. Thus, the digits 0 through 7 are used as follows:

| Decimal | Octal equivalent |
| :---: | :---: |
| 0 | 0 |
| 1 | 1 |
| 2 | 2 |
| 3 | 3 |
| 4 | 4 |
| 5 | 5 |
| 6 | 6 |
| 7 | 7 |
| 8 | 10 |

Thus, 21 in octal is the equivalent of decimal 17 and binary 10001 .

Hexadecimal numbers (often abbreviated hex) also find wide usage. The hexadecimal system has 16 as its base. The conventional numbers are used from 0 through 9 and the letters A through F for decimal 10 through 15. Thus:

| Decimal | Hexadecimal <br> equivalent |
| :---: | :---: |
| 0 | 0 |
| 1 | 1 |
| 2 | 2 |
| 3 | 3 |
| 4 | 4 |
| 5 | 5 |
| 6 | 6 |
| 7 | 7 |
| 8 | 8 |
| 9 | 9 |
| 10 | A |
| 11 | B |
| 12 | C |
| 13 | D |
| 14 | E |
| 15 | F |
| 16 | 10 |

Thus, 21 in hexadecimal is the equivalent of decimal 33 and binary 100001 . Likewise 1 A in hexadecimal is the equivalent of decimal 26.

## FUNDAMENTALS OF BOOLEAN ALGEBRA

Boolean algebra is based on symbolic logic, which requires that a statement be either true or false-it can be nothing else. The symbols $A, B$, and $C$ are used to designate various conditions, which may be characterized by statements. Two logical connectives-AND and OR-express relationships between two statements.

Two or more statements connected by the word "or" are considered to form a single true statement if at least one of the original statements is true. Similarly, if two parallel switches are connected in a circuit, the circuit is considered to be closed if at least one of the switches is closed. Thus, or is the logical equivalent of a parallel switch circuit. It is symbolized by a plus sign.

Two or more statements connected by the word "and" are considered to form a single true statement if all of the original statements are true. Similarly, if two series switches are connected in a circuit, the circuit is considered to be closed if all of the switches are closed. Thus, and is the logical equivalent of a series switch circuit. And is symbolized by a multiplication sign (.) or no sign at all.

Given any statement, the opposite or contradiction of that statement can be formed. The contradiction of any statement $A$ is called the negation of $A$. If $A$ is true, then the negation of A is false, and vice versa. Similarly, if a switch has two positions, then the open position may be considered the opposite or negation of the closed

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TABLE 6-7

## Basic Rules of Symbolic Logic

| Symbol | Logic | Switch | Meaning |
| :---: | :---: | :--- | :--- |
| 1 | true | closed | The statement is true. <br> The circuit is closed. |
| 0 | false | open | The statement is false. <br> The circuit is open. |
| + | series | $A$ and $B$ | $A$ is in series with $B$. |

position. Negation is indicated by a superior bar (') or prime (').

A true statement, and hence a closed circuit, is generally said to have a truth value of 1. Conversely, a false statement, and hence

TABLE 6-8
Summary of Logical Statements

| Logic | Meaning | Circuit |
| :---: | :--- | :--- |
| $0 \cdot 0=0$ | An open in series <br> with an open is open. |  |
| $0 \cdot 1=0$ | An open in series <br> with a closed is open. |  |
| $1 \cdot 1=1$ | A closed in series <br> with a closed is <br> closed. |  |
| $0+1=1$ | An open in parallel <br> with an open in parallel <br> withesed | A closed in parallel <br> with a closed is <br> llosed. |

an open circuit, is generally said to have a truth value of 0 . Applying the AND and OR (. and + ) relations to the truth values ( 0 and 1) yields the multiplication and addition tables of binary arithmetic.

The various symbols are given in Table 6-7. Table 6-8 summarizes the various logical statements, explains their meanings, and shows the equivalent switch circuits for the statements.

A further explanation of these Boolean algebra concepts is given by Figs. 6-23 through 6-26, which shown AND, OR, NAND, and nor gates. At $A$ in each figure, the symbol for the gate is given; at $B$, the gate is represented by an appropriate electrical circuit; and a truth table for each circuit is given at $C$.

The and gate is shown as having two inputs $A$ and $B$ and an output $C$. The gate is not limited to two inputs; any number could be used. Regardless of the number, they would all be shown in series in the circuit of $B$ (Fig. 6-23).

In the and truth tables, a 0 represents a false statement, or an open switch in the circuit. A 1 represents a true statement, or a closed switch. The truth table for the and

Fig. 6-23



| $A$ | $B$ | $F$ |  |
| :---: | :---: | :---: | :---: |
| 0 | 0 | 0 |  |
| 0 | 1 | 0 |  |
| 1 | 0 | 0 |  |
| 1 | 1 | 1 |  |
| AND Gate |  |  |  |

Fig. 6-24
Input $\longrightarrow O-O$ Output

| $A$ | $B$ | $F$ |  |
| :--- | :--- | :--- | :---: |
| 0 | 0 | 0 |  |
| 0 | 1 | 1 |  |
| 1 | 0 | 1 |  |
| 1 | 1 | 1 |  |
| OR Gate |  |  |  |

gate shows, then, that an output is obtained in only one case: when both $A$ and $B$ are 1 . If either $A$ or $B$, or both, are 0 , then the output is 0 , as shown by the first three lines of the truth table.

The or gate (Fig. 6-24) is represented by switches in parallel. The circuit shows that an output is obtained when one or the other, or both, switches are closed. These examples are represented by the last three lines in the truth table. If both switches are open (first line of the table), no output is obtained.

In logic circuits, a statement can be negated or contradicted by any device that inverts the input by $180^{\circ}$. This means that an input that would normally produce an output produces no output, and vice versa. In the gate circuits, this would be represented by a closed switch in place of an open one,
or by an open switch in place of a closed one. The negation of an and gate is a Nand gate (short for NOT AND). A nand gate is represented in Fig. 6-25. Notice in the circuit that switches are now shown in parallel, instead of in series as they were for the and gate. Also, do not forget that a 0 in the truth table now produces a closed switch and a 1 produces an open switch.

The output column for the and gate is the direct opposite or contradiction of the output column for the NAND gate, and vice versa. The input that produced an output with the and gate now produces no output with the NAND gate, and, conversely, the inputs that produced no output with the and gate now produce outputs with the Nand gate.

Figure 6-26 shows a NOR gate, a circuit, and a truth table. Since this is a contradic-

Fig. 6-25



| A | B | F |  |
| :---: | :---: | :---: | :---: |
| 0 | 0 | 1 |  |
| 0 | 1 | 1 |  |
| 1 | 0 | 1 |  |
| 1 | 1 | 0 |  |
| NAND Gate |  |  |  |

Fig. 6-26


| A | B | F |  |
| :---: | :---: | :---: | :---: |
| 0 | 0 | 1 |  |
| 0 | 1 | 0 |  |
| 1 | 0 | 0 |  |
| 1 | 1 | 0 |  |
| NOR Gate |  |  |  |

tion of the or gate, the circuit shows the switches in series instead of in parallel. A 0 input produces a closed switch, and a 1 in put produces an open switch. The output column is the direct opposite, or contradiction, of the output column for the or gate.

## COMMON LOGARITHMS

The logarithm of a quantity is the power to which a given number (base) must be raised in order to equal that quantity. Thus, any number may be used as the base. The most common system is the base 10. Logarithms with the base 10 are known as common, or Briggs, logarithms; they are written $\log _{11}$, or simply log. When the base is omitted, the base 10 is understood.

A common logarithm of a given number is the number which, when applied to the number 10 as an exponent, will produce the given number. Thus, 2 is the common logarithm of 100 , since $10^{\circ}$ equals $100 ; 3$ is the logarithm of 1000 , since $10^{3}$ equals 1000 . From this we can see that the logarithm of any number except a whole number power of 10 consists of a whole number and a decimal fraction.

## Characteristic of a Logarithm

The whole-number portion of a logarithm is called the characteristic. The characteristic of a whole number, or of a whole number and a fraction, has a positive value equal to one less than the number of digits preceding the decimal point. The characteristic of a decimal fraction has a negative value equal to one more than the number of zeros immediately following the decimal point. The characteristics of numbers between 0.0001 and 99,999 are:

| Numbers | Characteristic |
| :---: | :---: |
| $0.0001-0.0009$ | -4 |
| $0.001-0.009$ | -3 |
| $0.01-0.09$ | -2 |
| $0.1-0.9$ | -1 |
| $1-9$ | 0 |
| $10-99$ | 1 |
| $100-999$ | 2 |
| $1000-9999$ | 3 |
| $10,000-99,999$ | 4 |

## Use of Logarithm Table

The mantissa, or decimal-fracton portion, of a logarithm is obtained from Table $6-9$. To find the mantissa for the logarithm of any number, locate the first two figures of the number in the left-hand column ( $N$ ); then, in the column under the third figure of the number, the mantissa for that number will be found.

Example. To find the logarithm of 6673 , first locate 66 in the left-hand column ( $N$ ); then follow across to the column numbered 7. The mantissa for 667 (8241) is located at this point. The characteristic for the logarithm of 6673 is 3 . Therefore, the logarithm of 6670 is 3.8241 .

For most computations, greater accuracy will not be required. If accuracy to four places is desired, the columns labeled "Proportional parts" may be used. These columns list the numbers to be added to the logarithm to obtain four-place accuracy. The foregoing example demonstrated how to obtain the logarithm for 6670 (3.8241), not the logarithm for 6673. Using the "Proportional parts" column to find the proportional part for 3 , which is 2 , the logarithm for 6673 is 3.8241 plus 0.0002 , or 3.8243 .

The mantissa of a logarithm is usually positive, whereas a characteristic may be either positive or negative. The total logarithm is the sum of the mantissa and the

TABLE 6-9
Common Logarithms

| $N$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional parts |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | I | 2 | J | 4 | 5 | 6 | 7 | 8 | 9 |
| 10 | 0000 | 0043 | 0086 | 0128 | 0170 | 0212 | 0253 | 0294 | 0334 | 0374 | 4 | 8 | 12 | 17 | 21 | 25 | 29 | 33 | 37 |
| 11 | 0414 | 0453 | 0492 | 0531 | 0569 | 0607 | 0645 | 0682 | 0719 | 0755 | 4 | 8 | 11 | 15 | 19 | 23 | 26 | 30 | 34 |
| 12 | 0792 | 0828 | 0864 | 0899 | 0934 | 0969 | 1004 | 1038 | 1072 | 1106 | 3 | 7 | 10 | 14 | 17 | 21 | 24 | 28 | 31 |
| 13 | 1139 | 1173 | 1206 | 1239 | 1271 | 1303 | 1335 | 1367 | 1399 | 1430 | 3 | 6 | 10 | 13 | 16 | 19 | 23 | 26 | 29 |
| 14 | 1461 | 1492 | 1523 | 1553 | 1584 | 1614 | 1644 | 1673 | 1703 | 1732 | 3 | 6 | 9 | 12 | 15 | 18 | 21 | 24 | 27 |
| 15 | 1761 | 1790 | 1818 | 1847 | 1875 | 1903 | 1931 | 1959 | 1987 | 2014 | 3 | 6 | 8 | 11 | 14 | 17 | 20 | 22 | 25 |
| 16 | 2041 | 2068 | 2095 | 2122 | 2148 | 2175 | 2201 | 2227 | 2253 | 2279 | 3 | 5 | 8 | 11 | 13 | 16 | 18 | 21 | 24 |
| 17 | 2304 | 2330 | 2355 | 2380 | 2405 | 2430 | 2455 | 2480 | 2504 | 2529 | 2 | 5 | 7 | 10 | 12 | 15 | 17 | 20 | 22 |
| 18 | 2553 | 2577 | 2601 | 2625 | 2648 | 2672 | 2695 | 2718 | 2742 | 2765 | 2 | 5 | 7 | 9 | 12 | 14 | 16 | 19 | 21 |
| 19 | 2788 | 2810 | 2833 | 2856 | 2878 | 2900 | 2923 | 2945 | 2967 | 2989 | 2 | 4 | 7 | 9 | 11 | 13 | 16 | 18 | 20 |
| 20 | 3010 | 3032 | 3054 | 3075 | 3096 | 3118 | 3139 | 3160 | 3181 | 3201 | 2 | 4 | 6 | 8 | 11 | 13 | 15 | 17 | 19 |
| 21 | 3222 | 3243 | 3263 | 3284 | 3304 | 3324 | 3345 | 3365 | 3385 | 3404 | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 |
| 22 | 3424 | 3444 | 3464 | 3483 | 3502 | 3522 | 3541 | 3560 | 3579 | 3598 | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 15 | 17 |
| 23 | 3617 | 3636 | 3655 | 3674 | 3692 | 3711 | 3729 | 3747 | 3766 | 3784 | 2 | 4 | 6 | 7 | 9 | 11 | 13 | 15 | 17 |
| 24 | 3802 | 3820 | 3838 | 3856 | 3874 | 3892 | 3909 | 3927 | 3945 | 3962 | 2 | 4 | 5 | 7 | 9 | 11 | 12 | 14 | 16 |
| 25 | 3979 | 3997 | 4014 | 4031 | 4048 | 4065 | 4082 | 4099 | 4116 | 4133 | 2 | 3 | 5 | 7 | 9 | 1) | 12 | 14 | 15 |
| 26 | 4150 | 4166 | 4183 | 4200 | 4216 | 4232 | 4249 | 4265 | 4281 | 4298 | 2 | 3 | 5 | 7 | 8 | 10 | 11 | 13 | 15 |
| 27 | 4314 | 4330 | 4346 | 4362 | 4378 | 4393 | 4409 | 4425 | 4440 | 4456 | 2 | 3 | 5 | 6 | 8 | 9 | 11 | 13 | 14 |
| 28 | 4472 | 4487 | 4502 | 4518 | 4533 | 4548 | 4564 | 4579 | 4594 | 4609 | 2 | 3 | 5 | 6 | 8 | 9 | 11 | 12 | 14 |
| 29 | 4624 | 4639 | 4654 | 4669 | 4683 | 4698 | 4713 | 4728 | 4742 | 4757 | 1 | 3 | 4 | 6 | 7 | 9 | 10 | 12 | 13 |
| 30 | 4771 | 4786 | 4800 | 4814 | 4829 | 4843 | 4857 | 4871 | 4886 | 4900 | 1 | 3 | 4 | 6 | 7 | 8 | 10 | 11 | 13 |
| 31 | 4914 | 4928 | 4942 | 4955 | 4969 | 4983 | 4997 | 5011 | 5024 | 5038 | 1 | 3 | 4 | 6 | 7 | 8 | 10 | 11 | 12 |
| 32 | 5051 | 5065 | 5079 | 5092 | 5105 | 5119 | 5132 | 5145 | 5159 | 5172 | 1 | 3 |  | 5 | 7 | 8 | 9 | 11 | 12 |
| 33 | 5185 | 5198 | 5211 | 5224 | 5237 | 5250 | 5263 | 5276 | 5289 | 5302 | 1 | 3 | 4 | 5 | 6 | 8 | 9 | 10 | 12 |
| 34 | 5315 | 5328 | 5340 | 5353 | 5366 | 5378 | 5391 | 5403 | 5416 | 5428 | 1 | 3 | 4 | 5 | 6 | 8 | 9 | 10 | 11 |
| 35 | 5441 | 5453 | 5465 | 5478 | 5490 | 5502 | 5514 | 5527 | 5539 | 5551 | 1 | 2 | 4 | 5 | 6 | 7 | 9 | 10 | 11 |
| 36 | 5563 | 5575 | 5587 | 5599 | 5611 | 5623 | 5635 | 5647 | 5658 | 5670 | , | 2 | 4 | 5 | 6 | 7 | 8 | 10 | 11 |
| 37 | 5682 | 5694 | 5705 | 5717 | 5729 | 5740 | 5752 | 5763 | 5775 | 5786 | 1 | 2 | 3 | 5 | 6 | 7 | 8 | 9 | 10 |
| 38 | 5798 | 5809 | 5821 | 5832 | 5843 | 5855 | 5866 | 5877 | 5888 | 5899 | 1 | 2 | 3 | 5 | 6 | 7 | 8 | 9 | 10 |
| 39 | 5911 | 5922 | 5933 | 5944 | 5955 | 5966 | 5977 | 5988 | 5999 | 6010 | 1 | 2 | 3 | 4 | 5 | 7 | 8 | 9 | 10 |
| 40 | 6021 | 6031 | 6042 | 6053 | 6064 | 6075 | 6085 | 6096 | 6107 | 6117 | 1 | 2 | 3 | 4 | 5 | 6 | 8 | 9 | 10 |
| 41 | 6128 | 6138 | 6149 | 6160 | 6170 | 6180 | 6191 | 6201 | 6212 | 6222 | , | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 42 | 6232 | 6243 | 6253 | 6263 | 6274 | 6284 | 6294 | 6304 | 6314 | 6325 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 43 | 6335 | 6345 | 6355 | 6365 | 6375 | 6385 | 6395 | 6405 | 6415 | 6425 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 44 | 6435 | 6444 | 6454 | 6464 | 6474 | 6484 | 6493 | 6503 | 6513 | 6522 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |


Proportional parts

TABLE 6-9 Cont.
Common Logarithms

| $N$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional parts |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | $I$ | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 45 | 6532 | 6542 | 6551 | 6561 | 6571 | 6580 | 6590 | 6599 | 6609 | 6618 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 46 | 6628 | 6637 | 6646 | 6656 | 6665 | 6675 | 6684 | 6693 | 6702 | 6712 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 7 | 8 |
| 47 | 6721 | 6730 | 6739 | 6749 | 6758 | 6767 | 6776 | 6785 | 6794 | 6803 | 1 | 2 | 3 | 4 | 5 | 5 | 6 | 7 | 8 |
| 48 | 6812 | 6821 | 6830 | 6839 | 6848 | 6857 | 6866 | 6875 | 6884 | 6893 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 8 |
| 49 | 6902 | 6911 | 6920 | 6928 | 6937 | 6946 | 6955 | 6964 | 6972 | 6981 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 | 8 |
| 50 | 6990 | 6998 | 7007 | 7016 | 7024 | 7033 | 7042 | 7050 | 7059 | 7067 | 1 | 2 | 3 | 3 | 4 | 5 | 6 | 7 | 8 |
| 51 | 7076 | 7084 | 7093 | 7101 | 7110 | 7118 | 7126 | 7135 | 7143 | 7152 | 1 | 2 | 3 | 3 | 4 | 5 | 6 | 7 | 8 |
| 52 | 7160 | 7168 | 7177 | 7185 | 7193 | 7202 | 7210 | 7218 | 7226 | 7235 | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 7 | 7 |
| 53 | 7243 | 7251 | 7259 | 7267 | 7275 | 7284 | 7292 | 7300 | 7308 | 7316 | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 6 | 7 |
| 54 | 7324 | 7332 | 7340 | 7348 | 7356 | 7364 | 7372 | 7380 | 7388 | 7396 | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 6 | 7 |
| 55 | 7404 | 7412 | 7419 | 7427 | 7435 | 7443 | 7451 | 7459 | 7466 | 7474 | 1 | 2 | 2 | 3 | 4 | 5 | 5 | 6 | 7 |
| 56 | 7482 | 7490 | 7497 | 7505 | 7513 | 7520 | 7528 | 7536 | 7543 | 7551 | 1 | 2 | 2 | 3 | 4 | 5 | 5 | 6 | 7 |
| 57 | 7559 | 7566 | 7574 | 7582 | 7589 | 7597 | 7604 | 7612 | 7619 | 7627 | 1 | 2 | 2 | 3 | 4 | 5 | 5 | 6 | 7 |
| 58 | 7634 | 7642 | 7649 | 7657 | 7664 | 7672 | 7679 | 7686 | 7694 | 7701 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 |
| 59 | 7709 | 7716 | 7723 | 7731 | 7738 | 7745 | 7752 | 7760 | 7767 | 7774 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 7 |
| 60 | 7782 | 7789 | 7796 | 7803 | 7810 | 7818 | 7825 | 7832 | 7839 | 7846 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 6 |
| 61 | 7853 | 7860 | 7868 | 7875 | 7882 | 7889 | 7896 | 7903 | 7910 | 7917 | 1 | 1 | 2 | 3 | 4 | 4 | 5 | 6 | 6 |
| 62 | 7924 | 7931 | 7938 | 7945 | 7952 | 7959 | 7966 | 7973 | 7980 | 7987 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 6 | 6 |
| 63 | 7993 | 8000 | 8007 | 8014 | 8021 | 8028 | 8035 | 8041 | 8048 | 8055 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 64 | 8062 | 8069 | 8075 | 8082 | 8089 | 8096 | 8102 | 8109 | 8116 | 8122 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 65 | 8129 | 8136 | 8142 | 8149 | 8156 | 8162 | 8169 | 8176 | 8182 | 8189 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 66 | 8195 | 8202 | 8209 | 8215 | 8222 | 8228 | 8235 | 8241 | 8248 | 8254 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 67 | 8261 | 8267 | 8274 | 8280 | 8287 | 8293 | 8299 | 8306 | 8312 | 8319 | 1 | 1 | 2 | 3 | 3 | 4 | 5 | 5 | 6 |
| 68 | 8325 | 8331 | 8338 | 8344 | 8351 | 8357 | 8363 | 8370 | 8376 | 8382 | 1 | 1 | 2 | 3 | 3 | 4 | 4 | 5 | 6 |
| 69 | 8388 | 8395 | 8401 | 8407 | 8414 | 8420 | 8426 | 8432 | 8439 | 8445 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 6 |
| 70 | 8451 | 8457 | 8463 | 8470 | 8476 | 8482 | 8488 | 8494 | 8500 | 8506 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 6 |
| 71 | 8513 | 8519 | 8525 | 8531 | 8537 | 8543 | 8549 | 8555 | 8561 | 8567 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 72 | 8573 | 8579 | 8585 | 8591 | 8597 | 8603 | 8609 | 8615 | 8621 | 8627 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 73 | 8633 | 8639 | 8645 | 8651 | 8657 | 8663 | 8669 | 8675 | 8681 | 8686 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 74 | 8692 | 8698 | 8704 | 8710 | 8716 | 8722 | 8727 | 8733 | 8739 | 8745 | 1 | 1 | 2 | 2 | 3 | 4 | 4 | 5 | 5 |
| 75 | 8751 | 8756 | 8762 | 8768 | 8774 | 8779 | 8785 | 8791 | 8797 | 8802 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 5 | 5 |
| 76 | 8808 | 8814 | 8820 | 8825 | 8831 | 8837 | 8842 | 8848 | 8854 | 8859 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 5 | 5 |
| 77 | 8865 | 8871 | 8876 | 8882 | 8887 | 8893 | 8899 | 8904 | 8910 | 8915 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 78 | 8921 | 8927 | 8932 | 8938 | 8943 | 8949 | 8954 | 8960 | 8965 | 8971 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 79 | 8976 | 8982 | 8987 | 8993 | 8998 | 9004 | 9009 | 9015 | 9020 | 9025 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| $N$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | ropo | tion | 1 pa |  |  |  |

TABLE 6-9 Cont.
Common Logarithms

| $N$ | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | Proportional parts |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 80 | 9031 | 9036 | 9042 | 9047 | 9053 | 9058 | 9063 | 9069 | 9074 | 9079 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 81 | 9085 | 9090 | 9096 | 9101 | 9106 | 9112 | 9117 | 9122 | 9128 | 9133 |  | , | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 82 | 9138 | 9143 | 9149 | 9154 | 9159 | 9165 | 9170 | 9175 | 9180 | 9186 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 83 | 9191 | 9196 | 9201 | 9206 | 9212 | 9217 | 9222 | 9227 | 9232 | 9238 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 84 | 9243 | 9248 | 9253 | 9258 | 9263 | 9269 | 9274 | 9279 | 9284 | 9289 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 85 | 9294 | 9299 | 9304 | 9309 | 9315 | 9320 | 9325 | 9330 | 9335 | 9340 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 86 | 9345 | 9350 | 9355 | 9360 | 9365 | 9370 | 9375 | 9380 | 9385 | 9390 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 | 5 |
| 87 | 9395 | 9400 | 9405 | 9410 | 9415 | 9420 | 9425 | 9430 | 9435 | 9440 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 88 | 9445 | 9450 | 9455 | 9460 | 9465 | 9469 | 9474 | 9479 | 9484 | 9489 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 89 | 9494 | 9499 | 9504 | 9509 | 9513 | 9518 | 9523 | 9528 | 9533 | 9538 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 90 | 9542 | 9547 | 9552 | 9557 | 9562 | 9566 | 9571 | 9576 | 9581 | 9586 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 91 | 9590 | 9595 | 9600 | 9605 | 9609 | 9614 | 9619 | 9624 | 9628 | 9633 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 92 | 9638 | 9643 | 9647 | 9652 | 9657 | 9661 | 9666 | 9671 | 9675 | 9680 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 93 | 9685 | 9689 | 9694 | 9699 | 9703 | 9708 | 9713 | 9717 | 9722 | 9727 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 94 | 9731 | 9736 | 9741 | 9745 | 9750 | 9754 | 9759 | 9763 | 9768 | 9773 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 95 | 9777 | 9782 | 9786 | 9791 | 9795 | 9800 | 9805 | 9809 | 9814 | 9818 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 96 | 9823 | 9827 | 9832 | 9836 | 9841 | 9845 | 9850 | 9854 | 9859 | 9863 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 97 | 9868 | 9872 | 9877 | 9881 | 9886 | 9890 | 9894 | 9899 | 9903 | 9908 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 98 | 9912 | 9917 | 9921 | 9926 | 9930 | 9934 | 9939 | 9943 | 9948 | 9952 | 0 | 1 | 1 | 2 | 2 | 3 | 3 | 4 | 4 |
| 99 | 9956 | 9961 | 9965 | 9969 | 9974 | 9978 | 9983 | 9987 | 9991 | 9996 | 0 | 1 | , | 2 | 2 | 3 | 3 | 3 | 4 |
| $N$ | 0 | I | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|  |  |  |  |  |  |  |  |  |  |  | Proportional parts |  |  |  |  |  |  |  |  |

characteristic. Thus, the mantissa of 0.0234 is 3692 , and the characteristic is -2 . The total logarithm is $-2+0.3692$, or -1.6308 . A negative logarithm is difficult to use; therefore, it is more convenient to convert the logarithm to a positive number. This is possible by adding 10 , or a multiple thereof, to the characteristic when it is negative, and compensating for this by indicating the subtraction of 10 from the entire logarithm. Thus, the logarithm of 0.0234 would be written $8.3692-10$, since $-2+0.3692$ equals $8+0.3692-10$. This logarithm may now be used like any other positive logarithm, except that the -10 must be consid-
ered in determining the characteristic of the answer.

## Antilogarithms

An antilogarithm (abbreviated antilog or $\log ^{-1}$ ) is a number corresponding to a given logarithm. To find an antilog, locate in the logarithm table the mantissa closest to that of the given logarithm. Record the number in the $N$ column directly opposite the mantissa located, and annex to this the number on the top line immediately above the mantissa. Next determine where the decimal point is located by counting off the number of places indicated by the character-
istic. Starting between the first and second digits, count to the right if the characteristic is positive, and to the left if it is negative. If greater accuracy is desired, the "Proportional parts" columns of the logarithm table can be used, in the same manner already described for finding the mantissa.

Example. Find the antilog of 3.4548 . Locate 4548 in Table 6-9. Then read the first two figures of the antilog from the $N$ column (28) and the third figure directly above the mantissa (5). Thus, the three figures of the antilog are 285 . Locate the decimal point by counting off three places to the right, from the point between the 2 and the 8 , to obtain 2850.0 -the antilog of 3.4548 .

In the foregoing example, if the logarithm had been $-2+0.4548$, the procedure would have been the same except for the location of the decimal point. The decimal point in this example would be located by starting at the point between the 2 and the 8 , and counting two places to the left to obtain 0.0285 -the antilog of $-2+0.4548$.

## Multiplication

Numbers are multiplied by adding their logarithms and finding the antilog of the sum.

Example. To multiply $682 \times 497$, procced as follows:

$$
\begin{aligned}
\log N & =\log 682+\log 497 \\
\log 682 & =2.8338 \\
+\log 497 & =\frac{2.6964}{5.5302} \\
\log N & =5 .
\end{aligned}
$$

$$
\text { antilog } 5.5302=339,000
$$

Example. To multiply $0.02 \times 0.03 \times 0.5$, proceed as follows:

$$
\begin{aligned}
& \log N=\log 0.02+\log 0.03+\log 0.5 \\
& \log 0.02=-2+0.3010=8.3010-10 \\
& +\log 0.03=-2+0.4771=8.4771-10 \\
& \begin{aligned}
+\log 0.5=-1+0.6990 & =\frac{9.6990-10}{26.4771-30} \\
\log N & =\frac{8.0}{0.4771}
\end{aligned} \\
& =-4+0.4771 \\
& \text { antilog }-4+0.4771=0.0003
\end{aligned}
$$

## Division

Numbers are divided by subtracting the logarithm of the divisor from the logarithm of the dividend and finding the antilog of the difference.

Example. To divide 39,200 by 27.2 , proceed as follows:

$$
\begin{aligned}
\log N & =\log 39,200-\log 27.2 \\
\log 39,200 & =4.5933 \\
-\log 27.2 & =\underline{1.4346} \\
\log N & =3.1587
\end{aligned}
$$

antilog $3.1587=1441$

Example. To divide 0.3 by 0.007 , proceed as follows:

$$
\log N=\log 0.3-\log 0.007
$$

$\begin{aligned} \log 0.3=-1+0.4771 & =9.4771-10 \\ -\log 0.007=-3+0.8451 & =\frac{7.8451-10}{1.6320-0}\end{aligned}$
antilog $1.6320=42.86$

## Raising to Powers

A given number can be raised to any power by multiplying the logarithm of the given number by the power to which the number is to be raised and finding the anti$\log$ of the product.

Example. To raise 39.7 to the third power, proceed as follows:

$$
\log N=\log 39.7 \times 3
$$

$$
\log 39.7=1.5988
$$

$$
\log N=1.5988 \times 3
$$

$$
=4.7964
$$

antilog $4.7964=62,570$

## Extracting Roots

Any root can be extracted from a given number by dividing the logarithm of the given number by the index of the root and finding the antilog of the quotient.

Example. To extract the cube root of 149, proceed as follows:

$$
\begin{aligned}
\log N & =\log 149 \div 3 \\
\log 149 & =2.1732 \\
\log N & =2.1732 \div 3 \\
& =0.7244
\end{aligned}
$$

antilog $0.7244=5.301$

## Natural Logarithms

Natural logarithms are similar to common logarithms, except that a natural logarithm uses the base 2.71828 instead of the base 10 . Natural logarithms are important because many desk-top computers process natural logarithms but do not process common logarithms. In turn, the programmer must convert terms with common logarithms into corresponding terms with natural logarithms. Thus, $\log _{10} x=\log _{\mathrm{e}} 10$. Note that $e=2.71828$.

## Example.

$$
\mathrm{dB} \text { power gain }=10 * \log _{10}(\mathrm{P} 2 / \mathrm{P} 1)
$$

## Programmer writes:

dB power gain $=10 * \log _{\mathrm{c}}(\mathrm{P} 2 / \mathrm{P} 1) / \log _{\mathrm{c}}(10)$

## SQUARES, CUBES, SQUARE ROOTS, CUBE ROOTS, AND RECIPROCALS

Table 6-10 gives, for the natural numbers up to 1000 , the squares, cubes, square roots, cube roots, and reciprocals multiplied by 1000 .

The " $1000 / n$ " column contains the product of $1 / n$ and 1000. To find the reciprocal of $n$ (viz., $1 / n$ ), divide the entry for $n$ in the " $1000 / n$ " column by 1000 (i.e., move the decimal point three places to the left).

For any number that is not a natural number between 1 and 1000 , its square and cube may be quickly, though perhaps approximately, obtained as follows. First, write the given number as the product of a number between 100 and 1000 , and a power of 10 . Disregard the nonzero digits, if any, to the right of the decimal point of the number between 100 and 1000. (If there are any numbers to the right of the decimal point, the square or cube obtained will be approximate.) Using the equations:

$$
\left(a \times 10^{b}\right)^{2}=a^{2} \times 10^{2 b}
$$

and

$$
\left(a \times 10^{b}\right)^{3}=a^{3} \times 10^{3 b}
$$

the square or cube of the given number may be obtained, the value of $a^{2}$ or $a^{3}$ being read from the table. The term $10^{2 b}$ or $10^{3 b}$ may be calculated mentally.

To find the square root of a number that is not a natural number between 1 and 1000,
write the number in the form $a \times 10^{\text {b }}$, where $a$ is between 10 and 1000 and $b$ is even and can be positive or negative. Disregard the nonzero digits, if any, to the right of the decimal point of the number $a$. (If there are any numbers to the right of the decimal point, the square root obtained will be approximate.) Locate the two- or three-digit number $a$ in the $n$ column, and read its square root. Multiplying this square root by $10^{\text {n: }}$ gives the square root of the given number.

To find the cube root of a number that is not a natural number between 1 and 1000 , write the given number in the form $a \times 10^{\text {b }}$, where $a$ is between 1 and 1000 and $b$ is divisible by 3 and can be positive or negative. Disregard the nonzero digits, if any, to the right of the decimal point of the number $a$. (If there are any, the cube root obtained will be
approximate.) Locate the number $a$ in the $n$ column of Table 6-10, and read its cube root. Multiplying this cube root by $10^{\text {b3 }}$ gives the cube root of the given number.

Note. Various kinds of numbers are used in electric and electronics formulas. The decimal numbers are $0,1,2,3,4,5,6,7,8$, and 9 ; the binary numbers are 0 and 1 . The negative numbers are -1 , $-2,-3$, and so on. Although +2 is greater than $+1,-2$ is less than -1 , and the computer processes negative numbers accordingly. The absolute value of -2 is greater than the absolute value of -1 , and the computer processes absolute values accordingly. The imaginary numbers are $\sqrt{-1}$, $-\sqrt{-1}, 2 \sqrt{-1},-3 \sqrt{-1}$, and so on. The $\sqrt{-1}$ is called the $j$ operator in electricity and electronics; $+j$ denotes inductive reactance, and $-j$ denotes capacitive reactance. Small computers cannot process imaginary numbers, and such formulas must be converted into square, square root, and trigonometric terms.

TABLE 6-10
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{\text {r }}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 1 | 1.0000 | 1.0000 | 1000.000 |
| 2 | 4 | 8 | 1.4142 | 1.2599 | 500.000 |
| 3 | 9 | 27 | 1.7321 | 1.4422 | 333.333 |
| 4 | 16 | 64 | 2.0000 | 1.5874 | 250.000 |
| 5 | 25 | 125 | 2.2361 | 1.7100 | 200.000 |
| 6 | 36 | 216 | 2.4495 | 1.8171 | 166.667 |
| 7 | 49 | 343 | 2.6458 | 1.9129 | 142.857 |
| 8 | 64 | 512 | 2.8284 | 2.0000 | 125.000 |
| 9 | 81 | 729 | 3.0000 | 2.0801 | 111.111 |
| 10 | 100 | 1000 | 3.1623 | 2.1544 | 100.000 |
| 11 | 121 | 1331 | 3.3166 | 2.2240 | 90.9091 |
| 12 | 144 | 1728 | 3.4641 | 2.2894 | 83.3333 |
| 13 | 169 | 2197 | 3.6056 | 2.3513 | 76.9231 |
| 14 | 196 | 2744 | 3.7417 | 2.4101 | 71.4286 |
| 15 | 225 | 3375 | 3.8730 | 2.4662 | 66.6667 |
| 16 | 256 | 4096 | 4.0000 | 2.5198 | 62.5000 |
| 17 | 289 | 4913 | 4.1231 | 2.5713 | 58.8235 |
| 18 | 324 | 5832 | 4.2426 | 2.6207 | 55.5556 |
| 19 | 361 | 6859 | 4.3589 | 2.6684 | 52.6316 |

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ |  | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 400 | 8000 | 4.4721 | 2.7144 | 50.0000 |
| 21 | 441 | 9261 | 4.5826 | 2.7589 | 47.6190 |
| 22 | 484 | 10648 | 4.6904 | 2.8020 | 45.4545 |
| 23 | 529 | 12167 | 4.7958 | 2.8439 | 43.4783 |
| 24 | 576 | 13824 | 4.8990 | 2.8845 | 41.6667 |
| 25 | 625 | 15625 | 5.0000 | 2.9240 | 40.0000 |
| 26 | 676 | 17576 | 5.0990 | 2.9625 | 38.4615 |
| 27 | 729 | 19683 | 5.1962 | 3.0000 | 37.0370 |
| 28 | 784 | 21952 | 5.2915 | 3.0366 | 35.7143 |
| 29 | 841 | 24389 | 5.3852 | 3.0723 | 34.4828 |
| 30 | 900 | 27000 | 5.4772 | 3.1072 | 33.3333 |
| 31 | 961 | 29791 | 5.5678 | 3.1414 | 32.2581 |
| 32 | 1024 | 32768 | 5.6569 | 3.1748 | 31.2500 |
| 33 | 1089 | 35937 | 5.7446 | 3.2075 | 30.3030 |
| 34 | 1156 | 39304 | 5.8310 | 3.2396 | 29.4118 |
| 35 | 1225 | 42875 | 5.9161 | 3.2711 | 28.5714 |
| 36 | 1296 | 46656 | 6.0000 | 3.3019 | 27.7778 |
| 37 | 1369 | 50653 | 6.0828 | 3.3322 | 27.0270 |
| 38 | 1444 | 54872 | 6.1644 | 3.3620 | 26.3158 |
| 39 | 1521 | 59319 | 6.2450 | 3.3912 | 25.6410 |
| 40 | 1600 | 64000 | 6.3246 | 3.4200 | 25.0000 |
| 41 | 1681 | 68921 | 6.4031 | 3.4482 | 24.3902 |
| 42 | 1764 | 74088 | 6.4807 | 3.4760 | 23.8095 |
| 43 | 1849 | 79507 | 6.5574 | 3.5034 | 23.2558 |
| 44 | 1936 | 85184 | 6.6332 | 3.5303 | 22.7273 |
| 45 | 2025 | 91125 | 6.7082 | 3.5569 | 22.2222 |
| 46 | 2116 | 97336 | 6.7823 | 3.5830 | 21.7391 |
| 47 | 2209 | 103823 | 6.8557 | 3.6088 | 21.2766 |
| 48 | 2304 | 110592 | 6.9282 | 3.6342 | 20.8333 |
| 49 | 2401 | 117649 | 7.0000 | 3.6593 | 20.4082 |
| 50 | 2500 | 125000 | 7.0711 | 3.6840 | 20.0000 |
| 51 | 2601 | 132651 | 7.1414 | 3.7084 | 19.6078 |
| 52 | 2704 | 140608 | 7.2111 | 3.7325 | 19.2308 |
| 53 | 2809 | 148877 | 7.2801 | 3.7563 | 18.8679 |
| 54 | 2916 | 157464 | 7.3485 | 3.7798 | 18.5185 |
| 55 | 3025 | 166375 | 7.4162 | 3.8030 | 18.1818 |
| 56 | 3136 | 175616 | 7.4833 | 3.8259 | 17.8571 |
| 57 | 3249 | 185193 | 7.5498 | 3.8485 | 17.5439 |
| 58 | 3364 | 195112 | 7.6158 | 3.8709 | 17.2414 |
| 59 | 3481 | 205379 | 7.6811 | 3.8930 | 16.9492 |
| 60 | 3600 | 216000 | 7.7460 | 3.9149 | 16.6667 |
| 61 | 3721 | 226981 | 7.8102 | 3.9365 | 16.3934 |
| 62 | 3844 | 238328 | 7.8740 | 3.9579 | 16.1290 |
| 63 | 3969 | 250047 | 7.9373 | 3.9791 | 15.8730 |
| 64 | 4096 | 262144 | 8.0000 | 4.0000 | 15.6250 |
| 65 | 4225 | 274625 | 8.0623 | 4.0207 | 15.3846 |

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TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 66 | 4356 | 287496 | 8.1240 | 4.0412 | 15.1515 |
| 67 | 4489 | 300763 | 8.1854 | 4.0615 | 14.9254 |
| 68 | 4624 | 314432 | 8.2462 | 4.0817 | 14.7059 |
| 69 | 4761 | 328509 | 8.3066 | 4.1016 | 14.4928 |
| 70 | 4900 | 343000 | 8.3666 | 4.1213 | 14.2857 |
| 71 | 5041 | 357911 | 8.4261 | 4.1408 | 14.0845 |
| 72 | 5184 | 373248 | 8.4853 | 4.1602 | 13.8889 |
| 73 | 5329 | 389017 | 8.5440 | 4.1793 | 13.6986 |
| 74 | 5476 | 405224 | 8.6023 | 4.1983 | 13.5135 |
| 75 | 5625 | 421875 | 8.6603 | 4.2172 | 13.3333 |
| 76 | 5776 | 438976 | 8.7178 | 4.2358 | 13.1579 |
| 77 | 5929 | 456533 | 8.7750 | 4.2543 | 12.9870 |
| 78 | 6084 | 474552 | 8.8318 | 4.2727 | 12.8205 |
| 79 | 6241 | 493039 | 8.8882 | 4.2908 | 12.6582 |
| 80 | 6400 | 512000 | 8.9443 | 4.3089 | 12.5000 |
| 81 | 6561 | 531441 | 9.0000 | 4.3267 | 12.3457 |
| 82 | 6724 | 551368 | 9.0554 | 4.3445 | 12.1951 |
| 83 | 6889 | 571787 | 9.1104 | 4.3621 | 12.0482 |
| 84 | 7056 | 592704 | 9.1652 | 4.3795 | 11.9048 |
| 85 | 7225 | 614125 | 9.2195 | 4.3968 | 11.7647 |
| 86 | 7396 | 636056 | 9.2736 | 4.4140 | 11.6279 |
| 87 | 7569 | 658503 | 9.3274 | 4.4310 | 11.4943 |
| 88 | 7744 | 681472 | 9.3808 | 4.4480 | 11.3636 |
| 89 | 7921 | 704969 | 9.4340 | 4.4647 | 11.2360 |
| 90 | 8100 | 729000 | 9.4868 | 4.4814 | 11.1111 |
| 91 | 8281 | 753571 | 9.5394 | 4.4979 | 10.9890 |
| 92 | 8464 | 778688 | 9.5917 | 4.5144 | 10.8696 |
| 93 | 8649 | 804357 | 9.6437 | 4.5307 | 10.7527 |
| 94 | 8836 | 830584 | 9.6954 | 4.5468 | 10.6383 |
| 95 | 9025 | 857375 | 9.7468 | 4.5629 | 10.5263 |
| 96 | 9216 | 884736 | 9.7980 | 4.5789 | 10.4167 |
| 97 | 9409 | 912673 | 9.8489 | 4.5947 | 10.3093 |
| 98 | 9604 | 941192 | 9.8995 | 4.6104 | 10.2041 |
| 99 | 9801 | 970299 | 9.9499 | 4.6261 | 10.1010 |
| 100 | 10000 | 1000000 | 10.0000 | 4.6416 | 10.0000 |
| 101 | 10201 | 1030301 | 10.0499 | 4.6570 | 9.90099 |
| 102 | 10404 | 1061208 | 10.0995 | 4.6723 | 9.80392 |
| 103 | 10609 | 1092727 | 10.1489 | 4.6875 | 9.70874 |
| 104 | 10816 | 1124864 | 10.1980 | 4.7027 | 9.61538 |
| 105 | 11025 | 1157625 | 10.2470 | 4.7177 | 9.52381 |
| 106 | 11236 | 1191016 | 10.2956 | 4.7326 | 9.43396 |
| 107 | 11449 | 1225043 | 10.3441 | 4.7475 | 9.34579 |
| 108 | 11664 | 1259712 | 10.3923 | 4.7622 | 9.25926 |
| 109 | 11881 | 1295029 | 10.4403 | 4.7769 | 9.17431 |

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TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | , $n$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 110 | 12100 | 1331000 | 10.4881 | 4.7914 | 9.09091 |
| 111 | 12321 | 1367631 | 10.5357 | 4.8059 | 9.00901 |
| 112 | 12544 | 1404928 | 10.5830 | 4.8203 | 8.92857 |
| 113 | 12769 | 1442897 | 10.6301 | 4.8346 | 8.84956 |
| 114 | 12996 | 1481544 | 10.6771 | 4.8488 | 8.77193 |
| 115 | 13225 | 1520875 | 10.7238 | 4.8629 | 8.69565 |
| 116 | 13456 | 1560896 | 10.7703 | 4.8770 | 8.62069 |
| 117 | 13689 | 1601613 | 10.8167 | 4.8910 | 8.54701 |
| 118 | 13924 | 1643032 | 10.8628 | 4.9049 | 8.47458 |
| 119 | 14161 | 1685159 | 10.9087 | 4.9187 | 8.40336 |
| 120 | 14400 | 1728000 | 10.9545 | 4.9324 | 8.33333 |
| 121 | 14641 | 1771561 | 11.0000 | 4.9461 | 8.26446 |
| 122 | 14884 | 1815848 | 11.0454 | 4.9597 | 8.19672 |
| 123 | 15129 | 1860867 | 11.0905 | 4.9732 | 8.13008 |
| 124 | 15376 | 1906624 | 11.1355 | 4.9866 | 8.06452 |
| 125 | 15625 | 1953125 | 11.1803 | 5.0000 | 8.00000 |
| 126 | 15876 | 2000376 | 11.2250 | 5.0133 | 7.93651 |
| 127 | 16129 | 2048383 | 11.2694 | 5.0265 | 7.87402 |
| 128 | 16384 | 2097152 | 11.3137 | 5.0397 | 7.81250 |
| 129 | 16641 | 2146689 | 11.3578 | 5.0528 | 7.75194 |
| 130 | 16900 | 2197000 | 11.4018 | 5.0658 | 7.69231 |
| 131 | 17161 | 2248091 | 11.4455 | 5.0788 | 7.63359 |
| 132 | 17424 | 2299968 | 11.4891 | 5.0916 | 7.57576 |
| 133 | 17689 | 2352637 | 11.5326 | 5.1045 | 7.51880 |
| 134 | 17956 | 2406104 | 11.5758 | 5.1172 | 7.46269 |
| 135 | 18225 | 2460375 | 11.6190 | 5.1299 | 7.40741 |
| 136 | 18496 | 2515456 | 11.6619 | 5.1426 | 7.35294 |
| 137 | 18769 | 2571353 | 11.7047 | 5.1551 | 7.29927 |
| 138 | 19044 | 2628072 | 11.7473 | 5.1676 | 7.24638 |
| 139 | 19321 | 2685619 | 11.7898 | 5.1801 | 7.19424 |
| 140 | 19600 | 2744000 | 11.8322 | 5.1925 | 7.14286 |
| 141 | 19881 | 2803221 | 11.8743 | 5.2048 | 7.09220 |
| 142 | 20164 | 2863288 | 11.9164 | 5.2171 | 7.04255 |
| 143 | 20449 | 2924207 | 11.9583 | 5.2293 | 6.99301 |
| 144 | 20736 | 2985984 | 12.0000 | 5.2415 | 6.94444 |
| 145 | 21025 | 3048625 | 12.0416 | 5.2536 | 6.89655 |
| 146 | 21316 | 3112126 | 12.0830 | 5.2656 | 6.84932 |
| 147 | 21609 | 3176523 | 12.1244 | 5.2776 | 6.80272 |
| 148 | 21904 | 3241792 | 12.1655 | 5.2896 | 6.75676 |
| 149 | 22201 | 3307949 | 12.2066 | 5.3015 | 6.71141 |
| 150 | 22500 | 3375000 | 12.2474 | 5.3133 | 6.66667 |
| 151 | 22801 | 3442951 | 12.2882 | 5.3251 | 6.62252 |
| 152 | 23104 | 3511808 | 12.3288 | 5.3368 | 6.57895 |
| 153 | 23409 | 3581577 | 12.3693 | 5.3485 | 6.53595 |
| 154 | 23716 | 3652264 | 12.4097 | 5.3601 | 6.49351 |
| 155 | 24025 | 3723875 | 12.4499 | 5.3717 | 6.45161 |

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TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 156 | 24336 | 3796416 | 12.4900 | 5.3832 | 6.41026 |
| 157 | 24649 | 3869893 | 12.5300 | 5.3947 | 6.36943 |
| 158 | 24964 | 3944312 | 12.5698 | 5.4061 | 6.32911 |
| 159 | 25281 | 4019679 | 12.6095 | 5.4175 | 6.28931 |
| 160 | 25600 | 4096000 | 12.6491 | 5.4288 | 6.25000 |
| 161 | 25921 | 4173281 | 12.6886 | 5.4401 | 6.21118 |
| 162 | 26244 | 4251528 | 12.7279 | 5.4514 | 6.17284 |
| 163 | 26569 | 4330747 | 12.7671 | 5.4626 | 6.13497 |
| 164 | 26896 | 4410944 | 12.8062 | 5.4737 | 6.09756 |
| 165 | 27225 | 4492125 | 12.8452 | 5.4848 | 6.06061 |
| 166 | 27556 | 4574296 | 12.8841 | 5.4959 | 6.02410 |
| 167 | 27889 | 4657463 | 12.9228 | 5.5069 | 5.98802 |
| 168 | 28224 | 4741632 | 12.9615 | 5.5178 | 5.95238 |
| 169 | 28561 | 4826809 | 13.0000 | 5.5288 | 5.91716 |
| 170 | 28900 | 4913000 | 13.0384 | 5.5397 | 5.88235 |
| 171 | 29241 | 5000211 | 13.0767 | 5.5505 | 5.84795 |
| 172 | 29584 | 5088448 | 13.1149 | 5.5613 | 5.81395 |
| 173 | 29929 | 5177717 | 13.1529 | 5.5721 | 5.78035 |
| 174 | 30276 | 5268024 | 13.1909 | 5.5828 | 5.74713 |
| 175 | 30625 | 5359375 | 13.2288 | 5.5934 | 5.71429 |
| 176 | 30976 | 5451776 | 13.2665 | 5.6041 | 5.68182 |
| 177 | 31329 | 5545233 | 13.3041 | 5.6147 | 5.64972 |
| 178 | 31684 | 5639752 | 13.3417 | 5.6252 | 5.61798 |
| 179 | 32041 | 5735339 | 13.3791 | 5.6357 | 5.58659 |
| 180 | 32400 | 5832000 | 13.4164 | 5.6462 | 5.55556 |
| 181 | 32761 | 5929741 | 13.4536 | 5.6567 | 5.52486 |
| 182 | 33124 | 6028568 | 13.4907 | 5.6671 | 5.49451 |
| 183 | 33489 | 6128487 | 13.5277 | 5.6774 | 5.46448 |
| 184 | 33856 | 6229504 | 13.5647 | 5.6877 | 5.43478 |
| 185 | 34225 | 6331625 | 13.6015 | 5.6980 | 5.40541 |
| 186 | 34596 | 6434856 | 13.6382 | 5.7083 | 5.37634 |
| 187 | 34969 | 6539203 | 13.6748 | 5.7185 | 5.34759 |
| 188 | 35344 | 6644672 | 13.7113 | 5.7287 | 5.31915 |
| 189 | 35721 | 6751269 | 13.7477 | 5.7388 | 5.29101 |
| 190 | 36100 | 6859000 | 13.7840 | 5.7489 | 5.26316 |
| 191 | 36481 | 6967871 | 13.8203 | 5.7590 | 5.23560 |
| 192 | 36864 | 7077888 | 13.8564 | 5.7690 | 5.20833 |
| 193 | 37249 | 7189057 | 13.8924 | 5.7790 | 5.18135 |
| 194 | 37636 | 7301384 | 13.9284 | 5.7890 | 5.15464 |
| 195 | 38025 | 7414875 | 13.9642 | 5.7989 | 5.12821 |
| 196 | 38416 | 7529536 | 14.0000 | 5.8088 | 5.10204 |
| 197 | 38809 | 7645373 | 14.0357 | 5.8186 | 5.07614 |
| 198 | 39204 | 7762392 | 14.0712 | 5.8285 | 5.05051 |
| 199 | 39601 | 7880599 | 14.1067 | 5.8383 | 5.02513 |

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{*}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 200 | 40000 | 8000000 | 14.1421 | 5.8480 | 5.00000 |
| 201 | 40401 | 8120601 | 14.1774 | 5.8578 | 4.97512 |
| 202 | 40804 | 8242408 | 14.2127 | 5.8675 | 4.95050 |
| 203 | 41209 | 8365427 | 14.2478 | 5.8771 | 4.92611 |
| 204 | 41616 | 8489664 | 14.2829 | 5.8868 | 4.90196 |
| 205 | 42025 | 8615125 | 14.3178 | 5.8964 | 4.87805 |
| 206 | 42436 | 8741816 | 14.3527 | 5.9059 | 4.85437 |
| 207 | 42849 | 8869743 | 14.3875 | 5.9155 | 4.83092 |
| 208 | 43264 | 8998912 | 14.4222 | 5.9250 | 4.80769 |
| 209 | 43681 | 9129329 | 14.4568 | 5.9345 | 4.78469 |
| 210 | 44100 | 9261000 | 14.4914 | 5.9439 | 4.76190 |
| 211 | 44521 | 9393931 | 14.5258 | 5.9533 | 4.73934 |
| 212 | 44944 | 9528128 | 14.5602 | 5.9627 | 4.71698 |
| 213 | 45369 | 9663597 | 14.5945 | 5.9721 | 4.69484 |
| 214 | 45796 | 9800344 | 14.6287 | 5.9814 | 4.67290 |
| 215 | 46225 | 9938375 | 14.6629 | 5.9907 | 4.65116 |
| 216 | 46656 | 10077696 | 14.6969 | 6.0000 | 4.62963 |
| 217 | 47089 | 10218313 | 14.7309 | 6.0092 | 4.60829 |
| 218 | 47524 | 10360232 | 14.7648 | 6.0185 | 4.58716 |
| 219 | 47961 | 10503459 | 14.7986 | 6.0277 | 4.56621 |
| 220 | 48400 | 10648000 | 14.8324 | 6.0368 | 4.54545 |
| 221 | 48841 | 10793861 | 14.8661 | 6.0459 | 4.52489 |
| 222 | 49284 | 10941048 | 14.8997 | 6.0550 | 4.50450 |
| 223 | 49729 | 11089567 | 14.9332 | 6.0641 | 4.48431 |
| 224 | 50176 | 11239424 | 14.9666 | 6.0732 | 4.46429 |
| 225 | 50625 | 11390625 | 15.0000 | 6.0822 | 4.44444 |
| 226 | 51076 | 11543176 | 15.0333 | 6.0912 | 4.42478 |
| 227 | 51529 | 11697083 | 15.0665 | 6.1002 | 4.40529 |
| 228 | 51984 | 11852352 | 15.0997 | 6.1091 | 4.38596 |
| 229 | 52441 | 12008989 | 15.1327 | 6.1180 | 4.36681 |
| 230 | 52900 | 12167000 | 15.1658 | 6.1269 | 4.34783 |
| 231 | 53361 | 12326391 | 15.1987 | 6.1358 | 4.32900 |
| 232 | 53824 | 12487168 | 15.2315 | 6.1446 | 4.31034 |
| 233 | 54289 | 12649337 | 15.2643 | 6.1534 | 4.29185 |
| 234 | 54756 | 12812904 | 15.2971 | 6.1622 | 4.27350 |
| 235 | 55225 | 12977875 | 15.3297 | 6.1710 | 4.25532 |
| 236 | 55696 | 13144256 | 15.3623 | 6.1797 | 4.23729 |
| 237 | 56169 | 13312053 | 15.3948 | 6.1885 | 4.21941 |
| 238 | 56644 | 13481272 | 15.4272 | 6.1972 | 4.20168 |
| 239 | 57121 | 13651919 | 15.4596 | 6.2058 | 4.18410 |
|  |  |  | 15.4919 | 6.2145 |  |
| 241 | 58081 | 13997521 | 15.5242 | 6.2231 | 4.14938 |
| 242 | 58564 | 14172488 | 15.5563 | 6.2317 | 4.13223 |
| 243 | 59049 | 14348907 | 15.5885 | 6.2403 | 4.11523 |
| 244 | 59536 | 14526784 | 15.6205 | 6.2488 | 4.09836 |
| 245 | 60025 | 14706125 | 15.6525 | 6.2573 | 4.08163 |

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[1]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 246 | 60516 | 14886936 | 15.6844 | 6.2658 | 4.06504 |
| 247 | 61009 | 15069223 | 15.7162 | 6.2743 | 4.04858 |
| 248 | 61504 | 15252992 | 15.7480 | 6.2828 | 4.03226 |
| 249 | 62001 | 15438249 | 15.7797 | 6.2912 | 4.01606 |
| 250 | 62500 | 15625000 | 15.8114 | 6.2996 | 4.00000 |
| 251 | 63001 | 15813251 | 15.8430 | 6.3080 | 3.98406 |
| 252 | 63504 | 16003008 | 15.8745 | 6.3164 | 3.96825 |
| 253 | 64009 | 16194277 | 15.9060 | 6.3247 | 3.95257 |
| 254 | 64516 | 16387064 | 15.9374 | 6.3330 | 3.93701 |
| 255 | 65025 | 16581375 | 15.9687 | 6.3413 | 3.92157 |
| 256 | 65536 | 16777216 | 16.0000 | 6.3496 | 3.90625 |
| 257 | 66049 | 16974593 | 16.0312 | 6.3579 | 3.89105 |
| 258 | 66564 | 17173512 | 16.0624 | 6.3661 | 3.87597 |
| 259 | 67081 | 17373979 | 16.0935 | 6.3743 | 3.86100 |
| 260 | 67600 | 17576000 | 16.1245 | 6.3825 | 3.84615 |
| 261 | 68121 | 17779581 | 16.1555 | 6.3907 | 3.83142 |
| 262 | 68644 | 17984728 | 16.1864 | 6.3988 | 3.81679 |
| 263 | 69169 | 18191447 | 16.2173 | 6.4070 | 3.80228 |
| 264 | 69696 | 18399744 | 16.2481 | 6.4151 | 3.78788 |
| 265 | 70225 | 18609625 | 16.2788 | 6.4232 | 3.77358 |
| 266 | 70756 | 18821096 | 16.3095 | 6.4312 | 3.75940 |
| 267 | 71289 | 19034163 | 16.3401 | 6.4393 | 3.74532 |
| 268 | 71824 | 19248832 | 16.3707 | 6.4473 | 3.73134 |
| 269 | 72361 | 19465109 | 16.4012 | 6.4553 | 3.71747 |
| 270 | 72900 | 19683000 | 16.4317 | 6.4633 | 3.70370 |
| 271 | 73441 | 19902511 | 16.4621 | 6.4713 | 3.69004 |
| 272 | 73984 | 20123648 | 16.4924 | 6.4792 | 3.67647 |
| 273 | 74529 | 20346417 | 16.5227 | 6.4872 | 3.66300 |
| 274 | 75076 | 20570824 | 16.5529 | 6.4951 | 3.64964 |
| 275 | 75625 | 20796875 | 16.5831 | 6.5030 | 3.63636 |
| 276 | 76176 | 21024576 | 16.6132 | 6.5108 | 3.62319 |
| 277 | 76729 | 21253933 | 16.6433 | 6.5187 | 3.61011 |
| 278 | 77284 | 21484952 | 16.6733 | 6.5265 | 3.59712 |
| 279 | 77841 | 21717639 | 16.7033 | 6.5343 | 3.58423 |
| 280 | 78400 | 21952000 | 16.7332 | 6.5421 | 3.57143 |
| 281 | 78961 | 22188041 | 16.7631 | 6.5499 | 3.55872 |
| 282 | 79524 | 22425768 | 16.7929 | 6.5577 | 3.54610 |
| 283 | 80089 | 22665187 | 16.8226 | 6.5654 | 3.53357 |
| 284 | 80656 | 22906304 | 16.8523 | 6.5731 | 3.52113 |
| 285 | 81225 | 23149125 | 16.8819 | 6.5808 | 3.50877 |
| 286 | 81796 | 23393656 | 16.9115 | 6.5885 | 3.49650 |
| 287 | 82369 | 23639903 | 16.9411 | 6.5962 | 3.48432 |
| 288 | 82944 | 23887872 | 16.9706 | 6.6039 | 3.47222 |
| 289 | 83521 | 24137569 | 17.0000 | 6.6115 | 3.46021 |

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 290 | 84100 | 24389000 | 17.0294 | 6.6191 | 3.44828 |
| 291 | 84681 | 24642171 | 17.0587 | 6.6267 | 3.43643 |
| 292 | 85264 | 24897088 | 17.0880 | 6.6343 | 3.42466 |
| 293 | 85849 | 25153757 | 17.1172 | 6.6419 | 3.41297 |
| 294 | 86436 | 25412184 | 17.1464 | 6.6494 | 3.40136 |
| 295 | 87025 | 25672375 | 17.1756 | 6.6569 | 3.38983 |
| 296 | 87616 | 25934336 | 17.2047 | 6.6644 | 3.37838 |
| 297 | 88209 | 26198073 | 17.2337 | 6.6719 | 3.36700 |
| 298 | 88804 | 26463592 | 17.2627 | 6.6794 | 3.35570 |
| 299 | 89401 | 26730899 | 17.2916 | 6.6869 | 3.34448 |
| 300 | 90000 | 27000000 | 17.3205 | 6.6943 | 3.33333 |
| 301 | 90601 | 27270901 | 17.3494 | 6.7018 | 3.32226 |
| 302 | 91204 | 27543608 | 17.3781 | 6.7092 | 3.31126 |
| 303 | 91809 | 27818127 | 17.4069 | 6.7166 | 3.30033 |
| 304 | 92416 | 28094464 | 17.4356 | 6.7240 | 3.28947 |
| 305 | 93025 | 28372625 | 17.4642 | 6.7313 | 3.27869 |
| 306 | 93636 | 28652616 | 17.4929 | 6.7387 | 3.26797 |
| 307 | 94249 | 28934443 | 17.5214 | 6.7460 | 3.25733 |
| 308 | 94864 | 29218112 | 17.5499 | 6.7533 | 3.24675 |
| 309 | 95481 | 29503629 | 17.5784 | 6.7606 | 3.23625 |
| 310 | 96100 | 29791000 | 17.6068 | 6.7679 | 3.22581 |
| 311 | 96721 | 30080231 | 17.6352 | 6.7752 | 3.21543 |
| 312 | 97344 | 30371328 | 17.6635 | 6.7824 | 3.20513 |
| 313 | 97969 | 30664297 | 17.6918 | 6.7897 | 3.19489 |
| 314 | 98596 | 30959144 | 17.7200 | 6.7969 | 3.18471 |
| 315 | 99225 | 31255875 | 17.7482 | 6.8041 | 3.17460 |
| 316 | 99856 | 31554496 | 17.7764 | 6.8113 | 3.16456 |
| 317 | 100489 | 31855013 | 17.8045 | 6.8185 | 3.15457 |
| 318 | 101124 | 32157432 | 17.8326 | 6.8256 | 3.14465 |
| 319 | 101761 | 32461759 | 17.8606 | 6.8328 | 3.13480 |
| 320 | 102400 | 32768000 | 17.8885 | 6.8399 | 3.12500 |
| 321 | 103041 | 33076161 | 17.9165 | 6.8470 | 3.11527 |
| 322 | 103684 | 33386284 | 17.9444 | 6.8541 | 3.10559 |
| 323 | 104329 | 33698267 | 17.9722 | 6.8612 | 3.09598 |
| 324 | 104976 | 34012224 | 18.0000 | 6.8683 | 3.08642 |
| 325 | 105625 | 34328125 | 18.0278 | 6.8753 | 3.07692 |
| 326 | 106276 | 34645976 | 18.0555 | 6.8824 | 3.06749 |
| 327 | 106929 | 34965783 | 18.0831 | 6.8894 | 3.05810 |
| 328 | 107584 | 35287552 | 18.1108 | 6.8964 | 3.04878 |
| 329 | 108241 | 35611289 | 18.1384 | 6.9034 | 3.03951 |
| 330 | 108900 | 35937000 | 18.1659 | 6.9104 | 3.03030 |
| 331 | 109561 | 36264691 | 18.1934 | 6.9174 | 3.02115 |
| 332 | 110224 | 36594368 | 18.2209 | 6.9244 | 3.01205 |
| 333 | 110889 | 36926037 | 18.2483 | 6.9313 | 3.00300 |
| 334 | 111556 | 37259704 | 18.2757 | 6.9382 | 2.99401 |
| 335 | 112225 | 37595375 | 18.3030 | 6.9451 | 2.98507 |

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TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 336 | 112896 | 37933056 | 18.3303 | 6.9521 | 2.97619 |
| 337 | 113569 | 38272753 | 18.3576 | 6.9589 | 2.96736 |
| 338 | 114244 | 38614472 | 18.3848 | 6.9658 | 2.95858 |
| 339 | 114921 | 38958219 | 18.4120 | 6.9727 | 2.94985 |
| 340 | 115600 | 39304000 | 18.4391 | 6.9795 | 2.94118 |
| 341 | 116281 | 39651821 | 18.4662 | 6.9864 | 2.93255 |
| 342 | 116964 | 40001688 | 18.4932 | 6.9932 | 2.92398 |
| 343 | 117649 | 40353607 | 18.5203 | 7.0000 | 2.91545 |
| 344 | 118336 | 40707584 | 18.5472 | 7.0068 | 2.90698 |
| 345 | 119025 | 41063625 | 18.5742 | 7.0136 | 2.89855 |
| 346 | 119716 | 41421736 | 18.6011 | 7.0203 | 2.89017 |
| 347 | 120409 | 41781923 | 18.6279 | 7.0271 | 2.88184 |
| 348 | 121104 | 42144192 | 18.6548 | 7.0338 | 2.87356 |
| 349 | 121801 | 42508549 | 18.6815 | 7.0406 | 2.86533 |
| 350 | 122500 | 42875000 | 18.7083 | 7.0473 | 2.85714 |
| 351 | 123201 | 43243551 | 18.7350 | 7.0540 | 2.84900 |
| 352 | 123904 | 43614208 | 18.7617 | 7.0607 | 2.84091 |
| 353 | 124609 | 43986977 | 18.7883 | 7.0674 | 2.83286 |
| 354 | 125316 | 44361864 | 18.8149 | 7.0740 | 2.82486 |
| 355 | 126025 | 44738875 | 18.8414 | 7.0807 | 2.81690 |
| 356 | 126736 | 45118016 | 18.8680 | 7.0873 | 2.80899 |
| 357 | 127449 | 45499293 | 18.8944 | 7.0940 | 2.80112 |
| 358 | 128164 | 45882712 | 18.9209 | 7.1006 | 2.79330 |
| 359 | 128881 | 46268279 | 18.9473 | 7.1072 | 2.78552 |
| 360 | 129600 | 46656000 | 18.9737 | 7.1138 | 2.77778 |
| 361 | 130321 | 47045881 | 19.0000 | 7.1204 | 2.77008 |
| 362 | 131044 | 47437928 | 19.0263 | 7.1269 | 2.76243 |
| 363 | 131769 | 47832147 | 19.0526 | 7.1335 | 2.75482 |
| 364 | 132496 | 48228544 | 19.0788 | 7.1400 | 2.74725 |
| 365 | 133225 | 48627125 | 19.1050 | 7.1466 | 2.73973 |
| 366 | 133956 | 49027896 | 19.1311 | 7.1531 | 2.73224 |
| 367 | 134689 | 49430863 | 19.1572 | 7.1596 | 2.72480 |
| 368 | 135424 | 49836032 | 19.1833 | 7.1661 | 2.71739 |
| 369 | 136161 | 50243409 | 19.2094 | 7.1726 | 2.71003 |
| 370 | 136900 | 50653000 | 19.2354 | 7.1791 | 2.70270 |
| 371 | 137641 | 51064811 | 19.2614 | 7.1855 | 2.69542 |
| 372 | 138384 | 51478848 | 19.2873 | 7.1920 | 2.68817 |
| 373 | 139129 | 51895117 | 19.3132 | 7.1984 | 2.68097 |
| 374 | 139876 | 52313624 | 19.3391 | 7.2048 | 2.67380 |
| 375 | 140625 | 52734375 | 19.3649 | 7.2112 | 2.66667 |
| 376 | 141376 | 53157376 | 19.3907 | 7.2177 | 2.65957 |
| 377 | 142129 | 53582633 | 19.4165 | 7.2240 | 2.65252 |
| 378 | 142884 | 54010152 | 19.4422 | 7.2304 | 2.64550 |
| 379 | 143641 | 54439939 | 19.4679 | 7.2368 | 2.63852 |

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\vee \overline{ }$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 380 | 144400 | 54872000 | 19.4936 | 7.2432 | 2.63158 |
| 381 | 145161 | 55306341 | 19.5192 | 7.2495 | 2.62467 |
| 382 | 145924 | 55742968 | 19.5448 | 7.2558 | 2.61780 |
| 383 | 146689 | 56181887 | 19.5704 | 7.2622 | 2.61097 |
| 384 | 147456 | 56623104 | 19.5959 | 7.2685 | 2.60417 |
| 385 | 148225 | 57066625 | 19.6214 | 7.2748 | 2.59740 |
| 386 | 148996 | 57512456 | 19.6469 | 7.2811 | 2.59067 |
| 387 | 149769 | 57960603 | 19.6723 | 7.2874 | 2.58398 |
| 388 | 150544 | 58411072 | 19.6977 | 7.2936 | 2.57732 |
| 389 | 151321 | 58863869 | 19.7231 | 7.2999 | 2.57069 |
| 390 | 152100 | 59319000 | 19.7484 | 7.3061 | 2.56410 |
| 391 | 152881 | 59776471 | 19.7737 | 7.3124 | 2.55755 |
| 392 | 153664 | 60236288 | 19.7990 | 7.3186 | 2.55102 |
| 393 | 154449 | 60698457 | 19.8242 | 7.3248 | 2.54453 |
| 394 | 155236 | 61162984 | 19.8494 | 7.3310 | 2.53807 |
| 395 | 156025 | 61629875 | 19.8746 | 7.3372 | 2.53165 |
| 396 | 156816 | 62099136 | 19.8997 | 7.3434 | 2.52525 |
| 397 | 157609 | 62570773 | 19.9249 | 7.3496 | 2.51889 |
| 398 | 158404 | 63044792 | 19.9499 | 7.3558 | 2.51256 |
| 399 | 159201 | 63521199 | 19.9750 | 7.3619 | 2.50627 |
| 400 | 160000 | 64000000 | 20.0000 | 7.3681 | 2.50000 |
| 401 | 160801 | 64481201 | 20.0250 | 7.3742 | 2.49377 |
| 402 | 161604 | 64964808 | 20.0499 | 7.3803 | 2.48756 |
| 403 | 162409 | 65450827 | 20.0749 | 7.3864 | 2.48139 |
| 404 | 163216 | 65939264 | 20.0998 | 7.3925 | 2.47525 |
| 405 | 164025 | 66430125 | 20.1246 | 7.3986 | 2.46914 |
| 406 | 164836 | 66923416 | 20.1494 | 7.4047 | 2.46305 |
| 407 | 165649 | 67419143 | 20.1742 | 7.4108 | 2.45700 |
| 408 | 166464 | 67917312 | 20.1990 | 7.4169 | 2.45098 |
| 409 | 167281 | 68417929 | 20.2237 | 7.4229 | 2.44499 |
| 410 | 168100 | 68921000 | 20.2485 | 7.4290 | 2.43902 |
| 411 | 168921 | 69426531 | 20.2731 | 7.4350 | 2.43309 |
| 412 | 169744 | 69934528 | 20.2978 | 7.4410 | 2.42718 |
| 413 | 170569 | 70444997 | 20.3224 | 7.4470 | 2.42131 |
| 414 | 171396 | 70957944 | 20.3470 | 7.4530 | 2.41546 |
| 415 | 172225 | 71473375 | 20.3715 | 7.4590 | 2.40964 |
| 416 | 173056 | 71991296 | 20.3961 | 7.4650 | 2.40385 |
| 417 | 173889 | 72511713 | 20.4206 | 7.4710 | 2.39808 |
| 418 | 174724 | 73034632 | 20.4450 | 7.4770 | 2.39234 |
| 419 | 175561 | 73560059 | 20.4695 | 7.4829 | 2.38664 |
| 420 | 176400 | 74088000 | 20.4939 | 7.4889 | 2.38095 |
| 421 | 177241 | 74618461 | 20.5183 | 7.4948 | 2.37530 |
| 422 | 178084 | 45151448 | 20.5426 | 7.5007 | 2.36967 |
| 423 | 178929 | 75686967 | 20.5670 | 7.5067 | 2.36407 |
| 424 | 179776 | 76225024 | 20.5913 | 7.5126 | 2.35849 |
| 425 | 180625 | 76765625 | 20.6155 | 7.5185 | 2.35294 |

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TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ |  | $n^{3}$ |  | $\sqrt{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |

Mathematical Tables and Formulas

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{*}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 470 | 220900 | 103823000 | 21.6795 | 7.7750 | 2.12766 |
| 471 | 221841 | 104487111 | 21.7025 | 7.7805 | 2.12314 |
| 472 | 222784 | 105154048 | 21.7256 | 7.7860 | 2.11864 |
| 473 | 223729 | 105823817 | 21.7486 | 7.7915 | 2.11417 |
| 474 | 224676 | 106496424 | 21.7715 | 7.7970 | 2.10971 |
| 475 | 225625 | 107171875 | 21.7945 | 7.8025 | 2.10526 |
| 476 | 226576 | 107850176 | 21.8174 | 7.8079 | 2.10084 |
| 477 | 227529 | 108531333 | 21.8403 | 7.8134 | 2.09644 |
| 478 | 228484 | 109215352 | 21.8632 | 7.8188 | 2.09205 |
| 479 | 229441 | 109902239 | 21.8861 | 7.8243 | 2.08768 |
| 480 | 230400 | 110592000 | 21.9089 | 7.8297 | 2.08333 |
| 481 | 231361 | 111284641 | 21.9317 | 7.8352 | 2.07900 |
| 482 | 232324 | 111980168 | 21.9545 | 7.8406 | 2.07469 |
| 483 | 233289 | 112678587 | 21.9773 | 7.8460 | 2.07039 |
| 484 | 234256 | 113379904 | 22.0000 | 7.8514 | 2.06612 |
| 485 | 235225 | 114084125 | 22.0227 | 7.8568 | 2.06186 |
| 486 | 236196 | 114791256 | 22.0454 | 7.8622 | 2.05761 |
| 487 | 237169 | 115501303 | 22.0681 | 7.8676 | 2.05339 |
| 488 | 238144 | 116214272 | 22.0907 | 7.8730 | 2.04918 |
| 489 | 239121 | 116930169 | 22.1133 | 7.8784 | 2.04499 |
| 490 | 240100 | 117649000 | 22.1359 | 7.8837 | 2.04082 |
| 491 | 241081 | 118370771 | 22.1585 | 7.8891 | 2.03666 |
| 492 | 242064 | 119095488 | 22.1811 | 7.8944 | 2.03252 |
| 493 | 243049 | 119823157 | 22.2036 | 7.8998 | 2.02840 |
| 494 | 244036 | 120553784 | 22.2261 | 7.9051 | 2.02429 |
| 495 | 245025 | 121287375 | 22.2486 | 7.9105 | 2.02020 |
| 496 | 246016 | 122023936 | 22.2711 | 7.9158 | 2.01613 |
| 497 | 247009 | 122763473 | 22.2935 | 7.9211 | 2.01207 |
| 498 | 248004 | 123505992 | 22.3159 | 7.9264 | 2.00803 |
| 499 | 249001 | 124251499 | 22.3383 | 7.9317 | 2.00401 |
| 500 | 250000 | 125000000 | 22.3607 | 7.9370 | 2.00000 |
| 501 | 251001 | 125751501 | 22.3830 | 7.9423 | 1.99601 |
| 502 | 252004 | 126506008 | 22.4054 | 7.9476 | 1.99203 |
| 503 | 253009 | 127263527 | 22.4277 | 7.9528 | 1.98807 |
| 504 | 254016 | 128024064 | 22.4499 | 7.9581 | 1.98413 |
| 505 | 255025 | 128787625 | 22.4722 | 7.9634 | 1.98020 |
| 506 | 256036 | 129554216 | 22.4944 | 7.9686 | 1.97629 |
| 507 | 257049 | 130323843 | 22.5167 | 7.9739 | 1.97239 |
| 508 | 258064 | 131096512 | 22.5389 | 7.9791 | 1.96850 |
| 509 | 259081 | 131872229 | 22.5610 | 7.9843 | 1.96464 |
| 510 | 260100 | 132651000 | 22.5832 | 7.9896 | 1.96078 |
| 511 | 261121 | 133432831 | 22.6053 | 7.9948 | 1.95695 |
| 512 | 262144 | 134217728 | 22.6274 | 8.0000 | 1.95312 |
| 513 | 263169 | 135005697 | 22.6495 | 8.0052 | 1.94932 |
| 514 | 264196 | 135796744 | 22.6716 | 8.0104 | 1.94553 |
| 515 | 265225 | 136590875 | 22.6936 | 8.0156 | 1.94175 |

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | - $n$ | $\sqrt{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 516 | 266256 | 137388096 | 22.7156 | 8.0208 | 1.93798 |
| 517 | 267289 | 138188413 | 22.7376 | 8.0260 | 1.93424 |
| 518 | 268324 | 138991832 | 22.7596 | 8.0311 | 1.93050 |
| 519 | 269361 | 139798359 | 22.7816 | 8.0363 | 1.92678 |
| 520 | 270400 | 140608000 | 22.8035 | 8.0415 | 1.92308 |
| 521 | 271441 | 141420761 | 22.8254 | 8.0466 | 1.91939 |
| 522 | 272484 | 142236648 | 22.8473 | 8.0517 | 1.91571 |
| 523 | 273529 | 143055667 | 22.8692 | 8.0569 | 1.91205 |
| 524 | 274576 | 143877824 | 22.8910 | 8.0620 | 1.90840 |
| 525 | 275625 | 144703125 | 22.9129 | 8.0671 | 1.90476 |
| 526 | 276676 | 145531576 | 22.9347 | 8.0723 | 1.90114 |
| 527 | 277729 | 146363183 | 22.9565 | 8.0774 | 1.89753 |
| 528 | 278784 | 147197952 | 22.9783 | 8.0825 | 1.89394 |
| 529 | 279841 | 148035889 | 23.0000 | 8.0876 | 1.89036 |
| 530 | 280900 | 148877000 | 23.0217 | 8.0927 | 1.88679 |
| 531 | 281961 | 149721291 | 23.0434 | 8.0978 | 1.88324 |
| 532 | 283024 | 150568768 | 23.0651 | 8.1028 | 1.87970 |
| 533 | 284089 | 151419437 | 23.0868 | 8.1079 | 1.87617 |
| 534 | 285156 | 152273304 | 23.1084 | 8.1130 | 1.87266 |
| 535 | 286225 | 153130375 | 23.1301 | 8.1180 | 1.86916 |
| 536 | 287296 | 153990656 | 23.1517 | 8.1231 | 1.86567 |
| 537 | 288369 | 154854153 | 23.1733 | 8.1281 | 1.86220 |
| 538 | 289444 | 155720872 | 23.1948 | 8.1332 | 1.85874 |
| 539 | 290521 | 156590819 | 23.2164 | 8.1382 | 1.85529 |
| 540 | 291600 | 157464000 | 23.2379 | 8.1433 | 1.85185 |
| 541 | 292681 | 158340421 | 23.2594 | 8.1483 | 1.84843 |
| 542 | 293764 | 159220088 | 23.2809 | 8.1533 | 1.84502 |
| 543 | 294849 | 160103007 | 23.3024 | 8.1583 | 1.84162 |
| 544 | 295936 | 160989184 | 23.3238 | 8.1633 | 1.83824 |
| 545 | 297025 | 161878625 | 23.3452 | 8.1683 | 1.83486 |
| 546 | 298116 | 162771336 | 23.3666 | 8.1733 | 1.83150 |
| 547 | 299209 | 163667323 | 23.3880 | 8.1783 | 1.82815 |
| 548 | 300304 | 164566592 | 23.4094 | 8.1833 | 1.82482 |
| 549 | 301401 | 165469149 | 23.4307 | 8.1882 | 1.82149 |
| 550 | 302500 | 166375000 | 23.4521 | 8.1932 | 1.81818 |
| 551 | 303601 | 167284151 | 23.4734 | 8.1982 | 1.81488 |
| 552 | 304704 | 168196608 | 23.4947 | 8.2031 | 1.81159 |
| 553 | 305809 | 169112377 | 23.5160 | 8.2081 | 1.80832 |
| 554 | 306916 | 170031464 | 23.5372 | 8.2130 | 1.80505 |
| 555 | 308025 | 170953875 | 23.5584 | 8.2180 | 1.80180 |
| 556 | 309136 | 171879616 | 23.5797 | 8.2229 | 1.79856 |
| 557 | 310249 | 172808693 | 23.6008 | 8.2278 | 1.79533 |
| 558 | 311364 | 173741112 | 23.6220 | 8.2327 | 1.79211 |
| 559 | 312481 | 174676879 | 23.6432 | 8.2377 | 1.78891 |

Mathematical Tables and Formulas

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 560 | 313600 | 175616000 | 23.6643 | 8.2426 | 1.78571 |
| 561 | 314721 | 176558481 | 23.6854 | 8.2475 | 1.78253 |
| 562 | 315844 | 177504328 | 23.7065 | 8.2524 | 1.77936 |
| 563 | 316969 | 178453547 | 23.7276 | 8.2573 | 1.77620 |
| 564 | 318096 | 179406144 | 23.7487 | 8.2621 | 1.77305 |
| 565 | 319225 | 180362125 | 23.7697 | 8.2670 | 1.76991 |
| 566 | 320356 | 181321496 | 23.7908 | 8.2719 | 1.76678 |
| 567 | 321489 | 182284263 | 23.8118 | 8.2768 | 1.76367 |
| 568 | 322624 | 183250432 | 23.8328 | 8.2816 | 1.76056 |
| 569 | 323761 | 184220009 | 23.8537 | 8.2865 | 1.75747 |
| 570 | 324900 | 185193000 | 23.8747 | 8.2913 | 1.75439 |
| 571 | 326041 | 186169411 | 23.8956 | 8.2962 | 1.75131 |
| 572 | 327184 | 187149248 | 23.9165 | 8.3010 | 1.74825 |
| 573 | 328329 | 188132517 | 23.9374 | 8.3059 | 1.74520 |
| 574 | 329476 | 189119224 | 23.9583 | 8.3107 | 1.74216 |
| 575 | 330625 | 190109375 | 23.9792 | 8.3155 | 1.73913 |
| 576 | 331776 | 191102976 | 24.0000 | 8.3203 | 1.73611 |
| 577 | 332929 | 192100033 | 24.0208 | 8.3251 | 1.73310 |
| 578 | 334084 | 193100552 | 24.0416 | 8.3300 | 1.73010 |
| 579 | 335241 | 194104539 | 24.0624 | 8.3348 | 1.72712 |
| 580 | 336400 | 195112000 | 24.0832 | 8.3396 | 1.72414 |
| 581 | 337561 | 196122941 | 24.1039 | 8.3443 | 1.72117 |
| 582 | 338724 | 197137368 | 24.1247 | 8.3491 | 1.71821 |
| 583 | 339889 | 198155287 | 24.1454 | 8.3539 | 1.71527 |
| 584 | 341056 | 199176704 | 24.1661 | 8.3587 | 1.71233 |
| 585 | 342225 | 200201625 | 24.1868 | 8.3634 | 1.70940 |
| 586 | 343396 | 201230056 | 24.2074 | 8.3682 | 1.70649 |
| 587 | 344569 | 202262003 | 24.2281 | 8.3730 | 1.70358 |
| 588 | 345744 | 203297472 | 24.2487 | 8.3777 | 1.70068 |
| 589 | 346921 | 204336469 | 24.2693 | 8.3825 | 1.69779 |
| 590 | 348100 | 205379000 | 24.2899 | 8.3872 | 1.69492 |
| 591 | 349281 | 206425071 | 24.3105 | 8.3919 | 1.69205 |
| 592 | 350464 | 207474688 | 24.3311 | 8.3967 | 1.68919 |
| 593 | 351649 | 208527857 | 24.3516 | 8.4014 | 1.68634 |
| 594 | 352836 | 209584584 | 24.3721 | 8.4061 | 1.68350 |
| 595 | 354025 | 210644875 | 24.3926 | 8.4108 | 1.68067 |
| 596 | 355216 | 211708736 | 24.4131 | 8.4155 | 1.67785 |
| 597 | 356409 | 212776173 | 24.4336 | 8.4202 | 1.67504 |
| 598 | 357604 | 213847192 | 24.4540 | 8.4249 | 1.67224 |
| 599 | 358801 | 214921799 | 24.4745 | 8.4296 | 1.66945 |
| 600 | 360000 | 216000000 | 24.4949 | 8.4343 | 1.66667 |
| 601 | 361201 | 217081801 | 24.5153 | 8.4390 | 1.66389 |
| 602 | 362404 | 218167208 | 24.5357 | 8.4437 | 1.66113 |
| 603 | 363609 | 219256227 | 24.5561 | 8.4484 | 1.65837 |
| 604 | 364816 | 220348864 | 24.5764 | 8.4530 | 1.65563 |
| 605 | 366025 | 221445125 | 24.5967 | 8.4577 | 1.65289 |

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 606 | 367236 | 222545016 | 24.6171 | 8.4623 | 1.65017 |
| 607 | 368449 | 223648543 | 24.6374 | 8.4670 | 1.64745 |
| 608 | 369664 | 224755712 | 24.6577 | 8.4716 | 1.64474 |
| 609 | 370881 | 225866529 | 24.6779 | 8.4763 | 1.64204 |
| 610 | 372100 | 226981000 | 24.6982 | 8.4809 | 1.63934 |
| 611 | 373321 | 228099131 | 24.7184 | 8.4856 | 1.63666 |
| 612 | 374544 | 229220928 | 24.7386 | 8.4902 | 1.63399 |
| 613 | 375769 | 230346397 | 24.7588 | 8.4948 | 1.63132 |
| 614 | 376996 | 231475544 | 24.7790 | 8.4994 | 1.62866 |
| 615 | 378225 | 232608375 | 24.7992 | 8.5040 | 1.62602 |
| 616 | 379456 | 233744896 | 24.8193 | 8.5086 | 1.62338 |
| 617 | 380689 | 234885113 | 24.8395 | 8.5132 | 1.62075 |
| 618 | 381924 | 236029032 | 24.8506 | 8.5178 | 1.61812 |
| 619 | 383161 | 237176659 | 24.8797 | 8.5224 | 1.61551 |
| 620 | 384400 | 238328000 | 24.8998 | 8.5270 | 1.61290 |
| 621 | 385641 | 239483061 | 24.9199 | 8.5316 | 1.61031 |
| 622 | 386884 | 240641848 | 24.9399 | 8.5362 | 1.60772 |
| 623 | 388129 | 241804367 | 24.9600 | 8.5408 | 1.60514 |
| 624 | 389376 | 242970624 | 24.9800 | 8.5453 | 1.60256 |
| 625 | 390625 | 244140625 | 25.0000 | 8.5499 | 1.60000 |
| 626 | 391876 | 245314376 | 25.0200 | 8.5544 | 1.59744 |
| 627 | 393129 | 246491883 | 25.0400 | 8.5590 | 1.59490 |
| 628 | 394384 | 247673152 | 25.0599 | 8.5635 | 1.59236 |
| 629 | 395641 | 248858189 | 25.0799 | 8.5681 | 1.58983 |
| 630 | 396900 | 250047000 | 25.0998 | 8.5726 | 1.58730 |
| 631 | 398161 | 251239591 | 25.1197 | 8.5772 | 1.58479 |
| 632 | 399424 | 252435968 | 25.1396 | 8.5817 | 1.58228 |
| 633 | 400689 | 253636137 | 25.1595 | 8.5862 | 1.57978 |
| 634 | 401956 | 254840104 | 25.1794 | 8.5907 | 1.57729 |
| 635 | 403225 | 256047875 | 25.1992 | 8.5952 | 1.57480 |
| 636 | 404496 | 257259456 | 25.2190 | 8.5997 | 1.57233 |
| 637 | 405769 | 258474853 | 25.2389 | 8.6043 | 1.56986 |
| 638 | 407044 | 259694072 | 25.2587 | 8.6088 | 1.56740 |
| 639 | 408321 | 260917119 | 25.2784 | 8.6132 | 1.56495 |
| 640 | 409600 | 262144000 | 25.2982 | 8.6177 | 1.56250 |
| 641 | 410881 | 263374721 | 25.3180 | 8.6222 | 1.56006 |
| 642 | 412164 | 264609288 | 25.3377 | 8.6267 | 1.55763 |
| 643 | 413449 | 265847707 | 25.3574 | 8.6312 | 1.55521 |
| 644 | 414736 | 267089984 | 25.3772 | 8.6357 | 1.55280 |
| 645 | 416025 | 268336125 | 25.3969 | 8.6401 | 1.55039 |
| 646 | 417316 | 269586136 | 25.4165 | 8.6446 | 1.54799 |
| 647 | 418609 | 270840023 | 25.4362 | 8.6490 | 1.54560 |
| 648 | 419904 | 272097792 | 25.4558 | 8.6535 | 1.54321 |
| 649 | 421201 | 273359449 | 25.4755 | 8.6579 | 1.54083 |

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TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | Vn | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 650 | 422500 | 274625000 | 25.4951 | 8.6624 | 1.53846 |
| 651 | 423801 | 275894451 | 25.5147 | 8.6668 | 1.53610 |
| 652 | 425104 | 277167808 | 25.5343 | 8.6713 | 1.53374 |
| 653 | 426409 | 278445077 | 25.5539 | 8.6757 | 1.53139 |
| 654 | 427716 | 279726264 | 25.5734 | 8.6801 | 1.52905 |
| 655 | 429025 | 281011375 | 25.5930 | 8.6845 | 1.52672 |
| 656 | 430336 | 282300416 | 25.6125 | 8.6890 | 1.52439 |
| 657 | 431649 | 283593393 | 25.6320 | 8.6934 | 1.52207 |
| 658 | 432964 | 284890312 | 25.6515 | 8.6978 | 1.51976 |
| 659 | 434281 | 286191179 | 25.6710 | 8.7022 | 1.51745 |
| 660 | 435600 | 287496000 | 25.6905 | 8.7066 | 1.51515 |
| 661 | 436921 | 288804781 | 25.7099 | 8.7110 | 1.51286 |
| 662 | 438244 | 290117528 | 25.7294 | 8.7154 | 1.51057 |
| 663 | 439569 | 291434247 | 25.7488 | 8.7198 | 1.50830 |
| 664 | 440896 | 292754944 | 25.7682 | 8.7241 | 1.50602 |
| 665 | 442225 | 294079625 | 25.7876 | 8.7285 | 1.50376 |
| 666 | 443556 | 295408296 | 25.8070 | 8.7329 | 1.50150 |
| 667 | 444889 | 296740963 | 25.8263 | 8.7373 | 1.49925 |
| 668 | 446224 | 298077632 | 25.8457 | 8.7416 | 1.49701 |
| 669 | 447561 | 299418309 | 25.8650 | 8.7460 | 1.49477 |
| 670 | 448900 | 300763000 | 25.8844 | 8.7503 | 1.49254 |
| 671 | 450241 | 302111711 | 25.9037 | 8.7547 | 1.49031 |
| 672 | 451584 | 303464448 | 25.9230 | 8.7590 | 1.48810 |
| 673 | 452929 | 304821217 | 25.9422 | 8.7634 | 1.48588 |
| 674 | 454276 | 306182024 | 25.9615 | 8.7677 | 1.48368 |
| 675 | 455625 | 307546875 | 25.9808 | 8.7721 | 1.48148 |
| 676 | 456976 | 308915776 | 26.0000 | 8.7764 | 1.47929 |
| 677 | 458329 | 310288733 | 26.0192 | 8.7807 | 1.47711 |
| 678 | 459684 | 311665752 | 26.0384 | 8.7850 | 1.47493 |
| 679 | 461041 | 313046839 | 26.0576 | 8.7893 | 1.47275 |
| 680 | 462400 | 314432000 | 26.0768 | 8.7937 | 1.47059 |
| 681 | 463761 | 315821241 | 26.0960 | 8.7980 | 1.46843 |
| 682 | 465124 | 317214568 | 26.1151 | 8.8023 | 1.46628 |
| 683 | 466489 | 318611987 | 26.1343 | 8.8066 | 1.46413 |
| 684 | 467856 | 320013504 | 26.1534 | 8.8109 | 1.46199 |
| 685 | 469225 | 321419125 | 26.1725 | 8.8152 | 1.45985 |
| 686 | 470596 | 322828856 | 26.1916 | 8.8194 | 1.45773 |
| 687 | 471969 | 324242703 | 26.2107 | 8.8237 | 1.45560 |
| 688 | 473344 | 325660672 | 26.2298 | 8.8280 | 1.45349 |
| 689 | 474721 | 327082769 | 26.2488 | 8.8323 | 1.45138 |
| 690 | 476100 | 328509000 | 26.2679 | 8.8366 | 1.44928 |
| 691 | 477481 | 329939371 | 26.2869 | 8.8408 | 1.44718 |
| 692 | 478864 | 331373888 | 26.3059 | 8.8451 | 1.44509 |
| 693 | 480249 | 332812557 | 26.3249 | 8.8493 | 1.44300 |
| 694 | 481636 | 334255384 | 26.3439 | 8.8536 | 1.44092 |
| 695 | 483025 | 335702375 | 26.3629 | 8.8578 | 1.43885 |

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TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 696 | 484416 | 337153536 | 26.3818 | 8.8621 | 1.43678 |
| 697 | 485809 | 338608873 | 26.4008 | 8.8663 | 1.43472 |
| 698 | 487204 | 340068392 | 26.4197 | 8.8706 | 1.43267 |
| 699 | 488601 | 341532099 | 26.4386 | 8.8748 | 1.43062 |
| 700 | 490000 | 343000000 | 26.4575 | 8.8790 | 1.42857 |
| 701 | 491401 | 344472101 | 26.4764 | 8.8833 | 1.42653 |
| 702 | 492804 | 345948408 | 26.4953 | 8.8875 | 1.42450 |
| 703 | 494209 | 347428927 | 26.5141 | 8.8917 | 1.42248 |
| 704 | 495616 | 348913664 | 26.5330 | 8.8959 | 1.42046 |
| 705 | 497025 | 350402625 | 26.5518 | 8.9001 | 1.41844 |
| 706 | 498436 | 351895816 | 26.5707 | 8.9043 | 1.41643 |
| 707 | 499849 | 353393243 | 26.5895 | 8.9085 | 1.41443 |
| 708 | 501264 | 354894912 | 26.6083 | 8.9127 | 1.41243 |
| 709 | 502681 | 356400829 | 26.6271 | 8.9169 | 1.41044 |
| 710 | 504100 | 357911000 | 26.6458 | 8.921 I | 1.40845 |
| 711 | 505521 | 359425431 | 26.6646 | 8.9253 | 1.40647 |
| 712 | 506944 | 360944128 | 26.6833 | 8.9295 | 1.40449 |
| 713 | 508369 | 362467097 | 26.7021 | 8.9337 | 1.40253 |
| 714 | 509796 | 363994344 | 26.7208 | 8.9378 | 1.40056 |
| 715 | 511225 | 365525875 | 26.7395 | 8.9420 | 1.39860 |
| 716 | 512656 | 367061696 | 26.7582 | 8.9462 | 1.39665 |
| 717 | 514089 | 368601813 | 26.7769 | 8.9503 | 1.39470 |
| 718 | 515524 | 370146232 | 26.7955 | 8.9545 | 1.39276 |
| 719 | 516961 | 371694959 | 26.8142 | 8.9587 | 1.39082 |
| 720 | 518400 | 373248000 | 26.8328 | 8.9628 | 1.38889 |
| 721 | 519841 | 374805361 | 26.8514 | 8.9670 | 1.38696 |
| 722 | 521284 | 376367048 | 26.8701 | 8.9711 | 1.38504 |
| 723 | 522729 | 377933067 | 26.8887 | 8.9752 | 1.38313 |
| 724 | 524176 | 379503424 | 26.9072 | 8.9794 | 1.38122 |
| 725 | 525625 | 381078125 | 26.9258 | 8.9835 | 1.37931 |
| 726 | 527076 | 382657176 | 26.9444 | 8.9876 | 1.37741 |
| 727 | 528529 | 384240583 | 26.9629 | 8.9918 | 1.37552 |
| 728 | 529984 | 385828352 | 26.9815 | 8.9959 | 1.37363 |
| 729 | 531441 | 387420489 | 27.0000 | 9.0000 | 1.37174 |
| 730 | 532900 | 389017000 | 27.0185 | 9.0041 | 1.36986 |
| 731 | 534361 | 390617891 | 27.0370 | 9.0082 | 1.36799 |
| 732 | 535824 | 392223168 | 27.0555 | 9.0123 | 1.36612 |
| 733 | 537289 | 393832837 | 27.0740 | 9.0164 | 1.36426 |
| 734 | 538756 | 395446904 | 27.0924 | 9.0205 | 1.36240 |
| 735 | 540225 | 397065375 | 27.1109 | 9.0246 | 1.36054 |
| 736 | 541696 | 398688256 | 27.1293 | 9.0287 | 1.35870 |
| 737 | 543169 | 400315553 | 27.1477 | 9.0328 | 1.35685 |
| 738 | 544644 | 401947272 | 27.1662 | 9.0369 | 1.35501 |
| 739 | 546121 | 403583419 | 27.1846 | 9.0410 | 1.35318 |

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 740 | 547600 | 405224000 | 27.2029 | 9.0450 | 1.35135 |
| 741 | 549081 | 406869021 | 27.2213 | 9.0491 | 1.34953 |
| 742 | 550564 | 408518488 | 27.2397 | 9.0532 | 1.34771 |
| 743 | 552049 | 410172407 | 27.2580 | 9.0572 | 1.34590 |
| 744 | 553536 | 411830784 | 27.2764 | 9.0613 | 1.34409 |
| 745 | 555025 | 413493625 | 27.2947 | 9.0654 | 1.34228 |
| 746 | 556516 | 415160936 | 27.3130 | 9.0694 | 1.34048 |
| 747 | 558009 | 416832723 | 27.3313 | 9.0735 | 1.33869 |
| 748 | 559504 | 418508992 | 27.3496 | 9.0775 | 1.33690 |
| 749 | 561001 | 420189749 | 27.3679 | 9.0816 | 1.33511 |
| 750 | 562500 | 421875000 | 27.3861 | 9.0856 | 1.33333 |
| 751 | 564001 | 423564751 | 27.4044 | 9.0896 | 1.33156 |
| 752 | 565504 | 425259008 | 27.4226 | 9.0937 | 1.32979 |
| 753 | 567009 | 426957777 | 27.4408 | 9.0977 | 1.32802 |
| 754 | 568516 | 428661064 | 27.4591 | 9.1017 | 1.32626 |
| 755 | 570025 | 430368875 | 27.4773 | 9.1057 | 1.32450 |
| 756 | 571536 | 432081216 | 27.4955 | 9.1098 | 1.32275 |
| 757 | 573049 | 433798093 | 27.5136 | 9.1138 | 1.32100 |
| 758 | 574564 | 435519512 | 27.5318 | 9.1178 | 1.31926 |
| 759 | 576081 | 437245479 | 27.5500 | 9.1218 | 1.31752 |
| 760 | 577600 | 438976000 | 27.5681 | 9.1258 | 1.31579 |
| 761 | 579121 | 440711081 | 27.5862 | 9.1298 | 1.31406 |
| 762 | 580644 | 442450728 | 27.6043 | 9.1338 | 1.31234 |
| 763 | 582169 | 444194947 | 27.6225 | 9.1378 | 1.31062 |
| 764 | 583696 | 445943744 | 27.6405 | 9.1418 | 1.30890 |
| 765 | 585225 | 447697125 | 27.6586 | 9.1458 | 1.30719 |
| 766 | 586756 | 449455096 | 27.6767 | 9.1498 | 1.30548 |
| 767 | 588289 | 451217663 | 27.6948 | 9.1537 | 1.30378 |
| 768 | 589824 | 452984832 | 27.7128 | 9.1577 | 1.30208 |
| 769 | 591361 | 454756609 | 27.7308 | 9.1617 | 1.30039 |
| 770 | 592900 | 456533000 | 27.7489 | 9.1657 | 1.29870 |
| 771 | 594441 | 458314011 | 27.7669 | 9.1696 | 1.29702 |
| 772 | 595984 | 460099648 | 27.7849 | 9.1736 | 1.29534 |
| 773 | 597529 | 461889917 | 27.8029 | 9.1775 | 1.29366 |
| 774 | 599076 | 463684824 | 27.8209 | 9.1815 | 1.29199 |
| 775 | 600625 | 465484375 | 27.8388 | 9.1855 | 1.29032 |
| 776 | 602176 | 467288576 | 27.8568 | 9.1894 | 1.28866 |
| 777 | 603729 | 469097433 | 27.8747 | 9.1933 | 1.28700 |
| 778 | 605284 | 470910952 | 27.8927 | 9.1973 | 1. 28535 |
| 779 | 606841 | 472729139 | 27.9106 | 9.2012 | 1.28370 |
| 780 | 608400 |  | 27.9285 | 9.2052 |  |
| 781 | 609961 | 476379541 | 27.9464 | 9.2091 | 1.28041 |
| 782 | 611524 | 478211768 | 27.9643 | 9.2130 | 1.27877 |
| 783 | 613089 | 480048687 | 27.9821 | 9.2170 | 1.27714 |
| 784 | 614656 | 481890304 | 28.0000 | 9.2209 | 1.27551 |
| 785 | 616225 | 483736625 | 28.0179 | 9.2248 | 1.27389 |

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TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 786 | 617796 | 485587656 | 28.0357 | 9.2287 | 1.27226 |
| 787 | 619369 | 487443403 | 28.0535 | 9.2326 | 1.27065 |
| 788 | 620944 | 489303872 | 28.0713 | 9.2365 | 1.26904 |
| 789 | 622521 | 491169069 | 28.0891 | 9.2404 | 1.26743 |
| 790 | 624100 | 493039000 | 28.1069 | 9.2443 | 1.26582 |
| 791 | 625681 | 494913671 | 28.1247 | 9.2482 | 1.26422 |
| 792 | 627264 | 496793088 | 28.1425 | 9.2521 | 1.26263 |
| 793 | 628849 | 498677257 | 28.1603 | 9.2560 | 1.26103 |
| 794 | 630436 | 500566184 | 28.1780 | 9.2599 | 1.25945 |
| 795 | 632025 | 502459875 | 28.1957 | 9.2638 | 1.25786 |
| 796 | 633616 | 504358336 | 28.2135 | 9.2677 | 1.25628 |
| 797 | 635209 | 506261573 | 28.2312 | 9.2716 | 1.25471 |
| 798 | 636804 | 508169592 | 28.2489 | 9.2754 | 1.25313 |
| 799 | 638401 | 510082399 | 28.2666 | 9.2793 | 1.25156 |
| 800 | 640000 | 512000000 | 28.2843 | 9.2832 | 1.25000 |
| 801 | 641601 | 513922401 | 28.3019 | 9.2870 | 1.24844 |
| 802 | 643204 | 515849608 | 28.3196 | 9.2909 | 1.24688 |
| 803 | 644809 | 517781627 | 28.3373 | 9.2948 | 1.24533 |
| 804 | 646416 | 519718464 | 28.3549 | 9.2986 | 1.24378 |
| 805 | 648025 | 521660125 | 28.3725 | 9.3025 | 1.24224 |
| 806 | 649636 | 523606616 | 28.3901 | 9.3063 | 1.24069 |
| 807 | 651249 | 525557943 | 28.4077 | 9.3102 | 1.23916 |
| 808 | 652864 | 527514112 | 28.4253 | 9.3140 | 1.23762 |
| 809 | 654481 | 529475129 | 28.4429 | 9.3179 | 1.23609 |
| 810 | 656100 | 531441000 | 28.4605 | 9.3217 | 1.23457 |
| 811 | 657721 | 533411731 | 28.4781 | 9.3255 | 1.23305 |
| 812 | $659344$ | 535387328 | 28.4956 | 9.3294 | 1.23153 |
| 813 | 660969 | 537367797 | 28.5132 | 9.3332 | 1.23001 |
| 814 | 662596 | 539353144 | 28.5307 | 9.3370 | 1.22850 |
| 815 | $664225$ | 541343375 | 28.5482 | 9.3408 | 1.22699 |
| 816 | 665856 | 543338496 | 28.5657 | 9.3447 | 1.22549 |
| 817 | 667489 | 545338513 | 28.5832 | 9.3485 | 1.22399 |
| 818 | 669124 | 547343432 | 28.6007 | 9.3523 | 1.22249 |
| 819 | 670761 | 549353259 | 28.6182 | 9.3561 | 1.22100 |
| 820 | 672400 | 551368000 | 28.6356 | 9.3599 | 1.21951 |
| 821 | 674041 | 553387661 | 28.6531 | 9.3637 | 1.21803 |
| 822 | 675684 | 555412248 | 28.6705 | 9.3675 | 1.21655 |
| 823 | 677329 | 557441767 | 28.6880 | 9.3713 | 1.21507 |
| 824 | 678976 | 559476224 | 28.7054 | 9.3751 | 1.21359 |
| 825 | 680625 | 561515625 | 28.7228 | 9.3789 | 1.21212 |
| 826 | 682276 | 563559976 | 28.7402 | 9.3827 | 1.21065 |
| 827 | 683929 | 565609283 | 28.7576 | 9.3865 | 1.20919 |
| 828 | 685584 | 567663552 | 28.7750 | 9.3902 | 1.20773 |
| 829 | 687241 | 569722789 | 28.7924 | 9.3940 | 1.20627 |

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TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 830 | 688900 | 571787000 | 28.8097 | 9.3978 | 1.20482 |
| 831 | 690561 | 573856191 | 28.8271 | 9.4016 | 1.20337 |
| 832 | 692224 | 575930368 | 28.8444 | 9.4053 | 1.20192 |
| 833 | 693889 | 578009537 | 28.8617 | 9.4091 | 1.20048 |
| 834 | 695556 | 580093704 | 28.8791 | 9.4129 | 1.19904 |
| 835 | 697225 | 582182875 | 28.8964 | 9.4166 | 1.19760 |
| 836 | 698896 | 584277056 | 28.9137 | 9.4204 | 1.19617 |
| 837 | 700569 | 586376253 | 28.9310 | 9.4241 | 1.19474 |
| 838 | 702244 | 588480472 | 28.9482 | 9.4279 | 1.19332 |
| 839 | 703921 | 590589719 | 28.9655 | 9.4316 | 1.19189 |
| 840 | 705600 | 592704000 | 28.9828 | 9.4354 | 1.19048 |
| 841 | 707281 | 594823321 | 29.0000 | 9.4391 | 1.18906 |
| 842 | 708964 | 596947688 | 29.0172 | 9.4429 | 1.18765 |
| 843 | 710649 | 599077107 | 29.0345 | 9.4466 | 1.18624 |
| 844 | 712336 | 601211584 | 29.0517 | 9.4503 | 1.18483 |
| 845 | 714025 | 603351125 | 29.0689 | 9.4541 | 1.18343 |
| 846 | 715716 | 605495736 | 29.0861 | 9.4578 | 1.18203 |
| 847 | 717409 | 607645423 | 29.1033 | 9.4615 | 1.18064 |
| 848 | 719104 | 609800192 | 29.1204 | 9.4652 | 1.17925 |
| 849 | 720801 | 611960049 | 29.1376 | 9.4690 | 1.17786 |
| 850 | 722500 | 614125000 | 29.1548 | 9.4727 | 1.17647 |
| 851 | 724201 | 616295051 | 29.1719 | 9.4764 | 1.17509 |
| 852 | 725904 | 618470208 | 29.1890 | 9.4801 | 1.17371 |
| 853 | 727609 | 620650477 | 29.2062 | 9.4838 | 1.17233 |
| 854 | 729316 | 622835864 | 29.2233 | 9.4875 | 1.17096 |
| 855 | 731025 | 625026375 | 29.2404 | 9.4912 | 1.16959 |
| 856 | 732736 | 627222016 | 29.2575 | 9.4949 | 1.16822 |
| 857 | 734449 | 629422793 | 29.2746 | 9.4986 | 1.16686 |
| 858 | 736164 | 631628712 | 29.2916 | 9.5023 | 1.16550 |
| 859 | 737881 | 633839779 | 29.3087 | 9.5060 | 1.16414 |
| 860 | 739600 | 636056000 | 29.3258 | 9.5097 | 1.16279 |
| 861 | 741321 | 638277381 | 29.3428 | 9.5134 | 1.16144 |
| 862 | 743044 | 640503928 | 29.3598 | 9.5171 | 1.16009 |
| 863 | 744769 | 642735647 | 29.3769 | 9.5207 | 1.15875 |
| 864 | 746496 | 644972544 | 29.3939 | 9.5244 | 1.15741 |
| 865 | 748225 | 647214625 | 29.4109 | 9.5281 | 1.15607 |
| 866 | 749956 | 649461896 | 29.4279 | 9.5317 | 1.15473 |
| 867 | 751689 | 651714363 | 29.4449 | 9.5354 | 1.15340 |
| 868 | 753424 | 653972032 | 29.4618 | 9.5391 | 1.15207 |
| 869 | 755161 | 656234909 | 29.4788 | 9.5427 | 1.15075 |
| 870 | 756900 | 658503000 | 29.4958 | 9.5464 | 1.14943 |
| 871 | 758641 | 660776311 | 29.5127 | 9.5501 | 1.14811 |
| 872 | 760384 | 663054848 | 29.5296 | 9.5537 | 1.14679 |
| 873 | 762129 | 665338617 | 29.5466 | 9.5574 | 1.14548 |
| 874 | 763876 | 667627624 | 29.5635 | 9.5610 | 1.14416 |
| 875 | 765625 | 669921875 | 29.5804 | 9.5647 | 1.14286 |

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TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{\prime}$ | $n^{\text {a }}$ | $\sqrt{n}$ | [ $n$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 876 | 767376 | 672221376 | 29.5973 | 9.5683 | 1.14155 |
| 877 | 769129 | 674526133 | 29.6142 | 9.5719 | 1.14025 |
| 878 | 770884 | 676836152 | 29.6311 | 9.5756 | 1.13895 |
| 879 | 772641 | 679151439 | 29.6479 | 9.5792 | 1.13766 |
| 880 | 774400 | 681472000 | 29.6648 | 9.5828 | 1.13636 |
| 881 | 776161 | 683797841 | 29.6816 | 9.5865 | 1.13507 |
| 882 | 777924 | 686128968 | 29.6985 | 9.5901 | 1.13379 |
| 883 | 779689 | 688465387 | 29.7153 | 9.5937 | 1.13250 |
| 884 | 781456 | 690807104 | 29.7321 | 9.5973 | 1.13122 |
| 885 | 783225 | 693154125 | 29.7489 | 9.6010 | 1.12994 |
| 886 | 784996 | 695506456 | 29.7658 | 9.6046 | 1.12867 |
| 887 | 786769 | 697864103 | 29.7825 | 9.6082 | 1.12740 |
| 888 | 788544 | 700227072 | 29.7993 | 9.6118 | 1.12613 |
| 889 | 790321 | 702595369 | 29.8161 | 9.6154 | 1.12486 |
| 890 | 792100 | 704969000 | 29.8329 | 9.6190 | 1.12360 |
| 891 | 793881 | 707347971 | 29.8496 | 9.6226 | 1.12233 |
| 892 | 795664 | 709732288 | 29.8664 | 9.6262 | 1.12108 |
| 893 | 797449 | 712121957 | 29.8831 | 9.6298 | 1.11982 |
| 894 | 799236 | 714516984 | 29.8998 | 9.6334 | 1.11857 |
| 895 | 801025 | 716917375 | 29.9166 | 9.6370 | 1.11732 |
| 896 | 802815 | 719323136 | 29.9333 | 9.6406 | 1.11607 |
| 897 | 804609 | 721734273 | 29.9500 | 9.6442 | 1.11483 |
| 898 | 806404 | 724150792 | 29.9666 | 9.6477 | 1.11359 |
| 899 | 808201 | 726572699 | 29.9833 | 9.6513 | 1.11235 |
| 900 | 810000 | 729000000 | 30.0000 | 9.6549 | 1.11111 |
| 901 | 811801 | 731432701 | 30.0167 | 9.6585 | 1.10988 |
| 902 | 813604 | 733870808 | 30.0333 | 9.6620 | 1.10865 |
| 903 | 815409 | 736314327 | 30.0500 | 9.6656 | 1.10742 |
| 904 | 817216 | 738763264 | 30.0666 | 9.6692 | 1.10619 |
| 905 | 819025 | 741217625 | 30.0832 | 9.6727 | 1.10497 |
| 906 | 820836 | 743677416 | 30.0998 | 9.6763 | 1.10375 |
| 907 | 822649 | 746142643 | 30.1164 | 9.6799 | 1.10254 |
| 908 | 824464 | 748613312 | 30.1330 | 9.6834 | 1.10132 |
| 909 | 826281 | 751089429 | 30.1496 | 9.6870 | 1.10011 |
| 910 | 828100 | 753571000 | 30.1662 | 9.6905 | 1.09890 |
| 911 | 829921 | 756058031 | 30.1828 | 9.6941 | 1.09769 |
| 912 | 831744 | 758550528 | 30.1993 | 9.6976 | 1.09649 |
| 913 | 833569 | 761048497 | 30.2159 | 9.7012 | 1.09529 |
| 914 | 835396 | 763551944 | 30.2324 | 9.7047 | 1.09409 |
| 915 | 837225 | 766060875 | 30.2490 | 9.7082 | 1.09290 |
| 916 | 839056 | 768575296 | 30.2655 | 9.7118 | 1.09170 |
| 917 | 840889 | 771095213 | 30.2820 | 9.7153 | 1.09051 |
| 918 | 842724 | 773620632 | 30.2985 | 9.7188 | 1.08932 |
| 919 | 844561 | 776151559 | 30.3150 | 9.7224 | 1.08814 |

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n$ |  |  | 1. | 1.7 |
| :---: | :---: | :---: | :---: | :---: | :---: |

TABLE 6-10 Cont.
Squares, Cubes, Square Roots, Cube Roots, and Reciprocals

| $n$ | $n^{2}$ | $n^{3}$ | $\sqrt{n}$ | $\sqrt[3]{n}$ | $\frac{1000}{n}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 966 | 933156 | 901428696 | 31.0805 | 9.8854 | 1.03520 |
| 967 | 935089 | 904231063 | 31.0966 | 9.8888 | 1.03413 |
| 968 | 937024 | 907039232 | 31.1127 | 9.8922 | 1.03306 |
| 969 | 938961 | 909853209 | 31.1288 | 9.8956 | 1.03199 |
| 970 | 940900 | 912673000 | 31.1448 | 9.8990 | 1.03093 |
| 971 | 942841 | 915498611 | 31.1609 | 9.9024 | 1.02987 |
| 972 | 944784 | 918330048 | 31.1769 | 9.9058 | 1.02881 |
| 973 | 946729 | 921167317 | 31.1929 | 9.9092 | 1.02775 |
| 974 | 948676 | 924010424 | 31.2090 | 9.9126 | 1.02669 |
| 975 | 950625 | 926859375 | 31.2250 | 9.9160 | 1.02564 |
| 976 | 952576 | 929714176 | 31.2410 | 9.9194 | 1.02459 |
| 977 | 954529 | 932574833 | 31.2570 | 9.9227 | 1.02354 |
| 978 | 956484 | 935441352 | 31.2730 | 9.9261 | 1.02249 |
| 979 | 958441 | 938313739 | 31.2890 | 9.9295 | 1.02145 |
| 980 | 960400 | 941192000 | 31.3050 | 9.9329 | 1.02041 |
| 981 | 962361 | 944076141 | 31.3209 | 9.9363 | 1.01937 |
| 982 | 964324 | 946966168 | 31.3369 | 9.9396 | 1.01833 |
| 983 | 966289 | 949862087 | 31.3528 | 9.9430 | 1.01729 |
| 984 | 968256 | 952763904 | 31.3688 | 9.9464 | 1.01626 |
| 985 | 970225 | 955671625 | 31.3847 | 9.9497 | 1.01523 |
| 986 | 972196 | 958585256 | 31.4006 | 9.9531 | 1.01420 |
| 987 | 974169 | 961504803 | 31.4166 | 9.9565 | 1.01317 |
| 988 | 976144 | 964430272 | 31.4325 | 9.9598 | 1.01215 |
| 989 | 978121 | 967361669 | 31.4484 | 9.9632 | 1.01112 |
| 990 | 980100 | 970299000 | 31.4643 | 9.9666 | 1.01010 |
| 991 | 982081 | 973242271 | 31.4802 | 9.9699 | 1.00908 |
| 992 | 984064 | 976191488 | 31.4960 | 9.9733 | 1.00806 |
| 993 | 986049 | 979146657 | 31.5119 | 9.9766 | 1.00705 |
| 994 | 988036 | 982107784 | 31.5278 | 9.9800 | 1.00604 |
| 995 | 990025 | 985074875 | 31.5436 | 9.9833 | 1.00503 |
| 996 | 992016 | 988047936 | 31.5595 | 9.9866 | 1.00402 |
| 997 | 994009 | 991026973 | 31.5753 | 9.9900 | 1.00301 |
| 998 | 996004 | 994011992 | 31.5911 | 9.9933 | 1.00200 |
| 999 | 998001 | 997002999 | 31.6070 | 9.9967 | 1.00100 |
| 1000 | 1000000 | 1000000000 | 31.6228 | 10.0000 | 1.00000 |

## Chapter 7

## Miscellaneous

## TEMPERATURE CONVERSION

The nomograph in Fig. 7-1 can be used to convert from degrees Fahrenheit to degrees Celsius (or vice versa) for any temperature between absolute zero and $540^{\circ} \mathrm{F}$ $\left(281^{\circ} \mathrm{C}\right)$. The term Celsius was officially adopted, in place of centigrade, by international agreement in 1948. Actually, Celsius and centigrade scales differ slightly-the Celsius scale is based on $0^{\circ}$ at the triple point of water $\left(0.01^{\circ} \mathrm{C}\right)$, and centigrade has $0^{\circ}$ at the freezing point of water. For all practical purposes, though, the two terms are interchangeable.

Two absolute temperature scales are also in use. The Fahrenheit absolute scale is called the Rankine- $0^{\circ} \mathrm{R}=-459.67^{\circ} \mathrm{F}$. The Celsius absolute scale is the Kelvin- $0 \mathrm{~K}=$ $-273.16^{\circ} \mathrm{C}$. Note the degree sign $\left({ }^{\circ}\right)$ is not used with Kelvin, the SI unit of temperature.

The following formulas can be used to convert from any temperature to the other:

$$
\begin{aligned}
& { }^{\circ} \mathrm{F}=\left({ }^{\circ} \mathrm{C} \times 9 / 5\right)+32 \\
& { }^{\circ} \mathrm{F}={ }^{\circ} \mathrm{R}-459.67
\end{aligned}
$$

$$
\begin{aligned}
{ }^{\circ} \mathrm{F} & =9 / 5(\mathrm{~K}-273.16)+32 \\
{ }^{\circ} \mathrm{C} & =5 / 9\left({ }^{\circ} \mathrm{F}-32\right) \\
{ }^{\circ} \mathrm{C} & =\mathrm{K}-273.16 \\
{ }^{\circ} \mathrm{C} & =5 / 9\left({ }^{\circ} \mathrm{R}-491.67\right) \\
{ }^{\circ} \mathrm{R} & ={ }^{\circ} \mathrm{F}+459.67 \\
{ }^{\circ} \mathrm{R} & =\left({ }^{\circ} \mathrm{C} \times 9 / 5\right)+491.67 \\
{ }^{\circ} \mathrm{R} & =9 / 5(\mathrm{~K}-273.16)+491.67 \\
\mathrm{~K} & ={ }^{\circ} \mathrm{C}+273.16 \\
\mathrm{~K} & =5 / 9\left({ }^{\circ} \mathrm{F}-32\right)+273.16 \\
\mathrm{~K} & =5 / 9\left({ }^{\circ} \mathrm{R}-491.67\right)+273.16
\end{aligned}
$$

## TELEPRINTER CODES

Letter and figure assignments for teleprinter codes are given in Table 7-1.

合


合

只

Fig．7－1．Temperature nomograph．

TABLE 7-1
Moore ARQ Code (Compared with Five-Unit Teleprinter Code)

| Code assignments |  | Moore ARQ code | Five-unit TTY code |
| :---: | :---: | :---: | :---: |
| letters case | Figures case | $\begin{gathered} \text { Bit } \\ \text { numbers } \\ 765432 I \end{gathered}$ | $\begin{gathered} \text { Bit } \\ \text { numbers } \end{gathered}$ $54321$ |
| blank | blank | 1110000 | 00000 |
| E | 3 | 0001110 | 00001 |
| line feed | line feed | 0001101 | 00010 |
| A | - | 0101100 | 00011 |
| space | space | 0001011 | 00100 |
| S | apostrophe | 0101010 | 00101 |
|  | 8 | 0000111 | 00110 |
| U | 7 | 0100110 | 00111 |
| carriage retur | carriage return | 1100001 | 01000 |
| D | ( ${ }^{\text {P }}$ | 0011100 | 01001 |
| R | 4 | 0010011 | 01010 |
| J | bell | 1100010 | 01011 |
| N | comma | 0010101 | 01100 |
| F | [ | 1100100 | 01101 |
| C | : | 0011001 | 01110 |
| K | ( | 1101000 | 01111 |
| T | 5 | 1010001 | 10000 |
| Z | + | 1000110 | 10001 |
| L | ) | 0100011 | 10010 |
| W | 2 | 1010010 | 10011 |
| H | $\lceil$ | 0100101 | 10100 |
| Y | 6 | 1010100 | 10101 |
| P | 0 | 0101001 | 10110 |
| Q | 1 | 1011000 | 10111 |
| O | 9 | 0110001 | 11000 |
| B | ? | 1001100 | 11001 |
| G | L | 1000011 | 11010 |
| figures | figures | 0110010 | 11011 |
| M |  | 1000101 | 11100 |
| X | 1 | 0110100 | 11101 |
| V | = | 1001001 | 11110 |
| letters | letters | 0111000 | 11111 |
| signal 1 | signal 1 | 0010110 |  |
| idle $\alpha$ | idle $\alpha$ | 1001010 |  |
| idle $\beta$ | idle $\beta$ | 0011010 |  |

Note: Transmission Order: Bit $1 \rightarrow$ Bit 7 .

## ASCII CODE

The American Standard Code for Information Interchange (ASCII) Code is used extensively in computer data transmission. The ASCII Code, which is produced by most computer keyboards, is shown in Table 7-2.

## KANSAS CITY STANDARD

The Kansas City standard is a widely used digital tape format, consisting of l's represented by eight cycles of 2400 Hz , and 0 's represented by four cycles of 1200 Hz (Fig. 7-2). It is a frequency-shift keying (FSK) mode of operation using tone bursts. A variation of the Kansas City standard employs the same frequencies for 1 and 0 , but with different durations. Each bit starts with a $3700-\mathrm{Hz}$ frequency and ends with a $2400-\mathrm{Hz}$ frequency, and each bit has the same duration ( 7.452 ms ). However, a 1 has its frequency-transition point one-third from the start of the burst, whereas a 0 has its frequency-transition point two-thirds from the start of the burst.


Fig. 7-2

TABLE 7-2
The ASCII Code


## CHARACTERISTICS OF THE ELEMENTS

A list of all the known elements (105) is given in Table 7-3. The symbol, atomic
number, and atomic weight are included for each element. Where known, the melting and boiling points of each element are also given.

TABLE 7-3
Characteristics of the Elements

| Element | Symbol | Atomic <br> number | Atomic <br> weight | Melting <br> point $\left({ }^{\circ} \mathrm{C}\right)$ | Boiling <br> point $\left({ }^{\circ} \mathrm{C}\right)$ | Density <br> $\left(\mathbf{2 0}{ }^{\circ} \mathrm{C}\right)$ <br> $\left(\mathrm{g} / \mathrm{cm}^{3}\right)$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| actinium | Ac | 89 | $227^{*}$ | 1050 | 3220 |  |
| aluminum | Al | 13 | 26.97 | 660.1 | 2467 |  |
| americium | Am | 95 | $243^{*}$ | 1000 | 7600 | 2.70 |
| antimony | Sb | 51 | 121.76 | 630.5 | 1380 |  |
| argon | A | 18 | 39.944 | -189.2 | -185.7 | 6.62 |
| arsenic | As | 33 | 74.91 | $(820)^{\ddagger}$ | 615 | $1.78^{\dagger}$ |
| astatine | At | 85 | $210^{*}$ | - | 5.73 |  |
| barium | Ba | 56 | 137.36 | 725 | 1140 |  |
| berkelium | Bk | 97 | $247^{*}$ | - | - | 3.50 |
| beryllium | Be | 4 | 9.013 | 1350 | 2970 |  |
| bismuth | Bi | 83 | 209.00 | 271.3 | 1560 | 1.82 |
| boron | B | 5 | 10.82 | 2300 | 2550 | 9.80 |

TABLE 7-3 Cont.
Characteristics of the Elements

| Element | Symbol | Atomic number | Atomic weight | Melting point ( ${ }^{\circ} \mathrm{C}$ ) | $\begin{gathered} \text { Boiling } \\ \text { point }\left({ }^{\circ} \mathrm{C}\right) \end{gathered}$ | Density $\left(20^{\circ} \mathrm{C}\right)$ (g/cm ${ }^{3}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| bromine | Br | 35 | 79.916 | -7.2 | 58.8 | 3.12 |
| cadmium | Cd | 48 | 112.41 | 320.9 | 766 | 8.65 |
| calcium | Ca | 20 | 40.08 | 850 | 1487 | 1.54 |
| californium | Cf | 98 | 251* | - |  | - |
| carbon | C | 6 | 12.01 | $>3500^{\text {s }}$ | 4827 | 2.22 |
| cerium | Ce | 58 | 140.13 | 795 | 3468 | 6.90 |
| cesium | Cs | 55 | 132.91 | 28 | 670 | 1.87 |
| chlorine | Cl | 17 | 35.457 | -101.6 | -34.7 | $3.21{ }^{1}$ |
| chromium | Cr | 24 | 52.01 | 1890 | 2482 | 7.14 |
| cobalt | Co | 27 | 58.94 | 1492 | 3000 | 8.90 |
| copper | Cu | 29 | 63.54 | 1083 | 2595 | 8.96 |
| curium | Cm | 96 | 247 | - | - | - |
| dysprosium | Dy | 66 | 162.46 | 1400 | 2600 | - |
| einstcinium | E | 99 | 254* | - | - | - |
| erbium | Er | 68 | 167.2 | 1497 | 2900 | - |
| europium | Eu | 63 | 152.0 | 826 | 1439 | - |
| fermium | Fm | 100 | 255* | - | - | - |
| fluorine | F | 9 | 19.00 | -223 | -188.14 | $1.69\left(15^{\circ}\right)^{\text {r }}$ |
| francium | Fr | 87 | 233* | - | - | - |
| gadolinium | Gd | 64 | 156.9 | 1312 | 3000 | - |
| gallium | Ga | 31 | 69.72 | 29.7 | 2403 | 5.91 |
| germanium | Ge | 32 | 72.60 | 958.5 | (2700) ${ }^{\text {t }}$ | 5.36 |
| gold | Au | 79 | 197.0 | 1063 | 2966 | 19.30 |
| hafnium | Hf | 72 | 178.6 | 2150 | 5400 | 11.40 |
| hahmium | Ha | 105 | 262* | - | - | - |
| helium | He | 2 | 4.003 | $<-271.4^{5}$ | -268.94 | $0.164^{*}$ |
| holmium | Ho | 67 | 164.94 | 1461 | 2600 | - |
| hydrogen | H | 1 | 1.0080 | -259.14 | -252.8 | $0.08375^{\dagger}$ |
| indium | 1 n | 49 | 114.76 | 155 | 2000 | 7.31 |
| iodine | 1 | 53 | 126.91 | 113.5 | 184.35 | 4.93 |
| iridium | Ir | 77 | 192.2 | 2443 | 4500 | 22.4 |
| iron | Fe | 26 | 55.85 | 1533 | 3000 | 7.87 |
| krypton | Kr | 36 | 83.8 | -156.6 | -151.8 | $3.448^{\text { }}$ |
| lanthanum | La | 57 | 138.92 | 920 | 3469 | 6.15 |
| lawrencium | L.w | 103 | 257* | - | - | - |
| lead | Pb | 82 | 207.21 | 327.4 | 1744 | 11.34 |
| lithium | Li | 3 | 6.940 | 186 | 1317 | 0.53 |
| lutetium | Lu | 71 | 174.99 | 1652 | 3327 | - |
| magnesium | Mg | 12 | 24.32 | 651 | 1100 | 1.74 |
| manganese | Mn | 25 | 54.94 | 1260 | 2097 | 7.44 |
| mendelevium | M | 101 | 256* | - | - | - |
| mercury | Hg | 80 | 200.61 | -38.87 | 356.9 | 13.55 |
| molybdenum | Mo | 42 | 95.95 | 2620 | 5660 | 10.20 |
| neodymium | Nd | 60 | 144.27 | 1024 | 3027 |  |
| neon | Ne | 10 | 20.183 | -248.67 | -245.9 | $0.8387^{\dagger}$ |
| neptunium | Np | 93 | 237* | 639 | - | - |
| nickel | Ni | 28 | 58.69 | 1453 | 2900 | 8.90 |
| niobium | Nb | 41 | 92.91 | 2500 | 4927 | 8.57 |
| nitrogen | N | 7 | 14.008 | -209.86 | -195.81 | $1.1649^{+}$ |
| nobelium | No | 102 | 253 | - | - |  |

TABLE 7-3 Cont.
Characteristics of the Elements

| Element S | Symbol | Atomic number | Atomic weight | Melting point ( ${ }^{\circ} \mathrm{C}$ ) | Boiling point ( ${ }^{\circ} \mathrm{C}$ ) | Density $\begin{gathered} \left(20^{\circ} \mathrm{C}\right) \\ \left(\mathrm{g} / \mathrm{cm}^{3}\right) \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| osmium | Os | 76 | 190.2 | 2700 | $(>5300)^{\mathrm{f}^{\frac{1}{3}}}$ | 22.48 |
| oxygen | O | 8 | 16.000 | -218.4 | -183 | $1.3318{ }^{1}$ |
| palladium | Pd | 46 | 106.7 | 1552 | 2927 | 12.00 |
| phosphorus | P | 15 | 30.975 | 44.1 | 280 | 1.82 |
| platinum | Pt | 78 | 195.23 | 1769 | 3800 | 21.45 |
| plutonium | Pu | 94 | 244 | 639 | 3250 | - |
| polonium | $\mathrm{P}_{0}$ | 84 | 210 | 250 | 960 | - |
| potassium | K | 19 | 39.100 | 62.3 | 760 | 0.86 |
| praseodymium | Pr | 59 | 140.92 | 940 | 3127 | 6.63 |
| promethium | Pm | 61 | 145* | 1035 | 2730 | - |
| protactinium | Pa | 91 | 231* | 1225 | - | - |
| radium | Ra | 88 | 226.05 | 700 | 1140 | 5.00 |
| radon | Rn | 86 | 222 | -76 | -62 | $4.40{ }^{1}$ |
| rhenium | Re | 75 | 186.31 | (3000) ${ }^{\text {: }}$ | 5627 | 20.00 |
| rhodium | Rh | 45 | 102.91 | 1960 | 3960 | 12.44 |
| rubidium | Rb | 37 | 85.48 | 38.5 | 700 | 1.53 |
| ruthenium | Ru | 44 | 101.1 | 2500 | 4111 | 12.2 |
| rutherfordium or | $\left.\begin{array}{l} \mathrm{Ri} \\ \mathrm{or} \end{array}\right\}$ | 104 | $260 *$ | - | - | - |
| kurchatonium Ku |  |  |  |  |  |  |
| samarium | Sm | 62 | 150.43 | $>1300^{5}$ | 1900 | 7.70 |
| scandium | Sc | 21 | 44.96 | 1539 | 2727 | 2.50 |
| sclenium | Se | 34 | 78.96 | 220 | 688 | 4.81 |
| silicon | Si | 14 | 28.09 | 1420 | 2355 | 2.40 |
| silver | Ag | 47 | 107.880 | 960.8 | 2212 | 10.49 |
| sodium | Na | 11 | 22.997 | 97.5 | 880 | 0.97 |
| strontium | Sr | 38 | 87.63 | 880 | 1384 | 2.60 |
| sulfur | S | 16 | 32.066 | 112.8 | 444.6 | 2.07 |
| tantalum | Ta | 73 | 180.95 | 3005 | 5425 | 16.60 |
| technetium | Tc | 43 | 97* | 2140 | - | - |
| tellurium | Te | 52 | 127.61 | 452 | 989.8 | 6.24 |
| terbium | Ib | 65 | 158.93 | 1356 | 2550 | - |
| thallium | T1 | 81 | 204.39 | 303.5 | 1457 | 11.85 |
| thorium | Th | 90 | 232.12 | 1845 | $>3000 \%$ | 11.50 |
| thulium | Tm | 69 | 168.94 | 1545 | 1727 | - |
| tin | Sn | 50 | 118.70 | 231.9 | 2260 | 7.30 |
| titanium | Ti | 22 | 47.90 | 1820 | $(>3000):$ ¢ | 4.54 |
| tungsten | W | 74 | 183.92 | 3380 | 5900 | 19.30 |
| uranium | U | 92 | 238.07 | 1133 | 3818 | 18.70 |
| vanadium | V | 23 | 50.95 | 1735 | (3000) ${ }^{\text {4 }}$ | 5.68 |
| xenon | Xe | 54 | 131.3 | -111.9 | -109.1 | $5.495{ }^{\dagger}$ |
| ytterbium | Yb | 70 | 173.04 | 875 | 1450 | - |
| yttrium | Y | 39 | 88.92 | 1490 | (2500) ${ }^{\text {a }}$ | 5.51 |
| zinc | Zn | 30 | 65.38 | 419.47 | 907 | 7.14 |
| zirconium | Zr | 40 | 91.22 | 1852 | 3578 | 6.40 |

[^9]MEASURES AND WEIGHTS
Linear Measure

| 1 inch | $=1000$ mils |
| :--- | :--- |
| 1 hand | $=4$ inches |
| 1 foot | $=12$ inches |
| 1 yard | $=3$ feet |
| 1 fathom | $=6$ feet |
| 1 rod | $=51 / 2$ yards |
| 1 furlong | $=40$ rods |
| 1 statute mile | $=8$ furlongs |
| 1 statute mile | $=5280$ feet |
| 1 nautical mile | $=6076.1$ feet |
| 1 nautical mile | $=1.1508$ statute |
|  | miles |
| 1 league | $=3$ miles |

## Square Measure

| 1 square foot | $=$144 square <br> inches |
| :--- | :--- |
| 1 square yard | $=9$ square feet |
| 1 square rod | $=$$30^{1 / 4}$ square <br> yards |
| 1 section (of  <br> land)  <br> 1 township $=1$ square mile <br>  $=$6 miles square <br> $(36$ square <br> miles $)$ <br>  $=$160 square <br> rods <br> 1 acre $=43,560$ square <br> feet  |  |

1 square mile $=640$ acres

## Volume Measure

| 1 cubic foot | $=$1728 cubic <br> inches |
| :--- | :--- |
| 1 cubic yard | $=27$ cubic feet |
| 1 U.S. gallon | $=$231 cubic <br> inches |

## Liquid Measure

| 1 pint | $=4$ gills |
| :--- | :--- |
| 1 quart | $=2$ pints |
| 1 gallon | $=4$ quarts |
| 1 barrel |  |
| (petroleum) | $=42$ gallons |
| 1 barrel | $=311 / 2$ gallons |
| 1 hogshead | $=2$ barrels $(63$ |
|  | gallons) |
| 1 tun | $=252$ gallons |

## Dry Measure

| 1 quart | $\begin{aligned} & =2 \text { pints } \\ & =67.2006 \text { cubic } \\ & \text { inches } \end{aligned}$ |
| :---: | :---: |
| 1 peck | $\begin{aligned} & =8 \text { quarts } \\ & =537.605 \text { cubic } \\ & \text { inches } \end{aligned}$ |
| 1 bushel | $\begin{aligned} & =4 \text { pecks } \\ & =2150.419 \\ & \quad \text { cubic inches } \end{aligned}$ |
| 1 barrel | $\begin{aligned} & =3.281 \text { bushels } \\ & =7056 \text { cubic } \\ & \text { inches } \end{aligned}$ |

## Avoirdupois Weight

(for other than drugs, gold, silver, etc.)
1 dram (dr) $=\underset{\text { grains* }}{27.3437}$

1 ounce (oz) $\quad=16$ drams
1 pound (lb) $\quad=16$ ounces
1 quarter $=25$ pounds
1 hundredweight

| $(\mathrm{cwt})$ | $=4$ quarters |
| :--- | :--- |
| 1 ton $(\mathrm{tn})$ | $=20$ |
|  | hundredweights |

$\begin{array}{ll}1 \text { short ton } & =2000 \text { pounds } \\ 1 \text { long ton } & =2240 \text { pounds }\end{array}$

## Troy Weight

(for gold, silver, etc.)
1 pennyweight
(dwt) $\quad=24$ grains*
1 ounce troy (ozt) $=20$
pennyweights
1 pound troy ( lb t ) $=12$ ounces troy
$=240$
pennyweights
$=5760$ grains

## Apothecaries' Weight

(for drugs)
1 dram apoth
(dr ap) $=3$ scruples
1 ounce apoth
(oz ap)
$=8$ drams apoth

1 pound apoth
$\left.\begin{array}{rl}\text { (lb ap) } & =\begin{array}{l}12 \text { ounces } \\ \text { apoth }\end{array} \\ & =96 \text { drams } \\ & \text { apoth }\end{array}\right)$

## METRIC SYSTEM

## Linear Measure

| 10 millimeters | $=1$ centimeter |
| :--- | :--- |
| 10 centimeters | $=1$ decimeter |
| 10 decimeters | $=1$ meter |
| 1000 meters | $=1$ kilometer |

## Area Measure

100 square

millimeters $\quad=$| 1 square |
| :--- |
| centimeter |

100 square

centimeters $\quad=$| decimeter |
| :--- |

100 square
decimeters $\quad=1$ square meter

## Volume Measure

1000 cubic
millimeters
$=1$ cubic centimeter

1000 cubic centimeters
$=1$ cubic decimeter

1000 cubic
decimeters $\quad=1$ cubic meter

[^10]Liquid Measure

| 10 milliliters | $=1$ centiliter |
| :--- | :--- |
| 10 centiliters | $=1$ deciliter |
| 10 deciliters | $=1$ liter |

Weight Measure

| 10 milligrams | $=1$ centigram |
| :--- | :--- |
| 10 centigrams | $=1$ decigram |
| 10 decigrams | $=1$ gram |
| 10 grams | $=1$ dekagram |
| 10 dekagrams | $=1$ hectogram |
| 10 hectograms | $=1$ kilogram |
| 1000 kilograms | $=1$ metric ton |

## WINDS

| Designation | Miles per hour |
| :--- | :---: |
| calm | less than 1 |
| light air | $1-3$ |
| light breeze | $4-7$ |
| gentle breeze | $8-12$ |
| moderate breeze | $13-18$ |
| fresh breeze | $19-24$ |
| strong breeze | $25-31$ |
| moderate gale | $32-38$ |
| fresh gale | $39-46$ |
| strong gale | $47-54$ |
| whole gale | $55-63$ |
| storm | $64-72$ |
| hurricane | above 72 |

## WEIGHT OF WATER

1 cubic inch $\quad=0.0360$ pound
12 cubic inches $=0.433$ pound
1 cubic foot $\quad=62.4$ pounds
1 cubic foot $\quad=7.48052$ U.S. gallons

| 1.8 cubic feet | $=112.0$ pounds |
| :--- | :--- |
| 35.96 cubic feet | $=2240.0$ pounds |
| 1 imperial gallon | $=10.0$ pounds |
| 11.2 imperial <br> gallons <br> 224 imperial <br> gallons | $=112.0$ pounds |
| 1 U.S. gallon | $=2240.0$ pounds |
| 13.45 U.S. <br> gallons <br> 269.0 U.S. <br> gallons | $=112.0$ pounds |
|  | $=2240.0$ pounds |

## HYDRAULIC EQUATIONS

pounds per

| square inch | $=$$0.434 \times$ head <br> of water in <br> feet |
| :--- | :--- |
| head in feet | $=$$2.31 \times$ <br> pounds per <br> square inch |

Approximate loss of head due to friction in clean iron pipes is:

$$
\frac{0.02 \times L \times V^{2}}{64.4 D} \mathrm{ft}
$$

where
$L$ is the length of pipe, in feet, $V$ is the velocity of flow, in feet per second,
$D$ is the diameter, in feet.
In calculating the total head to be pumped against, it is common to consider this value as being equal to the sum of the friction head and the actual head:

Horsepower of waterfall

$$
=\frac{62 \times A \times V \times H}{33,000}
$$

where
$A$ is the cross section of water, in square feet,
$V$ is the velocity of flow, in feet per minute,
$H$ is the head of fall, in feet.

## FALLING OBJECT

The speed acquired by a falling object is determined by the formula:

$$
V=32 t
$$

where
$V$ is the velocity, in feet per second, $t$ is the time, in seconds.

The distance traveled by a falling object is determined by the formula:

$$
d=16 t^{2}
$$

where
$d$ is the distance traveled, in feet, $t$ is the time, in seconds.

## SPEED OF SOUND

The speed of sound through air at $0^{\circ} \mathrm{C}$ is usually considered to be $1087.42 \mathrm{ft} / \mathrm{s}$, and at normal temperature, $1130 \mathrm{ft} / \mathrm{s}$. The speed of sound through any given temperature of air is determined by the formula:

$$
V=\frac{1087 \sqrt{(273+t)}}{16.52}
$$

where
$V$ is the speed, in feet per second, $t$ is the temperature, in degrees Celsius.

## PROPERTIES OF FREE SPACE

$$
\begin{aligned}
\text { velocity of light } & =c \\
& =\frac{1}{\left(\mu_{1} \varepsilon_{\mathrm{r}}\right)^{1 / 2}} \\
& =2.998 \times 10^{8} \mathrm{~m} / \mathrm{s} \\
& =186,280 \mathrm{mi} / \mathrm{s} \\
& =984 \times 10^{6} \mathrm{ft} / \mathrm{s} \\
\text { permeability } & =\mu_{v}=4 \pi \times 10^{-7} \\
& =1.257 \times 10^{-6} \\
& \mathrm{H} / \mathrm{m} \\
\text { permittivity } & =\varepsilon_{\mathrm{v}}=8.85 \times 10^{-12} \\
& \approx\left(36 \pi \times 10^{9}\right)^{-1} \mathrm{~F} / \mathrm{m}
\end{aligned}
$$

characteristic

$$
\begin{aligned}
\begin{aligned}
\text { haracteristic } \\
\text { impedance }
\end{aligned} & =Z_{0}=\left(\frac{\mu_{1}}{\varepsilon_{\mathrm{r}}}\right)^{1 / 2} \\
& =376.7 \\
& \approx 120 \pi \Omega
\end{aligned}
$$

## COST OF OPERATION

The cost of operation of an electrical device is determined by the formula:

$$
C=\frac{W t c}{1000}
$$

where
$C$ is the cost of operation, $W$ is the wattage of the device, in watts,
$t$ is the time, in hours, $c$ is the cost per kilowatt-hour of electricity.

## CONVERSION OF MATTER INTO ENERGY

The conversion of matter into energy (Einstein's theorem) is expressed by:

$$
E=m c^{2}
$$

where
$E$ is the energy, in ergs,
$m$ is the mass of the matter, in grams, $c$ is the speed of light, in centimeters
per second ( $c^{2}=9 \times 10^{20}$ ).

## ATOMIC SECOND

The atomic second was permanently adopted as the International Unit of Time by the 13th General Conference on Weights and Measures, in Paris on October 13, 1967. The atomic second is defined as the duration of $9,192,631,770$ periods of the radiation corresponding to the transition between two specific hyperfine levels of the fundamental state of the cesium-133 atom. It was chosen to be identical with the ephemeris second.

## INTERNATIONAL AND ABSOLUTE UNITS

The following list shows the international unit values compared to the absolute values. The values used will vary from one country to another.

$$
\begin{aligned}
& 1 \text { international } \\
& \text { volt }
\end{aligned} \quad \begin{aligned}
& 1.00033 \\
& \text { absolute volt }
\end{aligned}
$$

1 international

ohm $\quad=$| 1.000495 |
| :--- |
|  |
| absolute ohm |

1 international coulomb $\quad=0.999835$ absolute coulomb

1 international henry
$=1.00049$ absolute henry

1 international
farad $=0.999505$ absolute farad

1 international joule $=1.000165$ absolute joule

1 international watt
$=1.000165$ absolute watt

## DEGREES, MINUTES, AND SECONDS OF A CIRCLE

A complete circle consists of 360 equal divisions called degrees. Each degree is made up of 60 equal parts called minutes, and each minute is made up of 60 seconds. Thus, a circle consists of 360 degrees or 21,600 minutes, or $1,296,000$ seconds. Table $7-4$ converts minutes and seconds to decimal parts of a degree.

## GRAD

A grad is equal to 0.01 of a right angle. Computers designed for engineering applications may provide a choice of degrees, radians, or grads. There are $2 \pi$ ( $6.2832 \ldots$ ) radians in $360^{\circ}$.

TABLE 7-4
Minutes and Seconds in Decimal Parts of a Degree

| Minutes | Degrees | Minutes | Degrees | Seconds | Degrees | Seconds | Degrees |
| :---: | :--- | :--- | :--- | :---: | :--- | :---: | :---: |
| 1 | 0.01667 | 31 | 0.51667 | 1 | 0.00028 | 31 | 0.00861 |
| 2 | 0.03333 | 32 | 0.5333 | 2 | 0.00056 | 32 | 0.00889 |
| 3 | 0.05 | 33 | 0.55 | 3 | 0.00083 | 33 | 0.00917 |
| 4 | 0.06667 | 34 | 0.56667 | 4 | 0.00111 | 34 | 0.00944 |
| 5 | 0.08333 | 35 | 0.58333 | 5 | 0.00139 | 35 | 0.00972 |
|  |  |  |  |  |  |  |  |
| 6 | 0.10 | 36 | 0.60 | 6 | 0.00167 | 36 | 0.01 |
| 7 | 0.11667 | 37 | 0.61667 | 7 | 0.00194 | 37 | 0.01028 |
| 8 | 0.13333 | 38 | 0.63333 | 8 | 0.00222 | 38 | 0.01056 |
| 9 | 0.15 | 39 | 0.65 | 9 | 0.0025 | 39 | 0.01083 |
| 10 | 0.16667 | 40 | 0.66667 | 10 | 0.00278 | 40 | 0.01111 |
|  |  |  |  |  |  |  |  |
| 11 | 0.18333 | 41 | 0.68333 | 11 | 0.00306 | 41 | 0.01139 |
| 12 | 0.20 | 42 | 0.70 | 12 | 0.00333 | 42 | 0.01167 |
| 13 | 0.21667 | 43 | 0.71667 | 13 | 0.00361 | 43 | 0.01194 |
| 14 | 0.23333 | 44 | 0.73333 | 14 | 0.00389 | 44 | 0.01222 |
| 15 | 0.25 | 45 | 0.75 | 15 | 0.00417 | 45 | 0.0125 |
|  |  |  |  |  |  |  |  |
| 16 | 0.26667 | 46 | 0.76667 | 16 | 0.00444 | 46 | 0.01278 |
| 17 | 0.28333 | 47 | 0.78333 | 17 | 0.00472 | 47 | 0.01306 |
| 18 | 0.30 | 48 | 0.80 | 18 | 0.005 | 48 | 0.01333 |
| 19 | 0.31667 | 49 | 0.81667 | 19 | 0.00528 | 49 | 0.01361 |
| 20 | 0.33333 | 50 | 0.83333 | 20 | 0.00556 | 50 | 0.01389 |
|  |  |  |  |  |  |  |  |
| 21 | 0.35 | 51 | 0.85 | 21 | 0.00583 | 51 | 0.01417 |
| 22 | 0.36667 | 52 | 0.86667 | 22 | 0.00611 | 52 | 0.01444 |
| 23 | 0.38333 | 53 | 0.88333 | 23 | 0.00639 | 53 | 0.01472 |
| 24 | 0.40 | 54 | 0.90 | 24 | 0.00667 | 54 | 0.015 |
| 25 | 0.41667 | 55 | 0.91667 | 25 | 0.00694 | 55 | 0.01528 |
| 26 | 0.43333 |  | 56 | 0.93333 | 26 | 0.00722 |  |
| 27 | 0.45 | 57 | 0.95 | 27 | 0.0075 | 56 | 0.01556 |
| 28 | 0.46667 | 58 | 0.96667 | 28 | 0.00778 | 57 | 0.01583 |
| 29 | 0.48333 | 59 | 0.98333 | 29 | 0.00806 | 59 | 0.01611 |
| 30 | 0.50 | 60 | 1.00 | 30 | 0.00833 | 60 | 0.01639 |
|  |  |  |  |  |  |  |  |

## Appendix A

# Calculations Using Commodore $64{ }^{\circledR}$ Computer 

## Robert L. Kruse

The following pages contain programs which may be run on the Commodore $64{ }^{\circledR}$ computer to perform the following calculations:

1. Conversion of impedance to admittance and admittance to impedance.
2. Conversion of vectors from rectangular to polar form and polar form to rectangular form.
3. Impedance and phase angle of
resultant for two vectors (phasors) in parallel.
4. Input impedance and phase angle of RLC parallel resonant circuit.
5. Unsymmetrical two-section lag circuit (with or without resistive load).
6. Unsymmetrical two-section lead circuit (with or without resistive load).

For each application two programs are included. The first is for use without a printer and the second for use with a printer.

## Appenidix A

PROGRAM 1-Conversion of impedance to admittance and admittance to impedance

## Without Printer

```
5 REM PRG 1 U/D PRINTER
10 PRINT "*CONUERSION OF IMPEDANCE TO RDMITTANCE*"
2O PRINT " *QR ADMITTANCE ID IMPEDANCE*"
30 PRINT:PRINT:R=0:X=0:G=0:B=0:Y=0:GG=0:BB=0:PH=0:TH=0:Z=0
40 PRINT "IF IMPEDANCE DATA,RUN 90: IF ADMIITANCE DATA,RUN 240":END
GO PRINT:INPUT "R (OHMS)=";R
110 INPUI "X (OHMS)=";X
```



```
130Y=(G†2+BtE)+.5:PH=ATN(B/G):PH=-PH
140 PRINT "G CDNDUCTANCE (SIEMENS)=";G
1GO PRINT "B SUSCEPIANCE (SIEMENS)=";B
180 PRINT "(RECTANGULAR FORM)":PRINT
130 PRINT "Y ADMITTANCE (SIEMENS)=";Y
195 PZ=.01*INT((PH*360/6.2B32)*100)
210 PRINI "Y PHASE ANGLE (DEGREES)=";PZ
230 PRINT "(POLAR FORM)":PRINT:END
240 INPUT "G (SIEMENS)=";GG
260 INPUT "B (SIEMENS)=";BB:PRINT
2BO R=GG/(GG+2+BBt巳):X=BB/(GGt2+BB+2)
290 Z=(R+T+X+TZ)+.5:TH=AIN(X/R)
295 TP=.01*INT(R*100)
300 PRINT "R RESISTANCE (OHMS)=";IP
310 LP-.01*INT(X*100)
320 PRINT "X REACTANCE (OHMS)=";LP
340 PRINT "(RECTANGULAR FORM)":PRINT
345 PL=.O1*INT(2*100)
350 PRINT "Z IMPEDANCE (OMMS)=";PL
355 LA*.01*INT((IH*360/6.2832)*100)
370 PRINT "Z PHASE ANGLE (DEGREES)=";LA
390 PRINI "(POLAR FORM)":PRINI
4OO PRINT "******************************************:PRINT
410 END
```

With Printer

5 REM PRG 1 WITH PRINTER
10 PRINT "*CONUERSIDN DF IMPEDANCE IU ADMITTANCE*"
15 DPEN1, $4:$ PRINT\#1, "*CONUERSION OF IMPEDANCE TD ADMITTANCE*":CLOSE1, 4
20 PRINT " OR ADMITIANCE IO IMPEDANCE*"
25 OPEN1, 4: PRINT\#1," *OR ADMITTANCE TO IMPEDANCE*"
27 PRINT\#1,:PRINT\#1,:CLOSE1, 4
30 PRINT: PRINT:R-O:X-O:G=0:B=0:Y-O:GG=O:BB-O:PH-O:IH=0:Z=0
40 PRINT "IF IMPEDANCE DATA, RUN 90: IF ADMITTANCE DATA, RUN 240"
50 OPEN1, 4:PRINT\#1,"IF IMPEDANCE DATA,RUN 90:IF ADMITTANCE DATA,RUN 240"
EO PRINT\#1,:CLOSE1, 4:END
90 PRINT: OPEN1, 4:PRINT\#1,:CLOSE1, 4:INPUT "R (DHMS)=";R
100 OPEN1,4:PRINT\#1,"R (OHMS)m"; R:CLDSE1,4
110 INPUT "X (OHMS)="; X
115 OPEN1, 4 :PRINT\#1," $X(O H M S)=" ; X: P R I N T \# 1,:$ CLOSE1, 4
$120 G=R /(R+2+X+2): B=X /(R+2+X+2): P R I N I$
$130 \mathrm{Y}=(\mathrm{G}+ट+\mathrm{B} \uparrow \mathrm{C}) \dagger .5: \mathrm{PH}-\mathrm{ATN}(\mathrm{B} / \mathrm{G}): \mathrm{PH}=-\mathrm{PH}$
140 PRINI "G CDNDUCTANCE (SIEMENS)=";G
150 OPEN1,4:PRINT\#1,"G CONDUCTANCE (SIEMENS)=";G:CLDSE1,4
160 PRINT "B SUSCEPTANCE (SIEMENS)=";B
170 OPEN1,4:PRINT\#1,"B SUSCEPTANCE (SIEMENS)=";B:CLDSE1,4

## Calculations Using Commodore 64 Computer

```
1日0 PRINT "(RECTANGULAR FORM)":PRINT
185 OPEN1,4:PRINT#1,"(RECIANGULAR FORM)":PRINT#1,:CLOSE1,4
190 PRINT "Y ADMITTANCE (SIEMENS)=";Y
193 OPEN1,4:PRINT#1,"Y ADMITTANCE (SIEMENS)=";Y:CLOSE1,4
195 PZ-.01*INT((PH*360/6.2832)*100)
210 PRINT "Y PHASE ANGLE (DEGREES)-";PZ
220 OPEN1,4:PRINT#1,"Y PHASE ANGLE (DEGREES)=";PZ:CLOSE1,4
230 PRINT "(POLAR FORM)"
235 OPEN1,4:PRINT#1,"(POLAR FORM)":END:CLOSE1,4
240 PRINT:OPEN1,4:PRINT#1,:CLOSE1,4:INPUT "G (SIEMENS)=";GG
250 OPEN1,4:PRINT#1,"G (SIEMENS)=";GG:CLOSE1,4
260 INPUT "B (SIEMENS)=";BB
270 OPEN1,4:PRINT#1,"B (SIEMENS)=";BB:PRINT#1,:CLOSE1,4
2B0 R=GG/(GG+E+BB+E):X-BB/(GG+2+BB+2)
290 2-(R+2+Xt2)†.5:TH-ATN(X/R):PRINT
295 TP=.01*INT(R*100)
300 PRINT "R RESISTANCE (DHMS)=";TP
305 OPEN1,4:PRINT#1,"R RESISTANCE (OHMS)=";TP:CLOSE1,4
310 LP=.01*INT(X*100)
320 PRINT "X REACTANCE (OHMS)-";LP
330 OPEN1,4:PRINT#1,"X REACTANCE (DHMS)=";LP:CLOSE1,4
340 PRINT "(RECTANGULAR FORMJ":PRINT
342 OPEN1,4:PRINT#1,"(RECTANGULAR FORM)":PRINT#1,:CLOSE1,4
345 PL=.01*INT(2*100)
350 PRINI "Z IMPEDANCE (DHMS)=";PL
353 OPEN1,4:PRINT#1,"Z IMPEDANCE (OHMS)=";PL:CLOSE1,4
355 LA=.01*INT((IH*360/6.2日32)*100)
370 PRINT "Z PMASE ANGLE (DEGREES)=";LA
380 OPEN1,4:PRINT#1,"Z PHASE ANGLE (DEGREES)-";LA:CLOSE1,4
390 PRINT "(POLAR FORM)"
395 OPEN 1,4:PRINT#1,"(POLAR FDRM)":CLOSE1,4
4OO PRINT "****************************************:PRINT
405 OPEN1,4:PRINT#1,"******************************************":PRINT#1,:CLOSE1,4
4 1 0 ~ E N D
```

Sample Run

```
*CONUERSIDN OF IMPEDANCE IO ADMIITANCE*
```

    *OR ADMITTANCE TO IMPEDANCE*
    IF IMPEDANCE DATA, RUN 90: IF ADMITIANCE DATA, RUN 240
$R($ OHMS $)=75$
$\times($ OHMS $)=100$
6 CONDUCTANCE (SIEMENS)= 4.BE-03
B SUSCEPTANCE (SIEMENS)=6.4E-03
(RECTANGULAR FORM)
Y ADMIIIANCE (SIEMENS)= 日E-O3
$Y$ PHASE ANGLE (DEGREES)=-53.13
(POLAR FDRM)
G (SIEMENS)=4.8E-03
$B(S I E M E N S)=6.4 E-03$

## Appendix A

```
R RESISIANCE (OHMS)= 74.99
X REACTANCE (OMMS)= 99.99
(RECIANGULAR FORM)
2 IMPEDANCE (OHMS)=124.99
2 PHASE ANGLE (DEGREES)= 53.12
(POLAR FORM)
```

PROGRAM 2－Conversion of vectors from rectangular to polar form and from polar to rectangular form

## W＇ithout Printer

```
5 REM PRG 2 W/D PRINTER
10 PRINT "*CONUERSION OF UECTORS FROM RECTANGULAR TO POLAR FORM,"
15 PRINT "AND FROM POLAR TD RECTANGULAR FORM"":PRINT
30 PRINT "IF POLAR TO RECTANGULAR, RUN 70:IF RECTANGULAR TO POLAR, RUN 17O":END
70 PRINT:INPUT "Z (RESISTIUE COMPONENT, OHMS)=";A
90 INPUT "Z (REACIIUE COMPONENI, OHMS)=";B
110 PQ=(A`圤+B+2) †.5:QP=ATN(B/A)
115 LM=.01*INT(PQ*100)
120 PRINI "Z (MAGNITUDE, OMMS)m";LM
130 ML=.01*INT((QP*350/6.2832)*100)
140 PRINT "Z (ANGLE, DEGREES)=";ML
150 PRINT
16O END
170 PRINT:INPUT "Z (MAGNITUDE, DHMS)=";C
190 INPUI "Z (ANGLE, DEGREES)=";口
210 JK=C*COS(0*6.2日32/360):KJ=C*SIN(D*G.2832/350)
215 QQ=.01*INT(JK*100)
2こO PRINT "Z (RESISTIUE COMPONENT, OHMS)=";QQ
230 QZ=.01*INT(KJ*100)
240 PRINT "Z (REACIIUE COMPDNENT, OHMS)=";DZ
2GO PRINT "*************************************":PRINT
270 END
```

With Printer

```
5 REM PRG 2 WITH PRINTER
10 PRINT "*CONUERSION OF UECTORS FROM RECTANGULAR IO POLAR FORM,"
12 OPEN1,4
13 PRINT#1,"*CONUERSION OF UECTORS FROM RECTANGULAR TO POLAR FORM,"
14 CLOSE1,4
15 PRINT "AND FROM POLAR ID RECTANGULAR FDRM*":PRINT
2O OPEN1,4
2S PRINT#1,"AND FROM POLAR TD RECTANGULAR FORM*":PRINT#1,:CLOSE1,4
30 PRINT "IF POLAR TO RECTANGULAR, RUN 70:IF RECTANGULAR ID POLAR, RUN 170"
40 OPEN1,4
50 PRINT#1,"IF POLAR TO RECTANGULAR, RUN 70:IF RECTANGULAR ID POLAR, RUN 170"
60 PRINT#1,:CLOSE1,4:END
70 PRINT:INPUT "Z (RESISTIUE COMPGNENT,.OHMS)=";A
80 OPEN1,4:PRINT#1,"2 (RESISTIUE COMPONENT, OMMS)=";A:CLOSE1,4
90 INPUT "Z (REACTIUE COMPONENT, OHMS)=";B
100 OPEN1,4:PRINT#1,"Z (REACTIUE COMPONENT, OHMS)=";B:CLOSE1,4
110 PQ=(A†ट+B!巳)†.5:QP-AIN(B/A)
```

```
115 LM=.01*INT(PQ*100)
12O PRINI "2 (MAGNITUDE, DHMS)=";LM
125 OPEN1,4:PRINI#1,"Z (MAGNITUDE, OHMSJ=";LM:CLOSE1,4
130 ML=.01*INT( (QP*360/6.2日32)*100)
140 PRINT "Z (ANGLE, DEGREES)=";ML
145 OPEN1,4:PRINT#1,"Z (ANGLE, DEGREES)=";ML:CLDSE1,4
150 PRINT "*****************************************"
155 OPEN1,4:PRINT#1, "*************************************"
160 PRINT井1,:CLOSE1,4:END
170 PRINT:INPUT "Z (MAGNITUDE, OMMS)=";C
180 OPEN1, 4:PRINT#1,"Z (MAGNITUDE, OHMS)=";C:CLOSE1,4
190 INPUT "Z (ANGLE, DEGREES)=";D
2OO OPEN1,4:PRINT#1,"Z (ANGLE, DEGREES)=";D:CLOSE1,4
210 JK=C*COS(D*6.2日32/350):KJ=C*SIN(D*6.2B32/360)
215 QQ=.01*INT(JK*100)
22O PRINT "2 (RESISTIUE COMPONENT, OHMS)=";QQ
225 OPEN1,4:PRINT#1,"Z (RESISTIUE COMPONENT, OHMS)=";QQ:CLOSE1,4
230 02=.01*INT(KJ*100)
240 PRINT "Z (REACTIVE COMPONENT, DMMS)=";QZ
250 OPEN1,4:PRINT#1,"2 (REACTIUE COMPONENT, OMMS)=";QZ:CLISE1,4
2GO PRINI "##***********************************": PRINT
2G5 OPEN1, 4: PRINT#1, "**************************************", CLSSE1, 4
270 END
```

Sample Run
＊CONUERSION OF UECTORS FROM RECTANGULAR TO POLAR FORM， AND FROM POLAR TO RECTANGULAR FORM＊

IF POLAR TO RECTANGULAR，RUN 7O：IF RECTANGULAR TD POLAR，RUN 170
2 （RESISTIUE CDMPDNENI，OHMS）＝64．95
2 （REACTIUE COMPONENT，OHMS）＝37．5
2 （MAGNITUDE，OHMS）＝74．99
2 （ANGLE，DEGREES）＝ 30


2 （MAGNIIUDE，OHMS）－75
2 （ANGLE，DEGREES）－ 30
2 （RESISTIUE COMPDNENT，OHMS）－64．95
2 （REACIIUE CDMPONENT，OHMS）＝ 37.5

PROGRAM 3－Impedance and phase angle of resultant for two vectors（phasors）in parallel

## Without Printer

```
5 REM PRG 3 U/O PRINTER
10 PRINT "IMPEDANCE AND PHASE ANGLE DF RESLLIANT FOR TWD UECIORS (PMASORS)"
12 PRINT
30 PRINT "IF POLAR DATA, RUN 170: IF RECTANGULAR DAIA, RUN BO":END
80 PRINT:PRINT
90 INPUT "Z1 RESISIANCE (DMMS)=";A
110 INPUT "Z1 REACTANCE (OHMS)=";B
130 INPUT "Z2 RESISIANCE (OHMS)=";C
150 INPUT "Z2 REACTANCE (OHMS)=";D:PRINT:GOTO 2ES
```

```
170
    INPUI "Z1 MAGNITUDE (OHMS)=";E
190 INPUT "21 PHASE ANGLE (DEGREES)=";F
210 INPUT "Z2 MAGNITUDE (DHMS)=";G
230 INPUT "Z2 PHASE ANGLE (DEGREES)=";H:PRINT
250 A=E*COS(F*6.2832/360):B=E*SIN(F*6.2832/360):PRINT:PRINT
260 C=G*COS(H*6.2832/360): D=G*SIN(H*6, 2. (%32/350)
265 WA=.01*INT(A*100)
270 PRINT "R1 (OMMS)=";WA
275 WB=.01*INT(B*100)
280 PRINT "X1 (OHMS)-";WB
285 WC=.01*INT(C*100)
290 PRINI "R2 (OHMG)=";WC
295 WD=.01*INI(D*100)
300 PRINT "X2 (OHMS)=";WD
310 PRINT "(RECTANGULAR COMPDNENTS)":PRINT
320 E=(A+C+B+2)t.5:NJ=B/A:PH=ATN(NJ)
325 WE=.01*INT(E*1OO)
330 PRINT "21 (OMMS)-";WE
335 WF=.01*INT ((PH*350/6.2日32)*100)
340 PRINT "PHASE ANGLE (DEGREES)=";WF
360 PRINT "(PDLAR FORM)":PRINT
370 G=(C!2+D+2)t.5:JJ=D/C:HP=RTN(JJ)
375 WG=.01*INT(G*100)
360 PRINT "Z2 (OHMS)=";WG
385 WH=.01*INT(CMP*360/G.2832)*100)
390 PRINT "PHASE ANGLE (DEGREES)=";WH
410 PRINT "(POLAR FORM)":PRINT
420 Q=A+C:QQ=B+D
425 WI=.01*INT(Q*100)
430 PRINT "Z1+22 (OHMS RESISTANCE)=";WI
435 WJ=.O1*INT(DQ*100)
440 PRINT "Z1+Z2 (OHMS REACIANCE)-";WJ
460 PRINT "(RECTANGULAR FORM)":PRINT
470 NN-E*G:MM-PH+HP
475 WK=.01*INT(NN*100)
48O PRINT "Z1*Z2 (OMMS)=";WK
485 UL-.01*INT((MM*360/6.2gヨ2)*100)
490 PRINT "PMASE ANGLE (DEGREES)=";WL
510 PRINT "(POLAR FORM)":PRINT
520 Y=(Q+Z+QQ+己)+.5:XY=QQ/Q:TH-ATN(XY)
S2S WM=.O1*INT(Y*100)
530 PRINT "Z1+2己 (OHMS)=";WM
535 UN=.01*INI((TH*360/6.2832)*100)
540 PRINT "PHASE ANGLE (DEGREES)=";WN
560 PRINT "(POLAR FORM)":PRINT
570 RZ-NN*COS(MM):XZ-NN*SIN(MM)
575 WO*.O1*INT(RZ*100)
5BO PRINT "Z1*Z2 (OHMS RESISIANCE)=";WO
585 WP=.01*INT(XZ*100)
590 PRINT "Z1*Z2 (OHMS REACTANEE)=";WP
610 PRINI "(RECTANGULAR FORM`":PRINI
620 AQ=NN/Y:QA=MM-TH
G2S WQ=.01*INT(AO*100)
530 PRINI "Z1 AND Z2 IN PARALLEL (OHMS)=";W0
535 wR=.01*INT((QA*360/6.2日32)*100)
640 PRINT "PHASE ANGLE (DEGREES)=";WR
650 PRINI "(PQLAR FORM)":PRINT
670 BS=AQ*COS(QA): SB=AQ*SIN(QA)
675 WS=.01*INT(BS*100)
GBO PRINT "21 AND Z己 IN PARALLEL (DHMS RESISIANCE)=";WS
685 wT=.O1*INT(SB*100)
```

750 PRINT＂WHEN ANGLES GREATER THAN 90 DEGREES ARE BEING PROCESSED，＂
760 PRINT＂THERE IS A POSSIBLE 180 DEGREE AMBIGUITY IN THE FINAL ANSWER．＇
770 PRINT＂TO CHECK FOR 180 DEGREE AMBIGUITY，MAKE A ROUGH SKETCH OF＂
7 7 0 PRINT＂THE UECTOR DIAGRAM．＂：PRINT
790 PRINT＂SLIGHT INACCURACIES IN CDMPUTED UALUES MAY OCCUR DUE TD＂
800 PRINT＂SINGLE－PRECISION AND ROUNDING－OFF PROGRAMMING AND PROCESSING．＂
810 END

## With Printer

5 REM PRG 3 WITH PRINTER
10 PRINT＂IMPEDANCE AND PHASE ANGLE OF RESULTANT FOR TWD UECTORS（PHASORS）＂
15 OPEN1，4：PRINT\＃1，＂IMPEDANCE AND PHASE ANGLE OF RESULTANT FOR TWO UECTORS＂
20 PRINT\＃1，＂（PHASORS）＂：PRINT\＃1，：CLOSE1， 4
30 PRINT＂IF POLAR DATA，RUN 170：IF RECTANGULAR DATA，RUN BO＂
40 DPEN1，4：PRINT\＃1，＂IF POLAR DATA，RUN 170：IF RECTANGULAR DATA，RUN BO＂
50 PRINT\＃1，：PRINT\＃1，：CLOSE1，4：END
QO PRINT：PRINT
90 INPUT＂ 21 RESISTANCE（OHMS）＝＂；A
100 CPEN1，4：PRINT\＃1，＂Z1 RESISTANCE（OHMS）－＂；A：CLDSE1， 4
110 INPUT＂21 REACTANCE（GHMS）＝＂；B
120 OPEN1，4：PRINT\＃1，＂Z1 REACTANCE（OHMS）＝＂；B：CLOSE1，4
130 INPUT＂Z2 RESISTANCE（OHMS）＝＂；C
140 OPEN1，4：PRINT\＃1，＂Z己 RESISTANCE（OHMS）＝＂；C：CLOSE1，4
150 INPUT＂Z2 REACTANCE（OMMS）＝＂；D：PRINT
160 OPEN1，4：PRINT\＃1，＂Z2 REACTANCE（OHMS）＝＂；D：PRINT\＃1，：CLOSE1，4：GOTO 265
170 INPUT＂Z1 MAGNITUDE（GMMS）＝＂；
180 OPEN1，4：PRINT\＃1，＂21 MAGNITUDE（OMMS）－＂；E：CLOSE1， 4
190 INPUT＂Z1 PHASE ANGLE（DEGREES）＝＂；F
200 DPEN1， $4:$ PRINT\＃1，＂21 PHASE ANGLE（DEGREES）－＂；F：CLOSE1， 4
210 INPUT＂Z2 MAGNITUDE（OHMS）－＂；G
220 OPEN1，4：PRINT\＃1，＂22 MAGNITUDE（OMMS）＝＂；G：CLOSE1，4
230 INPUI＂Z2 PHASE ANGLE（DEGREES）＝＂；H：PRINT
240 OPEN1，4：PRINT\＃1，＂22 PHASE ANGLE（DEGREES）＝＂；H：PRINT\＃1，：CLOSE1，4
250 A＝E＊COS（F＊5．2832／360）：B＝E＊SIN（F＊6．2日32／360）：PRINT：PRINT
260 C－G＊COS（H＊6．2932／360）：D＝G＊SIN（H＊6．2832／360）
265 WA＝．01＊INT（A＊100）
270 PRINT＂R1（OMMS）＝＂；WA
273 DPEN1，4：PRINT\＃1，＂R1（OHMS）＝＂；WA：CLOSE1， 4
275 WB＝．01＊INT（B＊100）
2BO PRINT＂X1（OMMS）＝＂；WB
283 OPEN1，4：PRINT\＃1，＂X1（OHMS）－＂；WB：CLOSE1，4
285 WC＝．01＊INT（C＊100）
290 PRINT＂R2（DHMS）－＂；WC
293 OPEN1，4：PRINT\＃1，＂R2（OHMS）＝＂；WC：CLOSE1， 4
295 WD＝．01＊INT（D＊100）
300 PRINT＂X2（DHMS）＝＂；WD
305 OPEN1，4：PRINT\＃1，＂X2（OHMS）－＂；WD：CLOSE1，4
310 PRINT＂（RECTANGULAR COMPDNENTS）＂：PRINT
315 OPEN1，4：PRINT\＃1，＂（RECTANGULAR COMPONENTS）＂：PRINT\＃1，：CLOSE1，4
$320 E=(A+2+B+2)+.5: N J-B / A: P H-A T N(N J)$
325 WE＝．01＊INT（E＊100）
330 PRINT＂Z1（DHMS）＝＂；WE
333 OPEN1，4：PRINT\＃1，＂21（DHMS）＝＂；WE：CLOSE1，4
$335 \mathrm{WF}=.01 * \mathrm{INT}(\mathrm{CH}=360 / 6.2832) * 100)$
340 PRINT＂PHASE ANGLE（DEGREES）＂＂；WF
350 OPEN1，4：PRINT\＃1，＂PHASE ANGLE（DEGREES）＝＂；WF：CLOSE1， 4

## Appendix A

```
360
365 OPEN1,4:PRINT#1,"SPOLAR FORM)":PRINI#1,:CLOSE1, 4
370 G=(C.tこ+D+己) 1.5:JJ=\square/C:HP=ATN(JJ)
375 WG=.01*INT(G*100)
380 PRINT "Z己 (OHMS)=";WG
3日Э DPEN1,4:PRINT#1,"2己 (OHMS)=";WG:CLOSE1,4
305 WH=.O1*INT((HP*360/G.2日32)*100)
390 PRINT "PHASE ANGLE (DEGREES)="; WH
400 OPEN1, 4:PRINT#1,"PMASE ANGLE (DEGREES)="; WH:CLOSE1,4
410 PRINT "(POLRR FORM)":PRINT
415 OPEN1,4:PRINI#1,"(POLAR FORM)":PRINT#1,:CLOSE1,4
420 Q*A+C: OQ = B+D
42S WI=.01*INT(O*100)
430 PRINT "Z1+2己 (OHMS RESISTANCE)=";WI
433 OPEN1,4:PRINI#1,"Z1+22 (DHMS RESISTANCE)=";WI:CLOSE1,4
435 拢=.01*INI(QQ*10O)
440 PRINT "Z1+2己 (OHMS REACTANCE)=";WJ
450 OPEN2, 4:PRINT#1,"Z1+Z2 (OHMS REACTANCE)="; WJ:CLOSE1,4
460 PRINT "(RECTANGULAR FORM)":PRINT
465 OPEN1,4:PRINI#1,"(RECTANGULAR FORM)":PRINI#1,:CLOSE1,4
470 NN=E*G:MM-PH+HP
475 WK=.01*INI(NN*100)
4日0 PRINT "Z1*Z己 (OHMS)=";WK
4B3 OPEN1,4: PRINT#1,"Z1*Z2 (OHMS)=";WK:CLOSE1,4
4日5 wL=.O1*INT((MM*360/6.2832)*100)
490 PRINI "PHASE ANGLE (GEGREES)=";WL
5 0 0 ~ O P E N 1 , 4 : P R I N T \# 1 , " P H A S E ~ A N G L E ~ ( D E G R E E S ) = " ; W L : C L O S E 1 , 4 , ~
510 PRINT "(POLAR FDRM)":PRINT
515 DPEN1,4:PRINI#1,"(POLAR FORM)":PRINT#1,:CLOSE1,4
5こ0 Y-(0!己+QQ+2)1.5:XY=QQ/Q:TH-ATN(XY)
525 WM=.01*INT(Y*100)
53C PRINT "Z1+Z2 (OMMS)=";UM
533 OPEN1,4:PRINT#1,"21+22 (OHMS)="; WM:CLDSE1,4
535 WN=.01*INT((IH*360/6.2832)*1003
540 PRINT "PHASE ANGLE (DEGREES)"";UN
550 OPEN1,4:PRINT#1,"PHASE ANGLE (DEGREES)=";WN:CLDSE1,4
560 PRINT "(POLAR FORM)":PRINT
565 OPEN1, 4:PRINT#1,"(POLAR FORM)":PRINT#1,:CLOSEI, 4
570 RZ-NN*COS(MM):XZ-NN*SIN(MM)
575 WD=.01*INT(RZ*100)
5BO PRINT "Z1*22 (DHMS RESISTANCE)=";WO
5B3 OPEN1,4:PRINT#1,"Z1*2己 〔OHMS RESISTANCE`=";WO:CLOSE1,4
585 WP=.01*INT(XZ*100)
590 PRINT "Z1*Z2 (OHMS REACTANCE)=";WP
GOO OPEN1, 4:PRINT#1,"Z1*Z2 (OHMS REACTANCE) "*;WP:CLOSE1,4
G10 PRINT "(RECTANGULAR FDRM)":PRINT
615 OPEN1, 4:PRINT#1,"(RECTANGULAR FORM)":PRINT#1,:CLOSE1,4
EटO AQ=NN/Y:QA-MM-IH
625 Wロ=.01*INT (AQ*100)
630 PRINT "Z1 AND Z2 IN PARALLEL (OHMS)=";WQ
633 OPEN1, 4:PRINI#1,"21 aND Z己 IN PARALLEL (OHMS)=";WQ:CLOSE1,4
635 岒=.01*INI((QA*360/6.2832)*IOO)
540 PRINT "PHASE ANGLE (DEGREES)=";WR
650 OPEN1,4:PRINI#1,"PHASE ANGLE (DEGREES)=";WR:CLOSE1,4
GGO PRINT "(PQLAR FORM)":PRINT
665 OPEN1,4:PRINT#1,"(POLAR FORM)":PRINT#1,:CLDSE1,4
570 BS=AQ*COS(QA):SB-AQ*SIN(QA)
675 WS*.C1*INT(BS*100)
680 PRINT "Z1 AND Z2 IN PARALLEL (OMMS RESISTANCE)=";WS
GB3 OPEN1,4:PRINT#1,"Z1 AND 2己 IN PARALLEL (OHMS RESISTANCE)=";WS:CLDSE1,4
6日5 WT=.01*INT(SB*100)
```

```
700 PRINT "Z1 AND Z己 IN PARALLEL (OMMS REACTANCE)=";WI
710 OPEN1,4:PRINI#1,"Z1 AND Z己 IN PARALLEL (OHMS REACTANCE)=";WT:CLOSE1,4
720 PRINT "(RECTANGULAR FORM)":PRINT
725 OPEN1,4:PRINT#1,"(RECIANGULAR FORM)":PRINT#1,:PRINT#1,:CLOSE1,4
730 PRINT:PRINI
750 PRINT "WHEN ANGLES GREATER THAN SO DEGREES ARE BEING PROCESSED,"
755 DPEN1,4:PRINT#1,"WHEN ANGLES GREATER THAN SO DEGREES ARE BEING PROCESSED,"
757 CLOSE1,4
76O PRINT "THERE IS A POSSIBLE 18O DEGREE AMBIGUITY IN THE FINAL ANS|ER."
763 OPEN1,4
765 PRINT#1,"THERE IS A POSSIBLE 180 DEGREE AMBIGUITY IN THE FINAL ANSWER."
767 CLDSE1,4
770 PRINT "TO CHECK FOR 1BO DEGREE AMBIGUITY, MAKE A ROUGH SKETCH OF"
773 OPEN1,4
775 PRINT#1,"IO CHECK FOR 180 DEGREE AMBIGUITY, MAKE A ROUGH SXEICH OF"
777 CLOSE1,4
7BO PRINT "IHE UECIOR DIAGRAM.":PRINT
785 OPEN1,4:PRINT#1,"THE UECTOR DIAGRAM.":PRINT#1,:CLOSE1,4
790 PRINT "SLIGMI INACCLRACIES IN COMPUTED UALUES MAY DCCUR DUE TD"
793 OPEN1,4
795 PRINI#1,"SLIGHI INACCURACIES IN COMPUTED UALUES MAY OCCUR DUE IO"
797 CLDSEI,4
BOO PRINT "SINGLE-PRECISIDN AND RQUNDING-OFF PROGRAMMING AND PRDCESSING."
8O3 DPEN1,4
BO5 PRINT#I,"SINGLE-PRECISIDN AND ROUNDING-OFF PROGRAMMING AND PROCESSING."
807 CLDSE1,4
8 1 0 ~ P R I N T
815 OPEN1,4: PRINT#1, "****************************************",
82O END
```


## Sample Run

IMPEDANCE AND PHASE ANGLE OF RESULTANT FOR IUD UECTORS (PHASORS)

If polar data, run 170: if rectangular data, run bo

21 MAGNITUDE (OHMS)- 50
21 PHASE ANGLE (DEGREES)= 60
22 MAGNITUDE (OHMS)- 75
22 PHASE ANGLE (DEGREES)=20
R1 (OHMS)= 24.99
X1 (DHMS)= 43.3
R2 (OHMS)= 70.47
X2 (OHMS)= 25.65
(RECTANGULAR COMPONENTS)
21 (DHMS)= 50
PHASE ANGLE (DEGREES)= 59.99
(POLAR FORM)
22 (OMMS)= 75
PHASE ANGLE (DEGREES)= 20
(POLAR FGRM)

```
21+22 (OHMS RESISTANCE)= 95.47
21+22 (DHMS REACTANCE)= 68.95
(RECTANGULAR FORM)
Z1*22 (OMMS)= 3750
PHASE ANGLE (DEGREES)= 60
(POLAR FORM)
21+22 (OHMS)= 117.77
PHASE ANGLE (DEGREES)= 35.83
(POLAR FORM)
21*22 (OHMS RESISIANCE)= 651.16
21*Z2 (DMMS REACTANCE)= 3693.03
(RECTANGULAR FORM)
21 AND Z2 IN PARALLEL (OHMS)- 31.84
PHASE ANGLE (DEGREES)= 44.16
(POLAR FORM)
21 AND Z2 IN PARALLEL (OHMS RESISTANCE)- 22.84
21 AND Z2 IN PARALLEL (OHMS REACIANCE)= 22.1E
(RECTANGULAR FORM)
WHEN ANGLES GREATER IHAN SO DEGREES ARE BEING PROCESSED,
THERE IS A POSSIBLE 180 DEGREE AMBIGUITY IN THE FINAL ANSWER.
TO CHECK FOR 180 DEGREE AMBIGUITY, MAKE A ROUGH SKETCH OF
the uector difgram.
SLIGHT INACCURACIES IN COMPUTED UALUES MAY OCCUR DUE TD
SINGLE-PRECISION AND ROUNDING-DFF PROGRAMMING AND PROCESSING.
*************************
21 REACTANCE (OHMS)= 43.3
Z2 RESISTANCE (OHMS)-70.48
22 REACTANCE (OHMS)= 25.65
R1 (OMMS)- 25
X1 (OHMS)=43.29
R2 (OHMS)= 70.47
X2 (OHMS)= 25.64
(RECTANGULAR COMPONENIS)
21 (OMMS)-49.99
PHASE ANGLE (DEGREES)= 59.99
(POLAR FORM)
Z2 (OHMS)= 75
PMASE ANGLE (DEGREES)= 19.99
(POLAR FORM)
21+22 (OHMS RESISTANCE)- 95.47
21+22 (DHMS REACTANCE)= 68.94
(RECTANGULAR FORM)
21*22 (DHM5)= 3750.03
PHASE ANGLE (DEGREES)=79.99
(POLAR FORM)
```

```
Z1+22 (OHMS)= 117.77
PHASE ANGLE (DEGREES)= 35.83
(PGLAR FORM)
Z1*Z2 (DHMS RESISTANCE)= 651.35
Z1*Z己 (OHMS REACIANCE)= 3693.03
(RECTANGULAR FORM)
21 AND Z己 IN PARALLEL (OMMS)- 31.84
PHASE ANGLE (DEGREES)= 44.16
(POLAR FORM)
21 AND 22 IN PARALLEL (DHMS RESISIANCE)= 22.84
Z1 AND Z己 IN PARALLEL (DHMS REACTANCE)= ट2.1B
(RECIANGULAR FORM)
WHEN ANGLES GREATER IHAN GO DEGREES ARE BEING PRDCESSED,
THERE IS A PDSSIBLE 1BO DEGREE AMBIGUITY IN THE FINAL ANSWER.
TD CHECK FOR 1gO DEGREE AMBIGUITY, MAKE A ROUGH SKETCH OF
IHE UECTOR DIAGRAM.
SLIGHT INACCURACIES IN COMPUIED UALUES MAY OCCUR DUE TO
SINGLE-PRECISIDN AND RDUNDING-DFF PROGRAMMING AND PRDCESSING.
```

PROGRAM 4－Input impedance and phase angle of RIC parallel resonant circuit

## Without Printer

```
5 REM PRG 4 W/D PRINTER
10 PRINT "INPUT IMPEDANLE AND PHASE ANGLE OF RLC PARALLEL RESONANT CIRCUIT"
2O PRINT
30 INPUT "L (MH)=";L
40 INPUI "C (MFD)*";C
50 INPUI "RL (OHMS)=";RL
GO INPUT "RC (DMMS)=";RC
70 JNPUT "F (HZ)=";F
8O PRINT
90 XL=6.2832*F*L*.001:XC-1/(5.2日3己*F*C*10*-5)
```



```
110 RT=RL+RC:XT=XL-XC:DE=(RT \巳+XT \巳) †.S:ED=ATN(XI/RT)
12O BS=ZL*ZC:SB=LZ+CZ:HS=BS/DE:SH=SB-ED
125 QQ=INT(HS)
130 PRINT "ZIN (OHMS)m";QQ
135 QP=INT(SH*350/6.2B32)
140 PRINT "PHASE ANGLE (DEGREES)m";QP
150 END
```

With Printer
5 REM PRG 4 WITH PRINTER
10 PRINT＂INPUT IMPEDANCE AND PHASE ANGLE DF RLC PARALLEL RESDNANT CIRCUIT＂ 12 OPEN1，4
15 PRINT\＃1，＂INPUT IMPEDANCE AND PHASE ANGLE OF RLC PARALLEL RESONANT CIRCUIT＂
17 PRINT\#1,:CLOSE1,4
20 PRINT

## Appendix A

```
30 INPUT "L (MH)=";L
35 OPEN1,4:PRINT#1,"L (MH)*";L:CLOSE1,4
40 INPUT "C (MFD)=";C
45 OPEN1,4:PRINT#1, "C (MFD)=";C:CLOSE1,4
50 INPUT "RL (DHMS)=";RL
55 OPEN1,4:PRINT#1,"RL (OHMS)=";RL:CLOSE1,4
GO INPUT "RC (OMMS)=";RC
65 DPEN1,4:PRINT#1,"RC (OMMS)=";RC:CLOSE1,4
70 INPUT "F (HZ)=";F
75 OPEN1,4:PRINT#1,"F (HZ)=";F:PRINT#1,:CLOSE1,4
BO PRINT
90 XL=6.2832*F*L*.001:XC=1/(E.2日32*F*C*10ヶ-6)
```



```
110 RT=RL+RC:XT=XI-XC:DE=(RT†ट+XI'己)†.5:ED=ATN(XT/RT)
120 BS-2L*ZC:SB-LZ+CZ:HS=BS/DE:SH=SB-ED
125 QQ=INI(HS)
13O PRINT "ZIN (OHMS)=";QQ
132 OPEN1,4:PRINT#1,"ZIN (OHMS)=";QQ:CLOSE1,4
135 DP-INT(SH*350/G.2832)
140 PRINI "PHASE ANGLE (DEGREES)=";QP
142 OPEN1,4:PRINT#1,"PHASE ANGLE (DEGREES)=";QP:CLDSE1,4
150 END
```


## Sumple Run

INPUT IMPEDANCE AND PHASE ANGLE OF RLC PARALLEL RESONANI CIRCUIT
$L(M H)=150$
C（MFD）＝．15
RL（DHMS）＝3
RC（OHMS）＝1
$F(H Z)=1000$

ZIN（OHMS）－19094
PHASE ANGLE（DEGREES）＝ 85

PROGRAM 5－Unsymmetrical two－section lag circuit，with and without resistive load

## Whthout Printer

```
5 REM PRG 5 w/O PRINTER
10 PRINT "UNSYMMETRICAL 2-SECTION LAG CIRCUIT"
2O PRINT " (WITH/WITHOUT RESISTIUE LORD)"
30 PRINT "***************************************:PRINT
4O PRINT"COMPUTES UNLDADED QUTPUT IMPEDANCE AND PHASE ANGLE"
SO PRINT "(THEUENIN IMPEDANCE AND PHASE ANGLE)":PRINT
GO PRINT"COMPUTES UNLOADED EOUT/EIN AND PHASE ANGLE;"
70 PRINT "LOADED EOUT/EIN AND PHASE ANGLE":PRINI
80 INPUT "R1 (OHMS)=";RD
100 INPUT "R2 (OHMS)=";RT
120 INPUT "C1 (MFD)=";CO
140 INPUT "C2 (MFD)=";CT
160 INPUT "RL (OMMS)=";RL
180 INPUT "F (HZ)=";F:PRINT
200 X0-1/(6.2832*F*CO*10!-6)
202 XI-1/(6.2日32*F*CT*10†-5)
```

```
205 AB=RO*XD:BA=-5.2832/4
210 AC=(ROt2+XO!E) t.5:CA=-ATN(XD/RD)
215 AD=AB/AC:DA=BA-CA:AE=AD*CDS(DA)
220 AF=AD*SIN(DA):AG=AE+RI:AH=(AG+2+AF+C)+.5
225 HA=-ATN(AF/AG):AJ=AH*XT
230 JA=HA-6.2832/4:AK=AF-XT:KA=FA-6. 2B32/4
235 AL-(AG†2+AK†2) †.5:LA=-ATN(AK/AG)
240 AM=AJ/AL:MA=JA-LA:AN=AM:NA=MA:PF=F*NA
245 YZ-(RD+Z+XD+こ) !.5:ZY=-ATN(XO/RO)
247 لWA=INT(AN)
250 PRINT "ZOUT (OMMS)=";WA
255 XY=XD+XI:WX=(RT \ Z+XY!巳) !.5:XU=-ATN(XY/RT)
250 UW-WX*YZ:WU=XW+ZY:UU=UW/XD:UU=WU+G. 2B32/4
265 wB=INT(-NA* 360/6.2832)
270 PRINT "PHASE ANGLE, DEGREES (RL OPEN)=";WB
290 TU=UU*COS(UU):UT=UU*SIN(UU): ZUmUT + XO
295 RS=(TUTこ+ZW! 2) +.5:SR=-ATN(ZW/TU)
300 PU=XT/RS:UP=-5R-E. 2@\exists2/4:GU=PU*RL
30S HU=AN*COS(NA):JU=AN*SIN(NR):UG=UP
307 WC=.01*INT(PU*100)
310 PRINI"EDUI/EIN (RL OPEN)=";林
315 KU=HU-RL:LU=(KU+2+JUナこ)+.5
320 LL--ATN(JU/KU):NU=GU/LU:UN-UG-UL
325 WDm.01*INT((-UP*360/6.2832)*100)
330 PRINT "PHASE ANGLE (DEGREES)=";WD
340 WE-INT (AN)
350 PRINT "THEUENIN IMPEDANCE (OHMS)=";WE
360 WF=INT (-NA*360/6.2832)
370 PRINT "PHASE RNGLE (DEGREES)""; wF
380 WG=.01*INT(NU*100)
390 PRINT "EDUT/EIN (LOADED)=";WG
400 WH=.01*INT((-UN*360/6.2832)*100)
410 PRINT "PHASE ANGLE (DEGREES)=";WH:PRINT
430 PRINT "******************************************)
440 END
```


## With Printer

```
5 REM PRG 5 WITH PRINTER
10 PRINT＂UNSYMMETRICAL 2－SECTION LAG CIRCUIT＂
15 OPEN1，4：PRINT\＃1，＂UNSYMMETRICAL 2－SECTIDN LAG CIRCUIT＂：CLJSE1， 4
20 PRINT＂（WITH／WITHOUT RESISTIUE LOAD）＂
25 OPEN1，4：PRINI\＃1，＂（WITH／WITHOUT RESISIIUE LDAD）＂：CLDSE1， 4
30 PRINT＂＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＂：PRINT
35 OPEN1， \(4:\) PRINT\＃1，＂＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＂：PRINT\＃1，：CLCSE1， 4
40 PRINT＂CDMPUTES UNLDADED OUTPUT IMPEDANCE AND PHASE ANGLE＂
45 DPEN1，4：PRINT\＃1，＂COMPUTES UNLOADED DUTPUT IMPEDANCE AND PHASE ANGLF＂
46 CLOSE1，4
50 PRINT＂（THEUENIN IMPEDANCE AND PHASE ANGLE？＂：PRINT
55 QPEN1， \(4:\) PRINT\＃1，＂（THEUENIN IMPEDANCE AND PHASE ANGLE）＂：PRINT\＃1，：CLCSE1， 4
60 PRINT＂COMPUTES UNLOADED EOUT／EIN AND PHASE ANGLE；＂
65 OPEN1，4：PRINT\＃1，＂COMPUTES UNLOADED ECUT／EIN AND PHASE ANGLE；＂：CLCSE： 4
70 PRINT＂LOADED EDUT／EIN AND PHASE ANGLE＂：PRINT
75 OPEN1， \(4:\) PRINT\＃1，＂LOADED EOUT／EIN AND PHASE ANGLE＂：PRINT\＃1，：CLOSE1， 4
80 INPUT＂R1（OMMS）－＂；RD
S0 OPEN1， 4 ：PRINT\＃1，＂R1（OHMS）＝＂；RO：CLGSE1，4
100 INPUT＂R2（OHMS）＊＂；RT
110 OPEN1，4：PRINT\＃1，＂R2（DHMS）＝＂；RT：CLOSE1，4
120 INPUT＂C1（MFD）＝＂；CD
130 QPEN1，4：PRINT\＃1，＂C1（MFD）－＂；CO：CLOSE1，4
```


## Appendix A

```
140 INPUT "C2 (MFD)=";CI
150 DPEN1,4:PRINT"1,"C2 (MFD)=";CT:CLOSE1,4
160 INPUT "RL (OHMS)=";RL
170 DPEN1,4:PRINT#1,"RL (OHMS)=";RL:CLOSE1,4
18O INPUT "F (HZ)=";F:PRINT
190 DPEN1,4:PRINT#1,"F (HZ)=";F:PRINT#1,:CLOSE1,4
200 XO-1/(6.2.332*F*CO*10†-6)
202 XT=1/(6.2日32*F*CT*10!-6)
205 AB=RO*XO:BA=-5.2B32/4
210 AC=(RD tこ+XD+こ) !.5:CA=-ATN(XD/RD)
215 AD=AB/AC:DA-BA-CA:AE=AD*COS(DA)
220 AF=AD*SIN(DA):AG-AE+RT:AK=(AG+2+AF+ᄅ) +.5
225 HA=-AIN(AF/AG):AJ=AH*XT
230 JA=MA-6.2832/4:AK=AF-XI:KA=FA-6.2832/4
235 AL=(AG tट+AK†ट) †.5:LA=-AIN(AK/AG)
240 AM-AJ/AL:MA=JA-LA:AN=AM:NA=MA:PF=F*NA
245 YZ=(RD+ट+XD†こ) t.5:ZY=-ATN(XD/RO)
247 WA=INT(AN)
250 PRINI "ZOUI (OHMS)=";WA
253 OPEN1,4:PRINT#1,"ZOUT (OHMS)=";WA:CLOSE1,4
255 XYmXD+XI:WX=(RT †こ+XY!己) t.5:XW=-ATN(XY/RI)
250 UW=WX*YZ:WU-XW+ZY:UU=UW/XD:UU=WU+G.2B32/4
2G5 WB=INT(-NA*360/6.2日32)
270 PRINT "PHASE ANGLE, DEGREES (RL OPENJ="; UB
280 OPEN1,4:PRINT#1,"PMRSE ANGLE, DEGREES (RL DPEN)=";WB:CLOSE1,4
290 IU=UU*COS(UU): UT=UU*SIN(UU):ZW=UT+XO
295 RS=(IUtこ+ZW+2) †.5:5R=-ATN(ZW/TU)
300 PU=XT/RS:UP=-SR-6. 2G32/4:GU=PU*RL
305 HU*AN*COS(NA):JU*AN*SIN(NA): UG=UP
307 WC=.01*INT(PU*100)
310 PRINT"EQUT/EIN (RL OPEN)=";WC
312 OPEN1, 4:PRINT#1, "EOUT/EIN (RL OPEN)=";WC:CLOSE1,4
315 KU=HU-RL:LU=(XU`こ+JU†こ)+.5
320 UL=-ATN(JU/KU):NU=GU/LU: UN=UG-UL
325 WD=.01*INT( (-UP*360/6.2832)*100)
330 PRINI "PHASE ANGLE (DEGREES)="; WD
335 DPEN1,4:PRINT#1,"PHASE ANGLE (DEGREES)=";WD:CLDSE1,4
340 WE=INI (AN)
350 PRINT "THEUENIN IMPEDANCE (DHMS)=";WE
355 OPEN1,4:PRINT#1,"THEUENIN IMPEDANCE (DHMS)="; WE:CLOSE1,4
360 WF=INT(-NA*360/6.2B32)
370 PRINT "PHASE ANGLE (DEGREES)=";WF
375 DPEN1,4:PRINT#1,"PHASE ANGLE (DEGREES)=";WF:CLOSE1,4
3EO WG=.01*INT(NU*100)
390 PRINI "EOUT/EIN (LOADED)*"; LG
395 OPEN1,4:PRINI#1,"EOUT/EIN (LDADED)-";WG:CLOSE1,4
400 WH=.01*INT((-UN*360/6.2日32)*100)
410 PRINT "PHASE ANGLE (DEGREES)=";WH:PRINT
420 OPEN1,4:PRINI#1,"PHASE ANGLE (DEGREES)=";WH:PRINT#1,:CLDSE1,4
4 3 0 ~ P R I N T ~ " * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * " , ~ P R ~ I N T ~
```



```
440 CLOSE1,4:END
```


## Sample Run

```
UNSYMMEIRICAL 己-SECIIDN LAG CIRCUIT
    (WITH/WITHOUI RESISIIUE LOAD)
COMPUTES UNLDADED OUTPUT IMPEDANCE AND PHASE ANGLE
(THEUENIN IMPEDANCE AND PHASE ANGLE)
COMPUTES UNLDADED EOUT/EIN AND PHASE ANGLE;
LOADED EOUT/EIN AND PHASE ANGLE
R1 (OHMS)=5000
R2 (OHMS)=50000
C1 (MFD)= .015
C2 (MFD)= 1.5E-03
RL (DHMS)=15000
F (HZ)= 1500
ZOUT (DHMS)= 41735
PHASE ANGLE, DEGREES (RL OPEN)= = 4 41
EOUT/EIN (RL OPEN)= .63
PHASE ANGLE (DEGREES)= 108.62
TMEUENIN IMPEDANCE (OHMS)= 41735
PHASE ANGLE (DEGREES)= 141
EDUT/EIN (LDADED)= . 17
PHASE ANGLE (DEGREES)= 79.92
```

PROGRAM 6-Lnsymmetrical two-section lead circuit, with and without resistive load

## Without Printer

```
5 REM PRG 6 W/D PRINTER
10 PRINT "UNSYMMETRICAL 2-SECTION LEAD CIRCUIT"
2O PRINT" (WITH OR WITHOUT RESISTIVE LOAD)"
30 PRINT "***************************************:PRINT
SO PRINT "COMPUTES UNLQADED EDUT/EIN AND PHASE ANGLE;"
GO PRINT "LDADED EOUT/EIN AND PHASE ANGLE"
70 PRINT:PRINT
80 INPUT "R1 (OHMS)=";RD
100 INPUT "R2 (OHMS)=";RT
120 INPUT "C1 (MFD)=";CD
140 INPUT "C2 (MFD)=";CT
160 INPUT "RL (OHMS)=";RL
180 INPUT "F (HZ)=";F:PRINT:N-O
200 X0-1/(6.2832*F*CO*10†-6)
203 XT=1/(6.2B32*F*CT*10†-6)
```



```
210 BA=ATN(XI/RS):AC=(RD† + +XD+2) 1.5
215 CA=ATN(XD/RD):AD=AB*AC:DA=BA+CA:AE=AD/RD
220 EA-DA:AF-AE*COS(EA):AG*AE*SIN(EA)
225 AH-AF-RD:AJ=(AH+2+AG+こ)+.5:JA-ATN(AG/AH)
230 AK=RT/AJ:KA=-JA:KA=KA*360/6.2832:KA=KA-180
240 IF ABS(KA)>180 THEN KA=KA +180
250 IF N=1 THEN 295
255 WA=.01*INT(AK*100)
```


## Appendix A

2GO PRINT＂UNLOADED EDUT／EIN＂＂；WA
265 WB＝．01＊INT（KA＊100）
270 PRINT＂PHASE ANGLE（DEGREES）$="$ ；WB：$N=N+1$
290 RT－RT＊RL／（RT＋RL）：GDTD 200
295 WC＝．01＊INI（AK＊100）
300 PRINT＂LOADED EDUT／EIN＝＂；WC
305 WD＝．01＊INT（KA＊100）
310 PRINT＂PHASE ANGLE（DEGREES）＝＂；WD
330 PRINT＂＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＊＂：PRINT
340 END

## With Printer

```
5 \mp@code { R E M ~ P R G ~ 5 ~ U I T H ~ P R I N T E R }
    10 PRINT "UNSYMMETRICAL 2-SECTION LEAD CIRCUIT"
    15 DPEN1, 4:PRINI#1, "UNSYMMEIRICAL 己-SECIION LEAD CIRCUII":CLOSEI,4
    己O PRINT" (WITH OR WITHOUT RESISTIUE LOAD)"
25 OPEN1,4:PRINT#1," (WITH OR WITHOUT RESISTIUE LOAD)":CLOSE1,4
30 PRINT "************************************":PRINT
40 DPEN1, 4:PRINI#1, "***************************************":PRINT#1, : CLISSE1,4
5O PRINT "COMPUTES UNLQADED EQUT/EIN AND PHASE ANGLE;"
55 OPEN1,4:PRINT#1,"COMPUTES UNLDADED EOUT/EIN AND PHASE ANGLE;":CLOSE1,4
60 PRINT "LOADED EOUT/EIN AND PHASE ANGLE."
65 OPEN1,4:PRINT#1,"LDADED EOUT/EIN AND PHASE ANGLE.":PRINT#1,:PRINT#1,
60 CLOSE1,4
70 PRINT:PRINT
日0 INPUT "R1 (OMMS)=";RO
S0 DPEN1,4:PRINI#1,"R1 (OHMS)-";RD:CLDSE1, 4
100 INPUT "R2 (OHMS)=";RT
110 DPEN1,4:PRINT#1,"R2 (DHMS)m";RT:CLOSE1,4
120 INPUT "C1 (MFD)=";CO
130 OPEN1,4:PRINT#1, "C1 (MFD)=";CD:CLOSE1,4
140 INPUI "C2 (MFD)=";CI
150 OPEN1,4:PRINT#1, "C2 (MFD)=";CT:CLOSE1,4
160 INPUT "RL (OHMS)=";RL
170 OPEN1,4:PRINI#1,"RL (OHMS)=";RL:CLOSE1,4
180 INPUT "F (HZ)=";F:PRINT:N=O
190 OPEN1,4:PRINT#1,"F (HZ)=";F:PRINT#1,:CLDSE1,4
200 XO=1/(6.2832*F*CO*10†-6)
203 XT=1/(G.2g32*F*CT*10T-6)
205 RS=RO+RI:AB=(RSt2+XI +2)t.S
210 BA=ATN(XI/RS):AC=(RO+2+XD+2) 1.5
215 CA=ATN(XD/RD):AD=AB*AC:DA=BA+CA:AE=AD/RD
220 EA=DA:AF=AE*COS(EA):AG=AE*SIN(EA)
225 AH=AF-RD:AJ=(AH+2+AG +2) !.5:JA=ATN(AG/AH)
230 AK=RT/AJ:KA=-JA:KA=KA* 360/6. 2832:KA=KA-180
240 IF ABS(KA)>180 THEN KA=KA+180
250 IF N=1 THEN 295
255 WA=.01*INT(AK*100)
2EO PRINT "UNLDADED EDUT/EIN=";WA
263 OPEN1, 4:PRINT#1,"UNLDADED EOUT/EIN-"; WA:CLOSE1, 4
265 山B=.01*INT(KA*10O)
270 PRINT "PHASE ANGLE (DEGREES)-";WB:N-N+1
280 OPEN1,4:PRINT#1, "PHASE ANGLE (DEGREES)="; WB:CLDSE1,4
290 RT-RT*RL/(RI+RL):GOIO 2OO
295 WC=.01*INT (AK*100)
300 PRINT "LOADED EDUT/EIN-"; UC
303 OPEN1,4:PRINT#1, "LDADED EDUT/EIN=";WC:CLOSE1,4
305 WD-.01*INT(KA*100)
310 PRINT "PHASE ANGLE (DEGREES)=";WD
```

```
320 DPEN1,4:PRINT#1,"PHASE ANGLE (DEGREES)=";WD:CLOSE1,4
330 PRINT "****************************************":PRINT
335 OPEN1,4:PRINT#1,"********************************************:PRINT#1,
337 CLOSE1,4
340 END
```

Sample Run
UNSYMMETRICAL 2-SECTIDN LEAD CIRCUIT (WITH OR WITHOUT RESISTIUE LOAD)

```
**************************************
```

COMPUTES UNLOADED EDUT/EIN AND PHASE ANGLE; LOADED EDUT/EIN AND PHASE ANGLE.

R1 (OHMS)=5000
R2 (DHMS)= 50000
C1 (MFD) .015
C2 (MFD)=1.5E-03
RL (DHMS)= 15000
F(HZ)- 1500
UNLDADED EOUT/EIN= . 31
PHASE ANGLE (DEGREES)--108.63
LOADED EDUT/EIN= .OB
PHASE ANGLE (DEGREES)=-133.25

## Appendix B

## Program Conversions

Robert L. Kruse

## IBM ${ }^{\circledR}$ PC AND PC JR. ${ }^{\text {M }}$

A conversion of the Commodore 64 Program No. 5 (Appendix A) for the $I^{(B M}{ }^{\circledR}$ PC or PC Jr. ${ }^{\text {TM may be written as shown in }}$ Fig. B-1. Observe the following points:

1. The programs provided in Appendix A illustrate the distinctions that are involved in running routines with a printer, and without a printer. Note that when a printer is used, a duplicate line will be required to the input and print command lines, with its proper coding. This duplicate line permits the program to be displayed on both the video monitor and on the printer. Printer coding for the Commodore is more complex than for the IBM, as seen in the examples. Because the Commodore program opens with a file and device number (open 1,4 ), print the file number (print\#1,) and then close the file (close 1,4), the free memory is diminished and the amount of data that may be processed is limited in a long program. By way of comparison, th IBM PC merely requires addition of a duplicate line to the input and print
lines, starting with an LPRINT code as shown in Fig. B-1.
2. Typically, values will be processed to the seventh decimal place. To control the number of decimal places that will be printed out (rounding-off process), a subroutine using string functions is employed to accommodate the IBM PC. This is shown in line 8 of Fig. B-1. Here the entry A $\$=$ "\#\#\#\#\#\#" indicates that when a PRINT USING A\$ or LPRINT USING A\$ statement follows, a whole number is to be printed. Changing to "\#\#\#\#\#\#.\#" indicates one decimal place;
"\#\#\#\#\#\#.\#\#" indicates two decimal places, etc. This is illustrated at lines 13, 14, and 15 of Fig. B-1. The LPRINT USING A\$ and PRINT USING A\$ produce the whole numbers 19095 and 86 in the results. Without the rounding off of the results, the numbers would have been 19094.82 and 85.77663 . Thus in the conversion of any of the programs for use on the IBM PC, insert a string function to indicate the number of decimal places desired.

## Appendix B

```
1 LFFINT "INFUT IMFEDANCE AND FHASE ANGLE OF FLLC FAFALLEL FESONANT CIRCUIT"
2 FFINT "INFUT IMFEDANCE AND FHASE ANGLE OF FLC FAFALLEL FESONANT CIFCLIT"
T LFFINT"":FFINT"":INFUT "L (mH)=":L
4 LFFINT "L (mH)=";L:INFUT "C (MfiJ)=";C
S LFFFINT "C (Mfd)=":C:INFUT "FLL (Ohms)=";FL
6 LFFINNT "FLL (OHms)=";FL:INFUT "FCC (Ohms)=";FC
7 LFFINNT "FC (OHms)=";FRC:INFUT "f (Hz)=";F
8 LFFRINT "f (Hz)=";F:LFFINT"":FRINT"":A ="#######"
9 XL=6. 2قこ2*F*L*.001: XC=1/(0.2gこ2*F*C*10*-6)
```



```
11 FT=FL+FRC:XT=XL-XC:DE=(FTT2+XT, 2)* 5:ED=ATN(XT/FT)
12 ES=ZL*ZC:SE=LZ+CZ:HS=BS/DE:SH=SE-ED
LZ LFFINT "Zin (OMms)=";USING A#;HS:FFINT "Zin (Ohms)=":USING A生;HS
14 LFFINT "FHase Angle (Degrees)=":USING Aक;SH*S6O/G.2BS2
15 FFINNT "Fhase Anoje (Degrees)=":USING As;SH*SoO/G.28.S
16 END
```

INFUT IMFEDANCE AND FHASE ANGLE OF FLL FAFGLLEL FESONANT CIFCUIT

```
L (mH)= 160
C (Mfd)=.15
FiL (Ohins)== S
FiC (OMms)=1
f (Hz)=1000
Zin (Ohms:= 19095
Fhase Angle (Degrees)= Bo
```

Fig．B－1

## APPLE ${ }^{\circledR}$ IIe AND II＋

Apple ${ }^{®}$ II + conversions for the Com－ modore $64^{\circledR}$ programs（Appendix A）may be written as shown in Fig．B－2．Observe the following points：

1．Comparatively，Apple II＋printer coding is somewhat similar to that of the Commodore 64 in that the input and print command lines are dup－ licated with an opening command （PR\＃1）and a closing command （PR\＃0）．

2．Rounding－off printout（number of displayed decimal places）is controlled by means of a subroutine employing the INT function when coding Apple Ile and II＋programs．Note that the Commodore 64 also uses the INT function for this purpose．The proper entries to obtain the desired number of decimal places are：
$\mathrm{Q}=\operatorname{INT}(\mathrm{R})$
$\mathrm{Q}=.1 * \operatorname{INT}(\mathrm{R} * 10)$
［Whole Number］
［One Place］
$\mathrm{Q}=.01 * \mathrm{INT}(\mathrm{R} * 100)$
［Two Places］
［Three Places］

Etc．

Thus the statement:

$$
60 \text { PRINT "R1 (OHMS) = ";R }
$$

should be written
$55 \mathrm{Q}=.01 * \operatorname{INT}(\mathrm{R} * 100)$
60 PRINT "R1 (OHMS) = "; Q
to obtain a result to two decimal places.

```
10 GOSUE 145
OO FRINT "": FFINT "":
OO INFUT "L (mH)=":L
40 INFUT "C (Mfd)=":C
So INFUT "FLL (Ohms)=";FiL
60 INFUT "FC (Dhms)=";FC
70 INFUT "f (Hz)=;F
B0 FFINT "":FFINT "": HOME : GOSUE 147
31 FR# 1: FFINT "": FFINT "": FFINT "L (mH)=":L
82 FFINT "C (Mfd)=;C
gS FFINT "Fi_ (Ohms)=";FiL
84 FRINT "FC (Ohms)=":RC
85 FRINT "f (Hz)=":F
86 FRINT "": F'RINT "": F'Fi# 0
90 XL = 6.28.52 * F * L * .001: XC = 1 / (6. 28.32*F * C 10 * -6)
```



```
    FL) : CZ = - ATN {XC / FCC)
```



```
    RT)
12O ES = ZL * ZC : SE = LZ + CZ : HS = BS / DE : SH = SE - ED
125 OC = INT (HS)
130 FR# 1 : FRINT "Zin (Ohms)=":OC
135 OF = INT (SH * 360 / 6.28.2)
140 FFINT "Fhase Angle (Degrees)=":GF
144 END
14S FFINT "INFUT IMFEDANCE AND FHASE ANGLE OF FLC FAFALLEL FESONANT CIRCUIT" :
    FFINT ""
140 FETURN
147 FF:# 1: FRINT "INFUT IMFEDANCE AND FHASE ANGLE OF FLC FAFIALLEL FESONANT CIRC
    UIT" : FRINT "" : FF'# %
148 FETUFN
```

JINFUT IMFEDANCE AND FHASE ANGLE OF RLC FAFIALLEL FESONANT CIRCUIT
$L(m H)=160$
C $(M f d)=.15$
FiL (Ohms) $=3$
FiC (Ohms) $=1$
f $(H z)=1000$

Zin (Ohms) $=19094$
Fhase Angle (Degrees) $=85$

Fig. B-2

## TYPICAL CONVERSION "BUGS"

Error messages resulting from incorrect coding are frequently vague, and the programmer must carefully proofread the routine. Inasmuch as programmers tend to repeat "pet" coding errors, somcone else should also proofread the routine. Some common "bugs" are:

1. Numeral 0 typed in instead of capital O .
2. Letters in a two-letter variable reversed (e.g., PQ for QP).
3. Semicolon typed in instead of a colon (or vice versa).
4. Complete program line omitted.
5. "Bug" hidden in the program memory caused by "illegal" word-processing operation. (Retype the complete line if this trouble is suspected.)
6. Plus sign erroneously used for a required minus sign, or plus sign inserted in a coded data line that requires a blank space to imply a plus sign.
7. Improper units employed in assignment of INPUT variables. Numerical values can, for example, be specified within permissible ranges by using compatible units in coding of programs (e.g., the programmer has a choice of farad, microfarad, or picofarad units).
8. Reserved word used illegally for variables. For example, if the programmer attempts to use OR, AND, COM, or INT as a variable, the program will not run.
9. Factors used incorrectly (e.g., $10^{6}$ for $10^{-6}$ or $6.2832 / 360$ for $360 / 6.2832$ ). Note also that logarithms of negative numbers will not be processed.

When a RUN stops at some point during the processing interval and an error message is displayed (or when a RUN stops with no error message), the programmer can operate the computer in its calculator (direct) mode to display successively the value of variables that have been processed up to the "bug" point. Accordingly, errors often become obvious. For example, the programmer may find a zero value for a variable or an extremely large value for a variable indicating (division by zero). Or, the programmer may note that the computed value for the variable is greater than one, although its correct value must be less than one (or vice versa). Patience and reasoning will help the programmer identify the coding error.

Programs sometimes appear to have coding "bugs" when the difficulty is actually an erroneous INPUT. Consider, as an illustration, the programmer who accidentally INPUTs 1500 instead of 15000 . Because of this small error, a "bug" will appear to be in the program. It is good practice to re-RUN such a program, to ensure that the trouble is actually in the coding and not in an erroneous INPUT.

## LINE-BY-LINE CHECKOUT

Although a program may RUN without any error messages, an incorrect answer is sometimes printed out. This difficulty requires a careful line-by-line checkout. Incorrect variables are often responsible-this involves "slips" such as R for RE, or VU for UV. A more subtle error in variable specification is encountered when a heuristic program is written with "recycled" equations.

## Program Conversions

In this situation, the INPUT variables may be $A, B, C$, and $D$. Then, the values of these INPUT variables may be redefined in following equations, and redefined again in following loops. Accordingly, the INPUT values must be kept separate from the redefined values; this is accomplished by coding $A A=A * f(X)$, instead of $A=A * f(X)$.

When an initial line-by-line checkout does not identify the "bug," remember that a PRINT command can be inserted into the program following each equation or logical operation. In turn, the programmer can re-
view the processing action in a printout and find the error in the program. This is a particularly helpful procedure when equations are "recycled" in a survey or heuristic routine.

Sometimes, the programmer is unable to identify the "bug(s)" in a long and involved routine. In this situation, it is advisable to ask someone else to retype the program. This procedure allows a fresh viewpoint, as well as eliminates the programmer's favorite and frequently repeated typing errors.

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Note: Pages listed in bold type indicate coverage in charts or tables

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[^5]:    *These thicknesses are intended to express the desired thickness in decimal fractions of an inch. They have no relation to gage numbers; they are approximately related to AWG sizes 3-34.

    Courtesy Whitehead Metal Products Co., Inc.

[^6]:    *"Wiring confined" ratings are based on 15 or more wires in a bunde, with the sum of all the actual load currents of the bundled wires not exceeding $20 \%$ of the permitted "Wiring contined" sum total carrying capacity of the bunded wires. These ratings approximate $60 \%$ of the free-air ratings (with some variations due to rounding). They should be used for wire in harnesses, cable, conduit, and general chassis conditions. Bundes of fewer than 15 wires may have the allowable sum of the load currents increased as the bundle approaches the single-wirc condition.

[^7]:    *Any number to the zero power is 1 .

[^8]:    The expression "are sin" or "sin-1" indicates "the angle whose sine is tangent is . . . ".

[^9]:    *Mass number of the tongest-lised of the known available forms of the element, usually symhetic.
    tirams per liter.
    $\$$ Values in parentheses indicate an approximate salue.
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